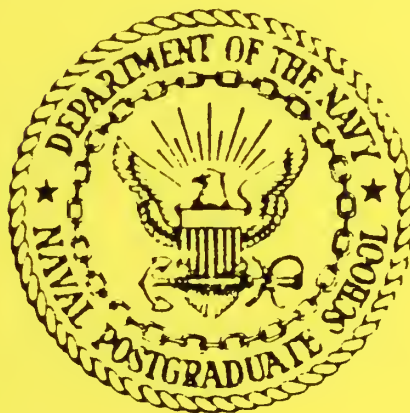


# NAVAL POSTGRADUATE SCHOOL

## Monterey, California



Monthly and Seasonal Climatology of the Northern  
Winter over the Global Tropics and  
Subtropics for the Period 1974 to 1983

Volume III. Surface Winds

by

James S. Boyle and C.-P. Chang

May 1986

Technical Report

May 1985 - May 1986

Approved for public release; distribution unlimited.

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NPS-63-86-002

NAVAL POSTGRADUATE SCHOOL  
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The work reported herein was supported by the National Oceanic and Atmospheric Administration, under Research Contracts NA83AAG03828 and 40AANW503656.

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REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER NPS-63-86-002	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle)  Monthly and Seasonal Climatology of the Northern Winter over the Global Tropics and Subtropics for the Period 1974 to 1983. Volume III. Surface Winds		5. TYPE OF REPORT & PERIOD COVERED Technical Report for May 1985 - May 1986
		6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(s)  James S. Boyle and C.-P. Chang		8. CONTRACT OR GRANT NUMBER(s)  NOAA Research Contracts NA83AAG03828 & 40AANW503656
9. PERFORMING ORGANIZATION NAME AND ADDRESS  Naval Postgraduate School Monterey, California 93943		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
11. CONTROLLING OFFICE NAME AND ADDRESS Climate Analysis Center/NMC National Oceanic and Atmospheric Administration Washington, D.C. 20233		12. REPORT DATE May 1986
		13. NUMBER OF PAGES 142
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		15. SECURITY CLASS. (of this report)  UNCLASSIFIED
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report)  Approved for public release; distribution unlimited.		

17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)

18. SUPPLEMENTARY NOTES

19. KEY WORDS (Continue on reverse side if necessary and identify by block number)

Interannual Variations  
Tropical Climatology  
Winter Circulations

20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

This atlas of the surface circulation field contains northern winter monthly and seasonal mean wind analyses, velocity potential and streamfunction from 40°S to 60°N over a global belt for the period 1974 through 1983. In addition, the deviations of the individual annual seasonal and monthly means from their respective nine-year means are presented for the same variables. The basic wind data used are the operational Global Band Analyses of the United States Navy's Fleet Numerical Oceanography Center.

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## *ABSTRACT*

This atlas of the surface circulation field contains northern winter monthly and seasonal mean wind analyses, velocity potential and streamfunction from 40°S to 60°N over a global belt for the period 1974 through 1983. In addition, the deviations of the individual annual seasonal and monthly means from their respective nine-year means are presented for the same variables. The basic wind data used are the operational Global Band Analyses of the United States Navy's Fleet Numerical Oceanography Center.



## *1. INTRODUCTION*

This atlas depicts the wintertime (December, January, February) seasonal and monthly mean atmospheric surface motion fields for the period 1974/1975 to 1982/1983. The charts display surface streamfunction, wind vectors, isotachs, and velocity potential from 40°S to 60°N. In addition, to the nine-year seasonal and monthly means and the individual annual seasonal and monthly averages, the deviations of the individual seasonal and monthly means from their nine-year averages are also presented. The seasonal calculations are based on the months of December, January, and February. The data used as the basis for these motion fields are the Global Band Analysis (GBA) of the United States Navy's Fleet Numerical Oceanography Center (FNOC). The procedure used in producing these analyses are described in section 2.

The motion fields for the winters from 1974/75 to 1982/83 are of interest since the data cover a period not previously examined in other collections of data. Other works such as Oort (1983) and Krishnamurti et. al. (1983) have presented detailed analysis of the decade prior to 1974. The 1974 - 1983 period contains two El Nino/Southern Oscillation (ENSO) events, one occurring in 1976/77 and the other in 1982/83. The latter event is the most intense ENSO event yet observed. Also, the analyses presented here allow the FGGE winter to be placed in a longer term perspective since the FGGE/WMONEX experiment took place in the midst of the period.

## *2. DATA SOURCES, ANALYSIS AND COMPUTATIONAL PROCEDURES*

### *2.1 GLOBAL BAND ANALYSIS*

The wind data set used in this work are the operational analyses of the Global Band Analyses of FNOG. These data are produced four times daily by objective procedures on a mercator grid which extends from 40°S to 60°N. The use of the mercator secant projection results in a change in the actual distance between grid points from 140 km at 60°N to a maximum value of 280 km at the equator. The objective scheme is designed to take advantage of all the reports in the operational data base, surface synoptic, aircraft, pilot balloons, rawinsonde and satellite data.

The analysis is performed every six hours for the surface, 700, 400, 250 and 200 mb levels. The first guess field used as input for the objective analysis is the six hour persistence field. The approach is to first interpolate the irregularly spaced data to grid points using a successive corrections technique based on Cressman's (1959) method. The successive corrections method takes several scans through the data reducing the scan radius on each successive scan. Analyses are performed of both wind and temperature by this method. These fields are then adjusted to be consistent with a set of numerical variational analysis (NVA) equations which have incorporated the dynamical constraints of the momentum equations with friction included in the surface layer, (Lewis and Grayson, 1972). Temperature and wind fields are adjusted subject to mutual constraints on the fields. However, the surface and 200 mb wind data serve only as a lower and upper boundary condition for the NVA and are not subject to an adjustment.



## 2.2 COMPUTATION OF STREAMFUNCTION AND VELOCITY POTENTIAL

The streamfunction (  $\psi$  ) and velocity potential (  $\chi$  ) were computed from the following equations:

$$\nabla^2 \chi = \delta$$

$$\nabla^2 \psi = \zeta$$

where:

$\zeta$  is the relative vorticity =  $\partial v / \partial y - \partial u / \partial x$  and

$\delta$  is the divergence =  $\partial u / \partial x + \partial v / \partial y$ . Both  $\zeta$  and  $\delta$  were computed using centered differences on the GBA mercator grid taking the appropriate map scale factor into account.

Equation (2) was solved using the boundary condition that  $\chi = 0$  on the north and south boundaries which are at 60°N and 40°S respectively. The method used to compute  $\psi$  was essentially the method II of Shukla and Saha (1974). This technique uses the previously computed values of  $\chi$  to formulate boundary conditions for  $\psi$ .

The depiction of the divergence field appears reasonable away from the boundary. Comparison with the global fields produced by the National Meteorological Center (NMC) for the years since the NMC  $\chi$  fields have become available indicate that the effect of the boundary conditions on  $\chi$  is not significant between  $40^{\circ}\text{N}$  and  $30^{\circ}\text{S}$ . Thus, the  $\psi$  and  $\chi$  fields in the equatorial regions are sufficiently removed from the boundaries that we can assume that these values are not unduly affected by the choice of boundary conditions.

In addition, the windfield was directly decomposed into its rotational and divergent components using the method of Endlich (1967). This method does not require any assumption about the boundary conditions. The divergent wind vectors shown in the figures are not computed from  $\chi$  but are those computed by the Endlich technique. The excellent agreement between the  $\chi$  field and the divergent winds over the entire grid gives confidence in the accuracy of the computations.

### 3. DISCUSSION

The winter (DJF) mean nine-year data (Figs. A1 - A3) are in reasonable agreement with the data of Fu et. al. (1983), Wright et. al. (1985) and Newell et. al. (1974). The familiar features of all these data compilations are prominent in the present work. The Aleutian and Icelandic lows, the subtropical highs, the Siberian anticyclone and the west Australian heat low are all apparent. The  $\chi$  field shows a broad band of equatorial convergence, with maxima over South America, Africa and a zonally elongated

maxima centered on New Guinea. These features are consistent with the tropical outgoing longwave radiation (OLR) data, (Boyle and Chang, 1984). However, the South Pacific convergence zone (SPCZ) which is in evidence in the OLR data does not appear to be a distinct feature in the surface  $\chi$  field.

Figure 1 is a time, longitude plot of  $\chi$  winter, seasonal anomalies along the Equator. The sense of anomalies is that positive anomaly maxima imply convergence relative to the mean. The largest anomalies are found in the winters of 1981/82 and 1982/83, evidently in association with the strong ENSO event. These data indicate that one of the largest anomalies of 82/83 occurs over Africa (00 to 30°E). The relative suppression of convection west of 150°E and enhancement to the east, seen in the OLR anomalies, is also suggested by the  $\chi$  field. However, examination of the anomalies do not indicate as strong a relationship between the  $\chi_{sfc}$  and the OLR anomalies as exhibited between the  $\chi_{200mb}$  and OLR anomalies, Boyle and Chang (1983).

Further overviews of the interannual, seasonal variations are provided by Figs. II, III and IV. These are time, longitude plots of surface wind winter season anomalies along 40°N, 20°N and the Equator. In Fig. II the 82/83 ENSO event is prominent, with very large westerly anomalies around the dateline. The subtropical flow of Fig. III indicates a change in the zonal flow regime from the 78/79 winter to the 79/80 winter, probably a reflection in a shift in the position/strength of the subtropical anticyclone. The midlatitude flow in Fig. IV has the largest variations in the Pacific circulation; the strong variability is also seen in the data of Wright et. al. (1985). The large variations from 60°E to 90°E are in a region of very high terrain and thus, are of uncertain value.



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*FIGURE 1*

Time versus longitude plot of winter season anomalies of surface velocity potential averaged from 5°N to 5°S about the Equator. The ordinate labels refer to the year of the January of the winter involved. The contour interval is  $0.25 \times 10^6 \text{ ms}^{-2}$ . Dashed lines are negative, solid lines are positive values. The zero contour is suppressed.

*FIGURE II*

- (a) As in Fig. I except for the zonal wind component. The contour interval is  $0.25 \text{ ms}^{-1}$  (b)  
As in (a) except for the meridional wind component.

*FIGURE III*

As in Fig. II except the reference latitude is  $20^{\circ}\text{N}$ .

*FIGURE IV*

As in Fig. II except the reference latitude is  $40^{\circ}\text{N}$ .

*FIGURES A1 - A3*

Nine winter season (1974/75 - 1982/83 ) mean circulation fields at the surface. Variables displayed are wind vectors and isotachs streamfunction, and velocity potential. Contour interval for the streamfunction is  $2.0 \times 10^6 \text{ m}^2\text{s}^{-1}$ , for the velocity potential it is  $1.0 \times 10^6 \text{ m}^2\text{s}^{-1}$ , and for the isotachs it is  $2.5 \text{ ms}^{-1}$ . The vector scale is given in the upper right portion of the wind vector isotach plots. The grid intervals of the FNOC Global Band Analysis mercator grid are shown on the left hand side and bottom of each figure. The longitude grid is marked every  $30^\circ$  from the Greenwich meridian on the extreme left and the latitude is marked every  $10^\circ$  from  $40^\circ\text{S}$  at the bottom of the figure. The black dots on the wind vector plots indicate terrain heights greater or equal to 1000 m, smoothed to the GBA grid. The contour plots use the convention that negative values are dashed, positive values are solid. Although the sign of the streamfunction and velocity potential has no meaning in itself, this plotting convention allows the principal maxima and minima in these fields to be more readily discerned.



*FIGURES B1 TO B27*

Individual winter season mean and deviation circulation fields at the surface for the winters from 1974/75 to 1982/83. The deviations are differences from the nine-year seasonal mean ( Figs. A1 to A3). The figures are labeled with the year corresponding to the year of the January of the winter. Variables displayed are the wind vectors and isotachs, streamfunction, and velocity potential. For the mean fields the contour interval for the streamfunction is  $2.0 \times 10^6 \text{ m}^2 \text{ s}^{-1}$ , for velocity potential it is  $1.0 \times 10^6 \text{ m}^2 \text{ s}^{-1}$ , and for the isotachs it is  $2.5 \text{ ms}^{-1}$ . For the deviation fields the contour interval for the streamfunction is  $1.0 \times 10^6 \text{ m}^2 \text{ s}^{-1}$ , for velocity potential it is  $1.0 \times 10^6 \text{ m}^2 \text{ s}^{-1}$ , and for the isotachs it is  $1.5 \text{ ms}^{-1}$ . On the deviation plots the contours corresponding to negative values are dashed, those corresponding to positive values are solid. The zero contour is not drawn. The vector scale is given in the upper right part of the wind vector plots.

*FIGURES C1 TO C9*

Nine year (1974 to 1983) monthly mean circulation fields at the surface. The months displayed are December, January and February. Variables displayed are the wind vectors and isotachs, streamfunction and velocity potential. The contour interval for the streamfunction is  $2.0 \times 10^6 \text{ m}^2\text{s}^{-1}$ , for velocity potential it is  $1.0 \times 10^6 \text{ m}^2\text{s}^{-1}$ , and for the isotachs it is  $2.5 \text{ ms}^{-1}$ . The vector scale is given in the upper right part of the wind vector plots.

### *FIGURES D1 TO D81*

Individual monthly mean and deviation circulation fields at the surface for the months from December 1974 to February 1983. The deviations are differences from the nine-year monthly mean ( Figs. C1 to C9). The months displayed are December, January, and February. Variables displayed are the wind vectors and isotachs, streamfunction, and velocity potential. For the mean fields the contour interval for the streamfunction is  $2.0 \times 10^6 \text{ m}^2 \text{ s}^{-1}$ , for velocity potential it is  $1.0 \times 10^6 \text{ m}^2 \text{ s}^{-1}$ , and for the isotachs it is  $2.5 \text{ ms}^{-1}$ . For the deviation fields the contour interval for the streamfunction is  $1.0 \times 10^6 \text{ m}^2 \text{ s}^{-1}$ , for velocity potential it is  $1.0 \times 10^6 \text{ m}^2 \text{ s}^{-1}$ , and for the isotachs it is  $1.5 \text{ ms}^{-1}$ . On the deviation plots the contours corresponding to negative values are dashed, those corresponding to positive values are solid. The zero contour is not drawn on the deviations. The vector scale is given in the upper right part of the wind vector plots.

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1983 CHIS CON=  $2.50 \times 10^{-1}$  TOT DF LAT= 0.0 AVG= 2

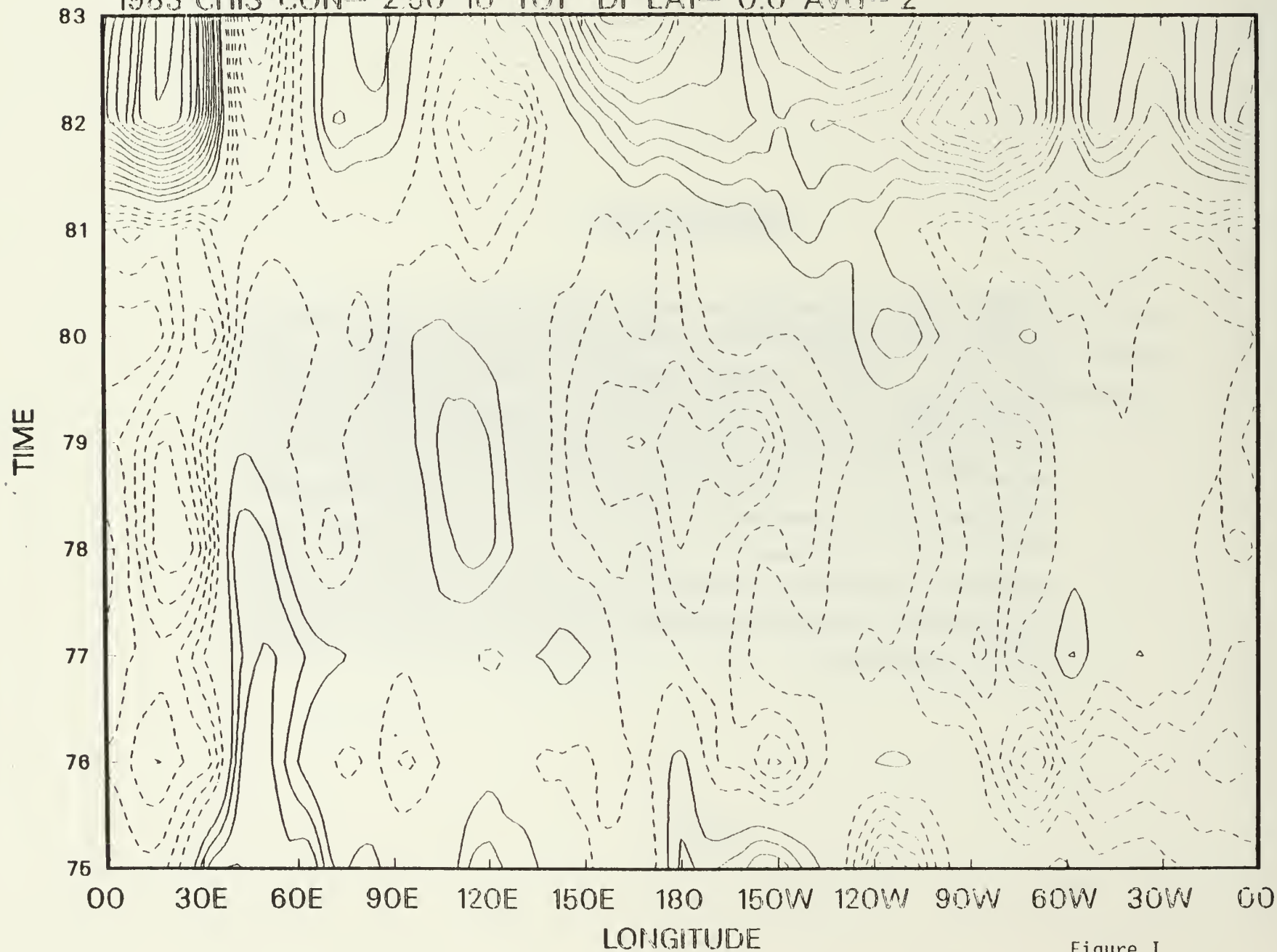
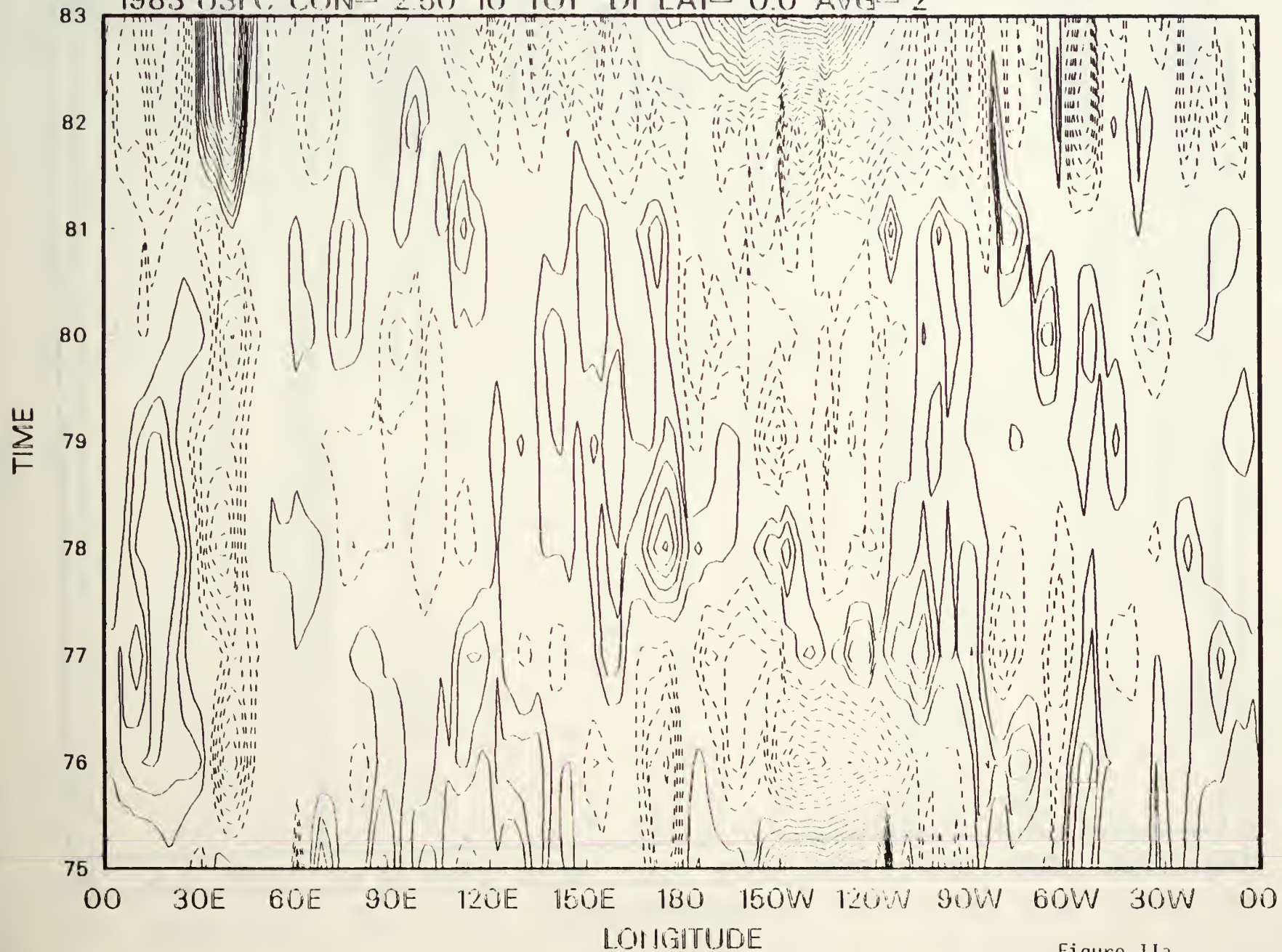


Figure I

USFC UNFILT DJF  
1983 USFC CON=  $2.50 \times 10^{-1}$  TOT DF LAT= 0.0 AVG= 2





VSFC UNFILT DJF  
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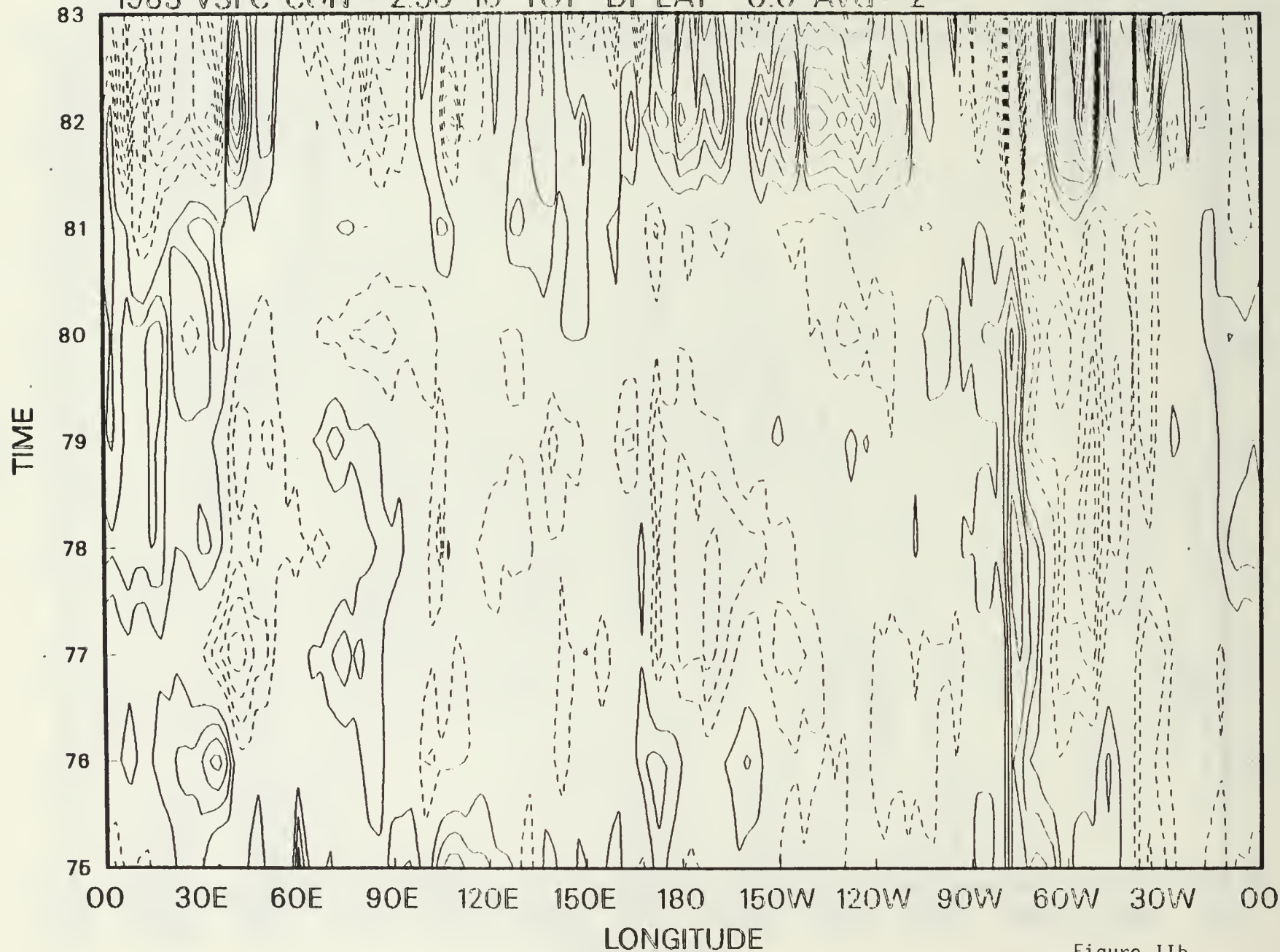


Figure IIb



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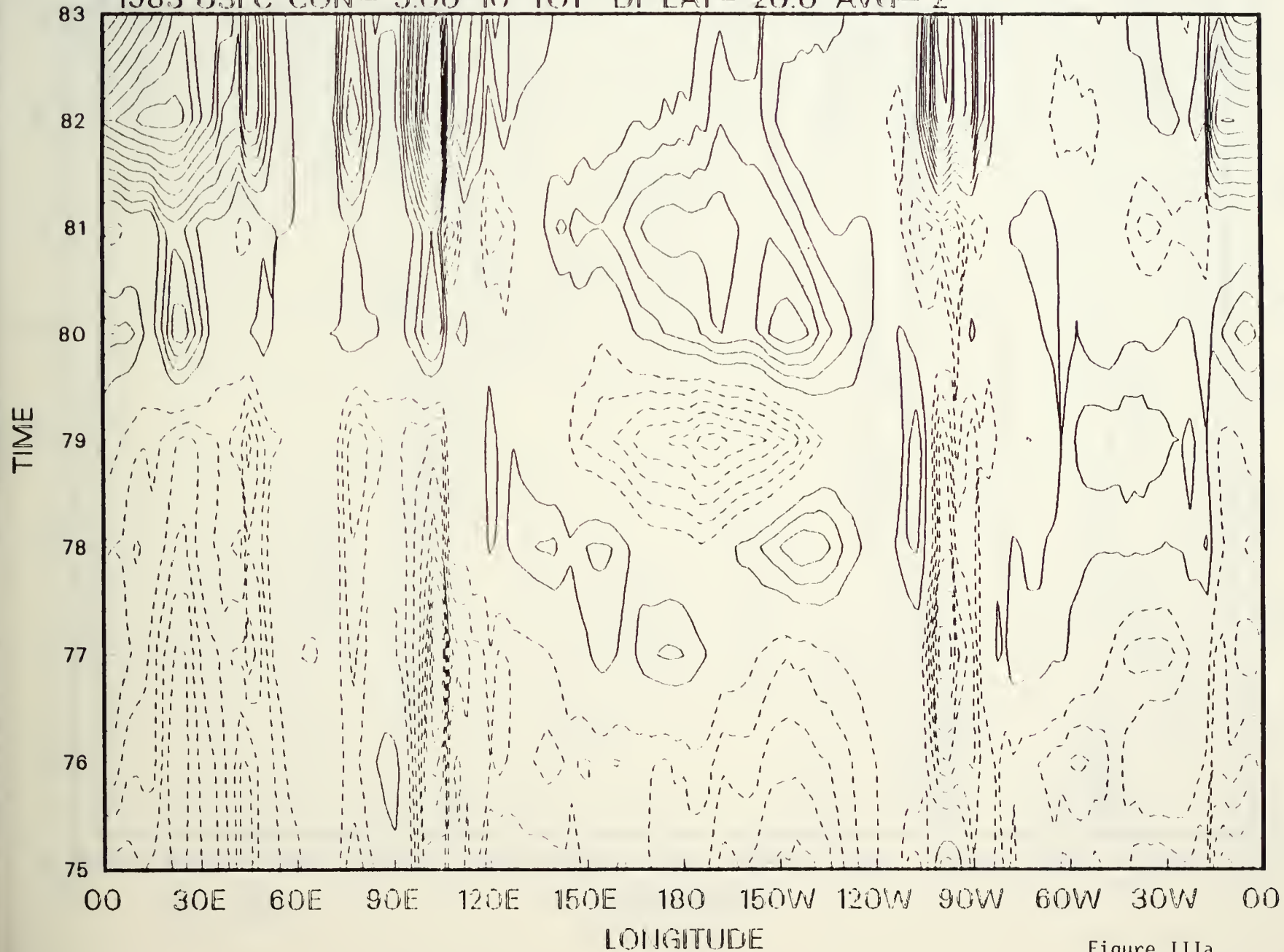


Figure IIIa

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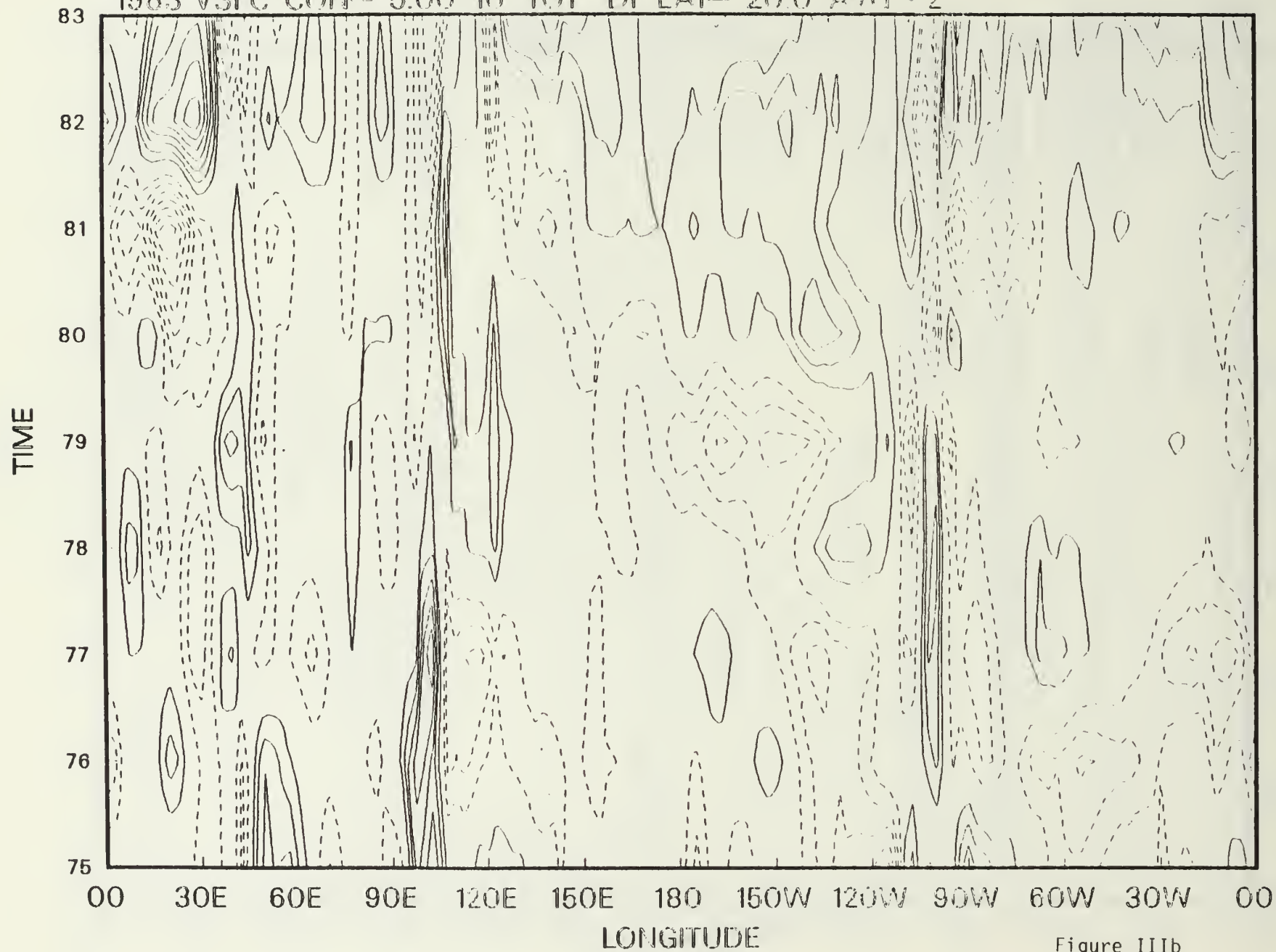


Figure IIIb

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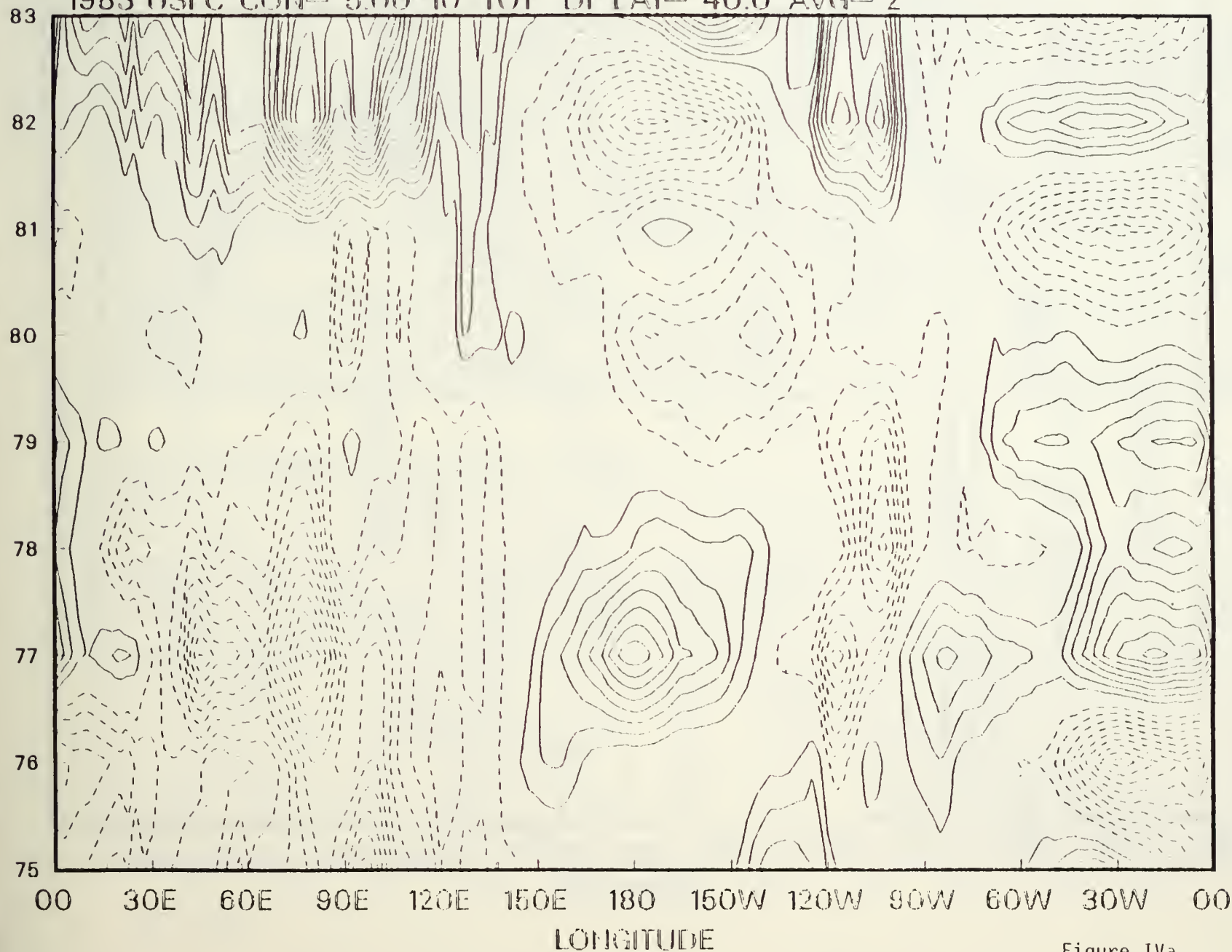


Figure IVa



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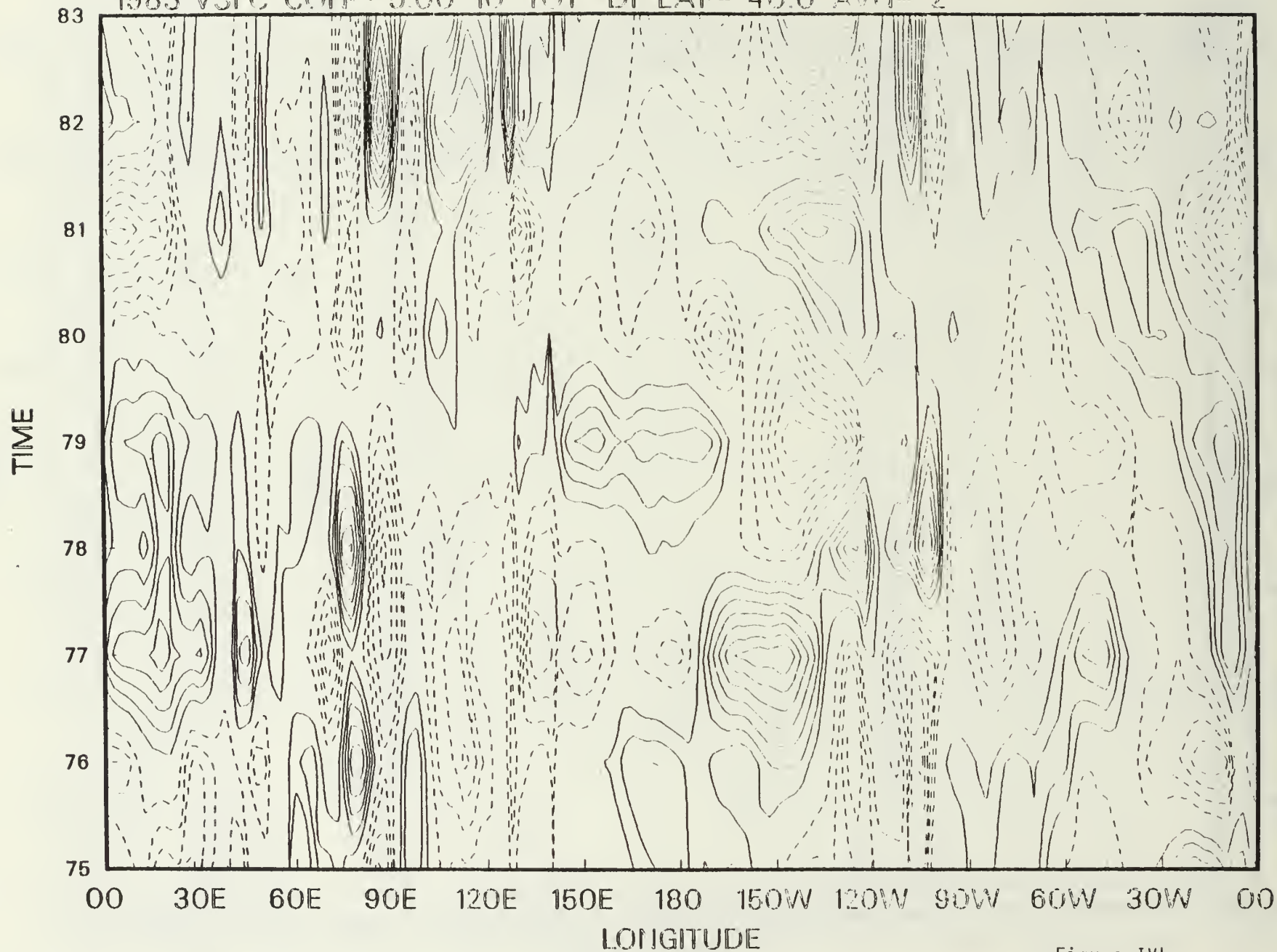
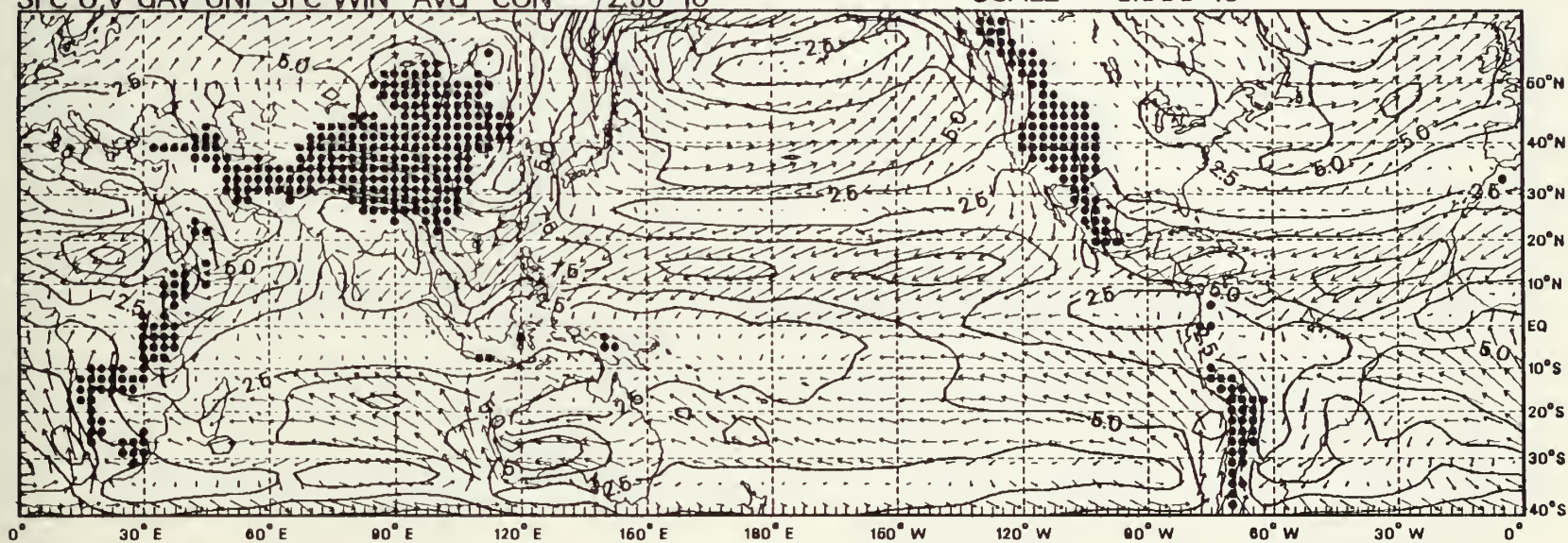


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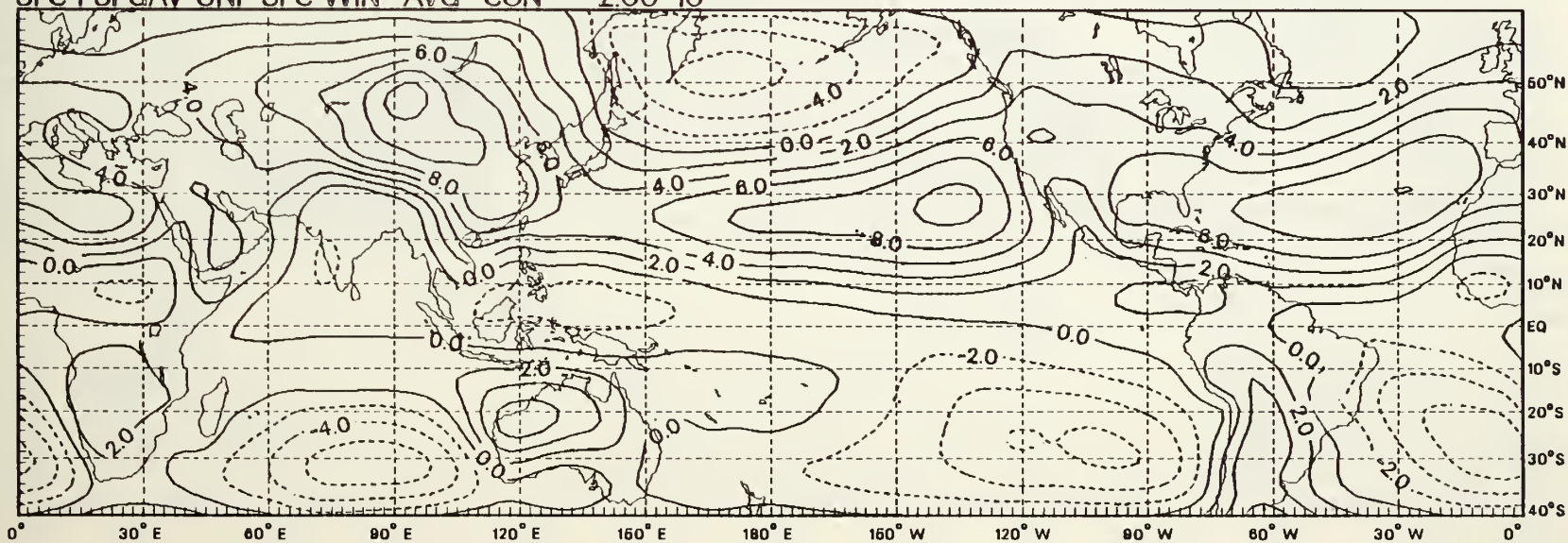
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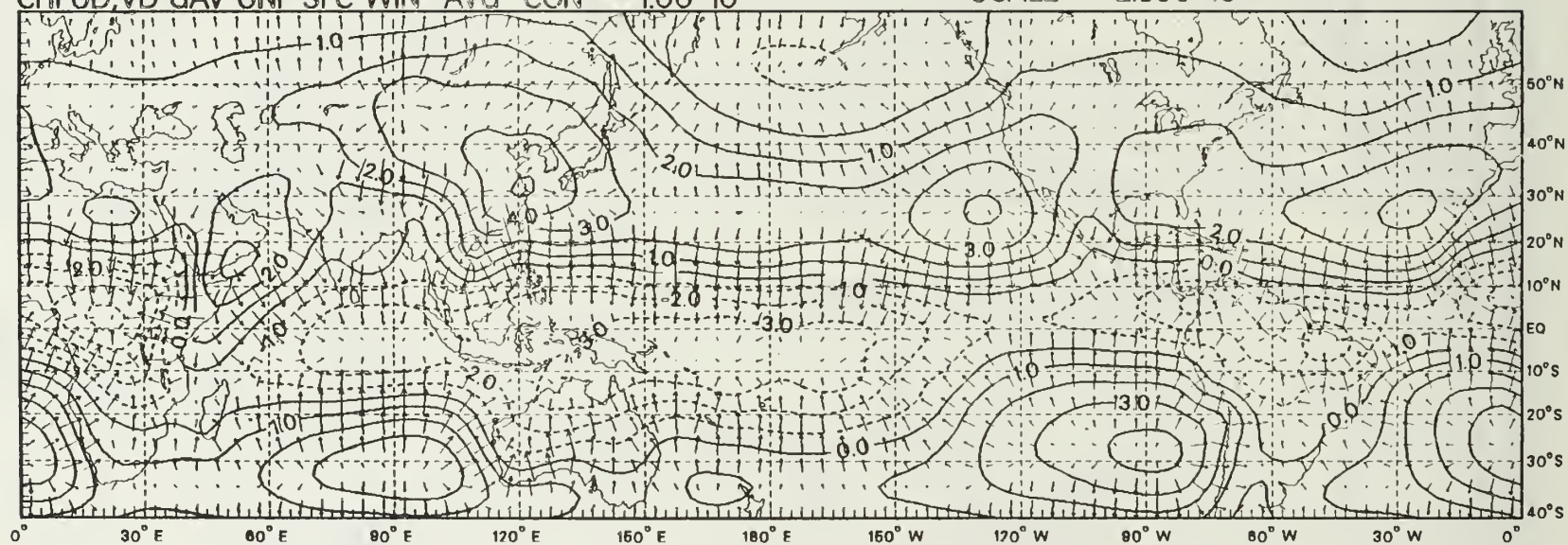


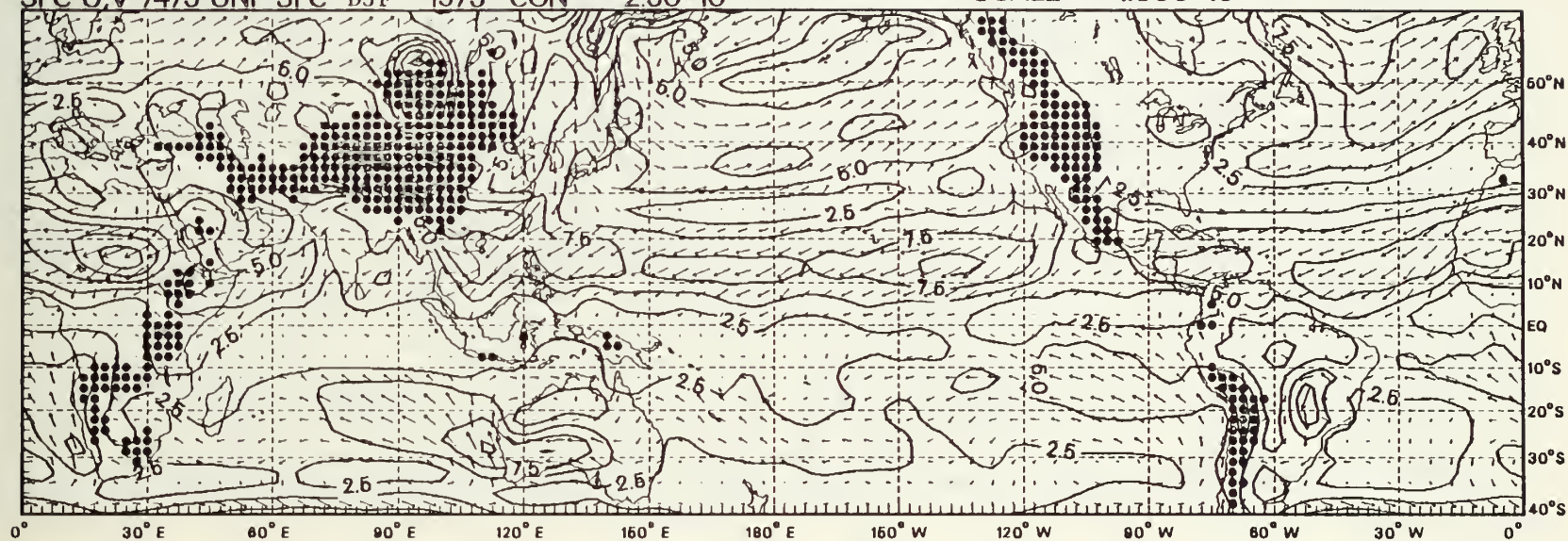
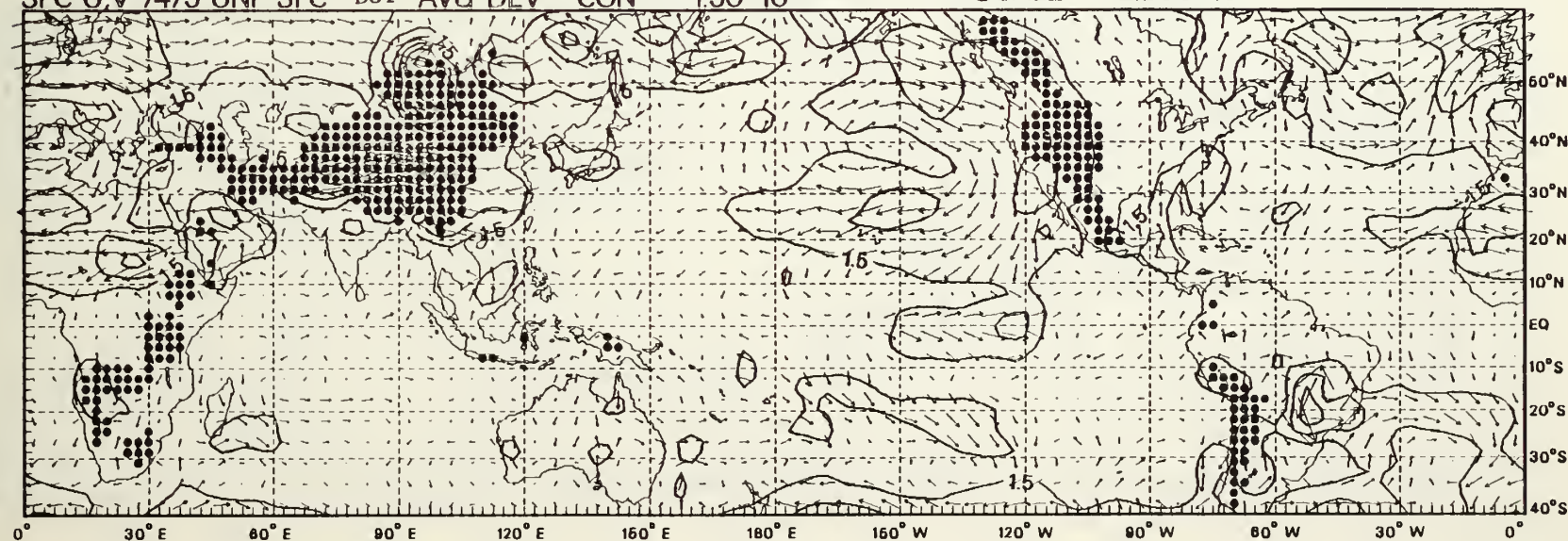


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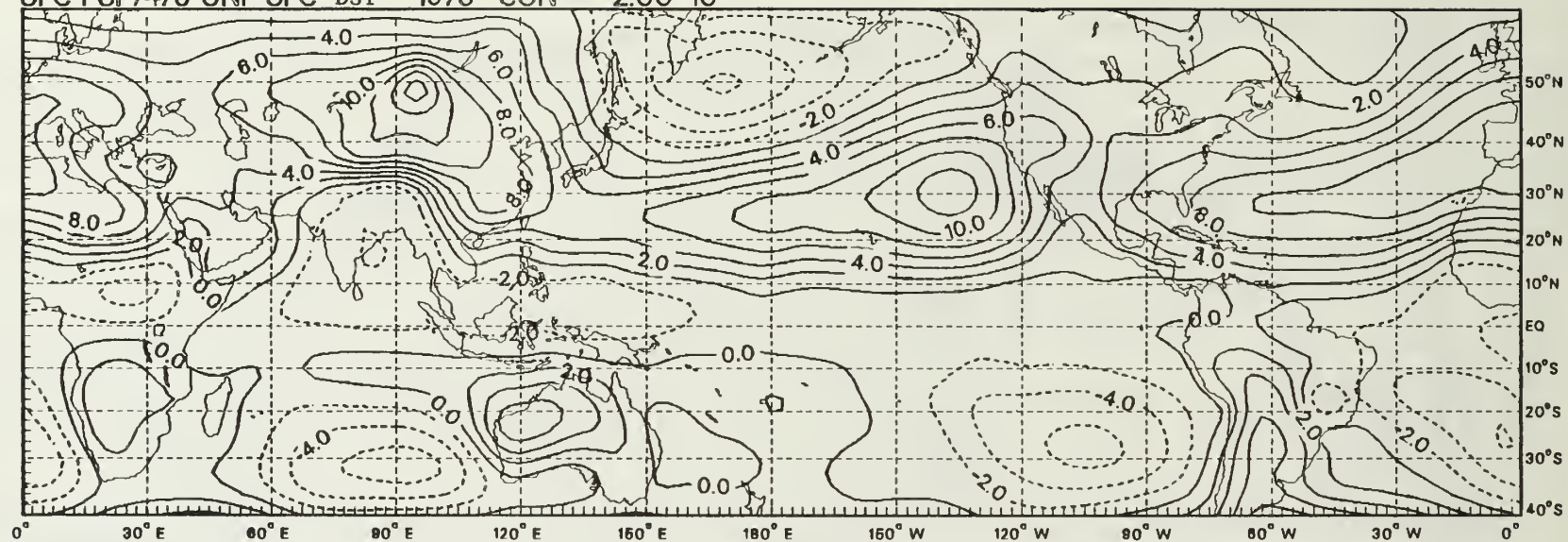
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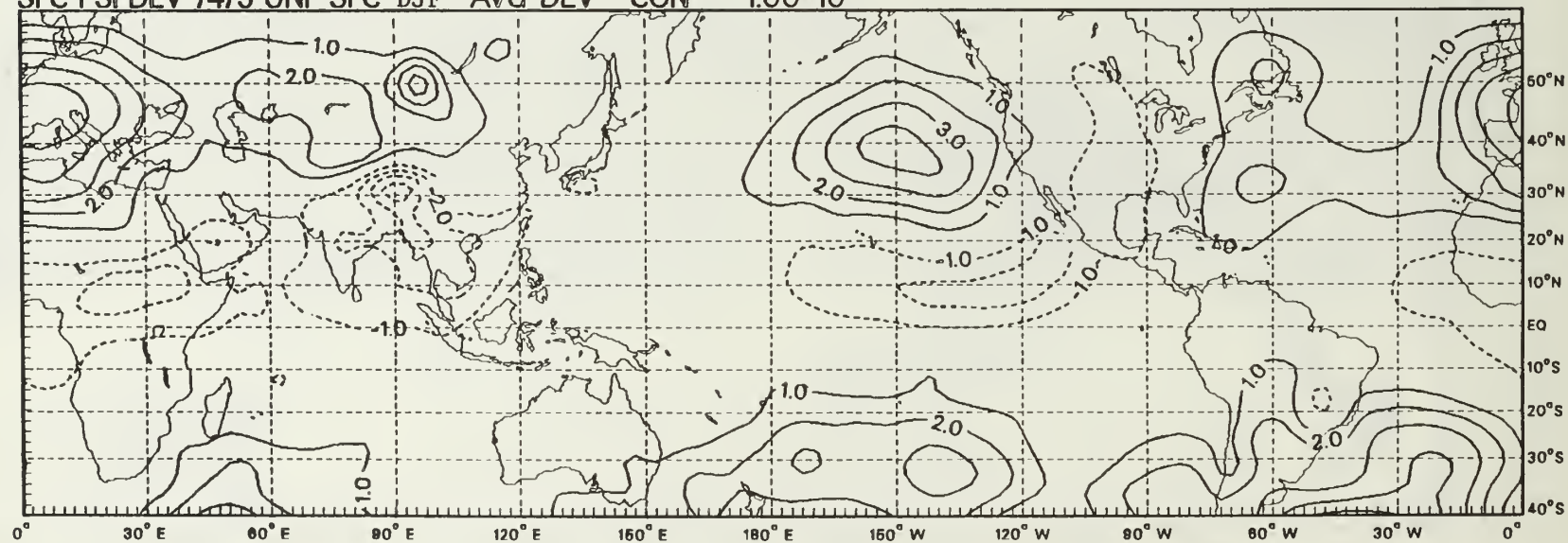
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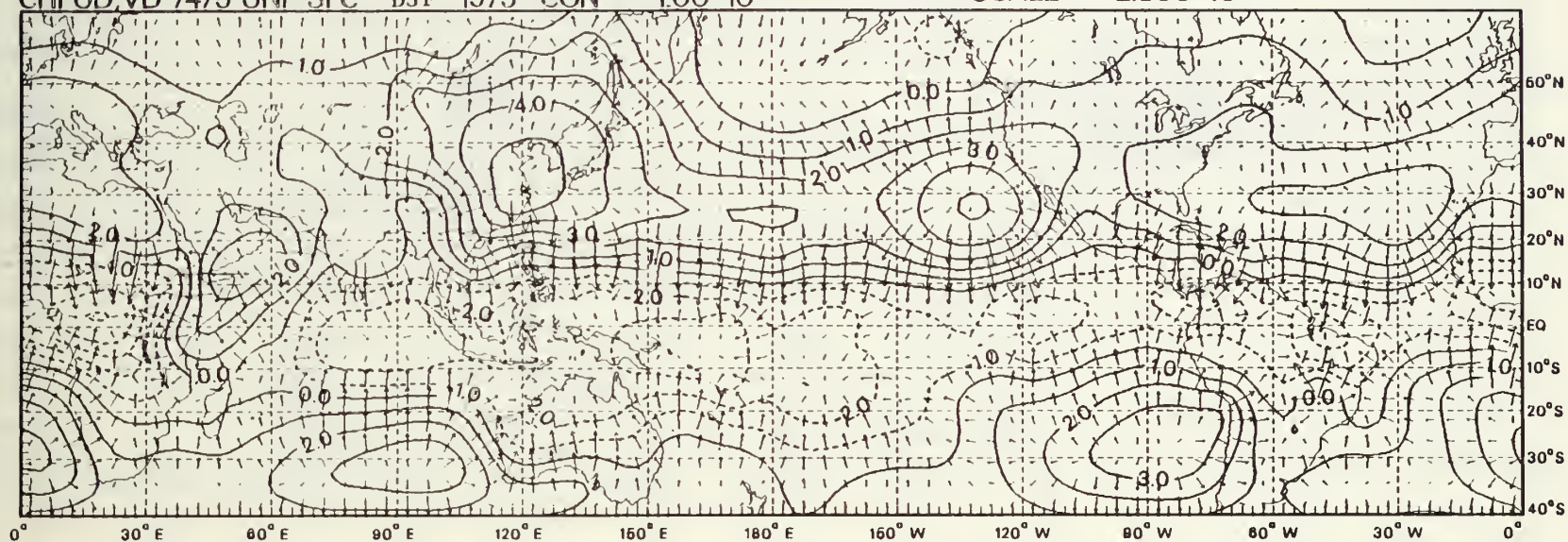
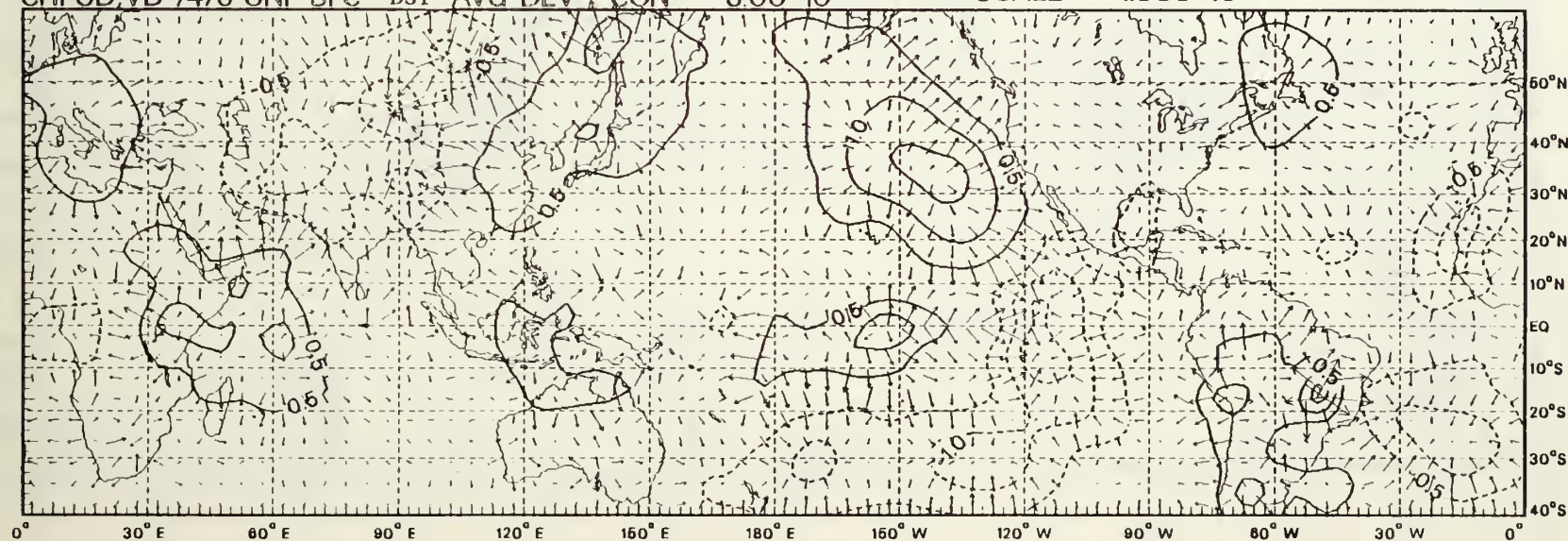
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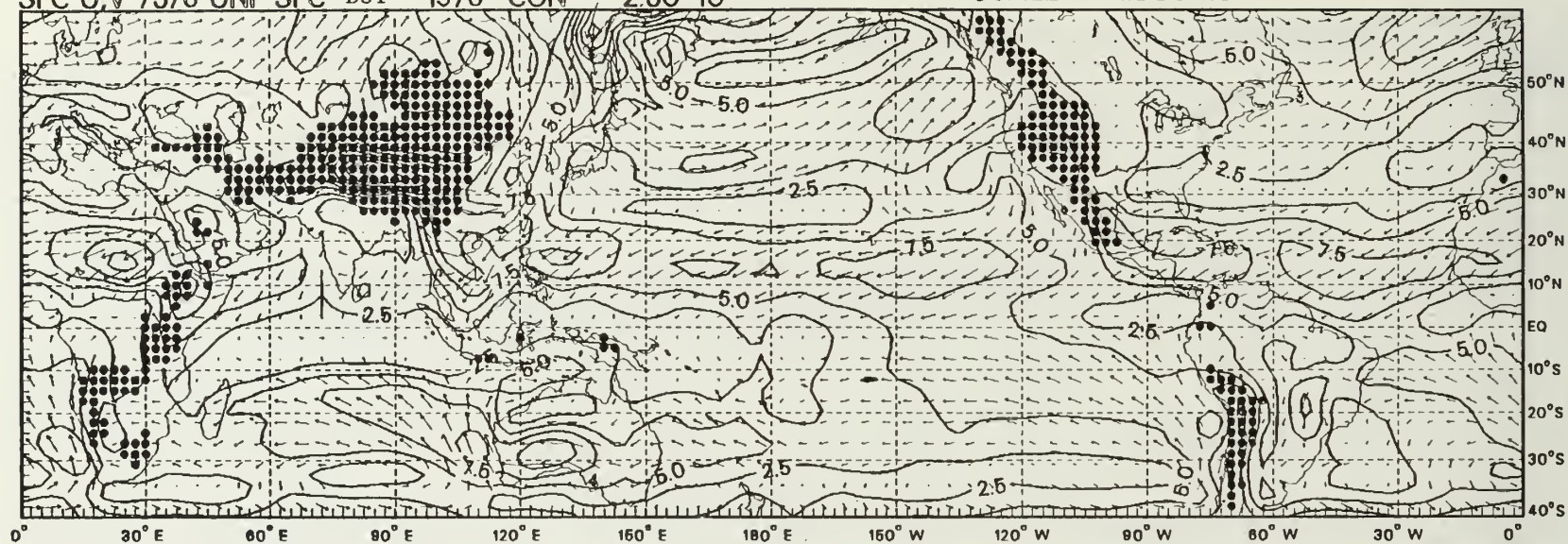
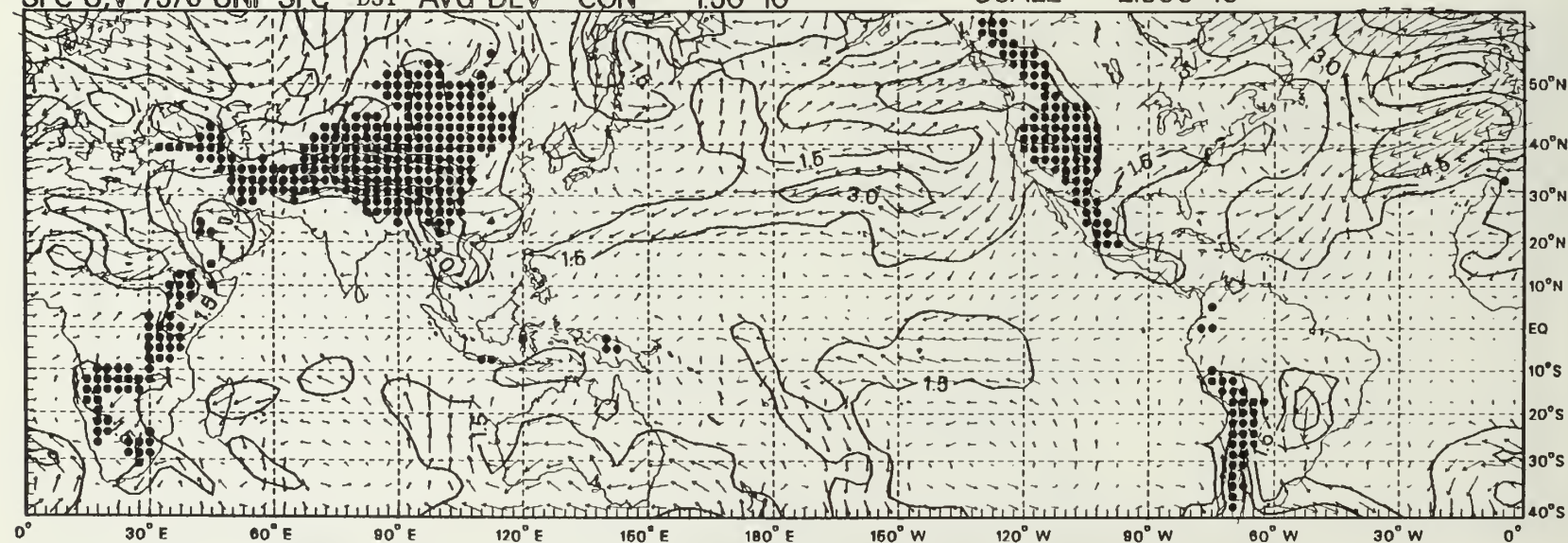


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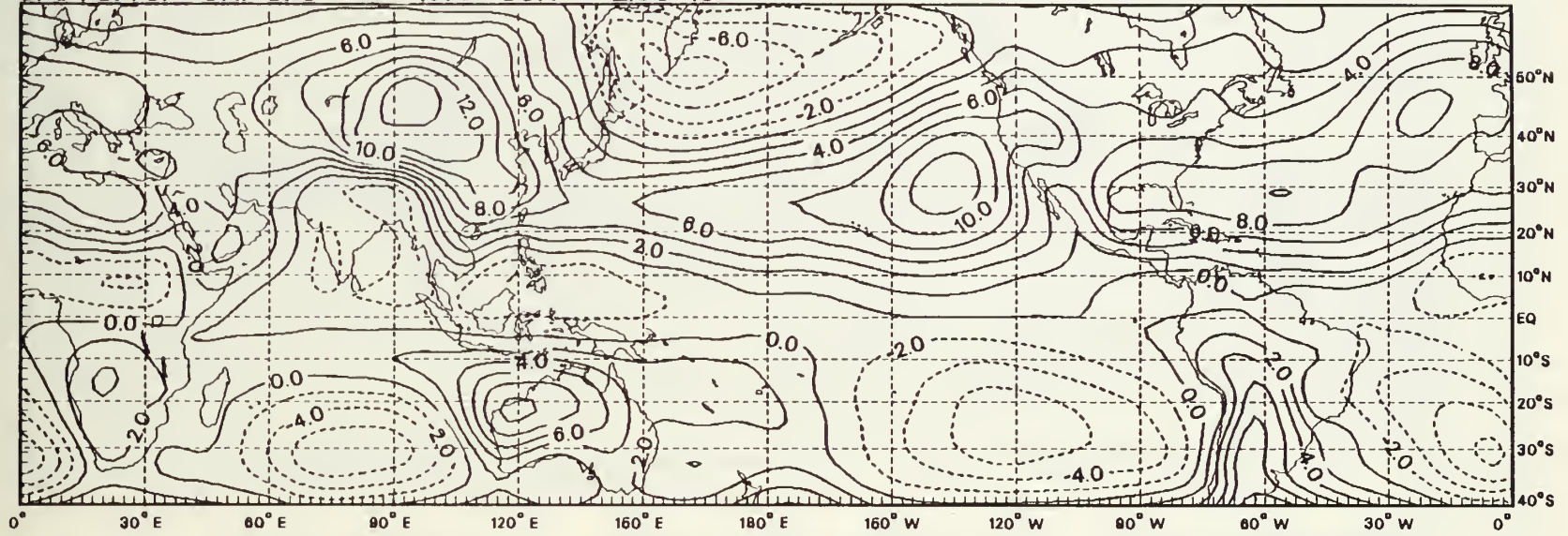


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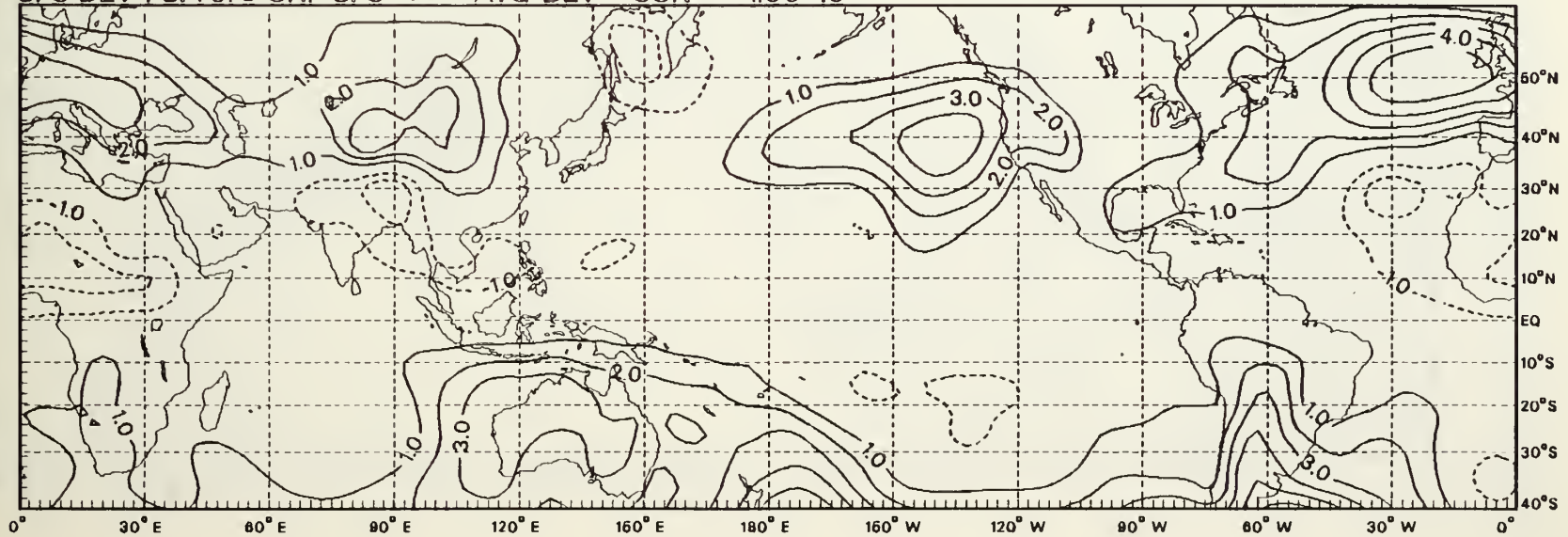
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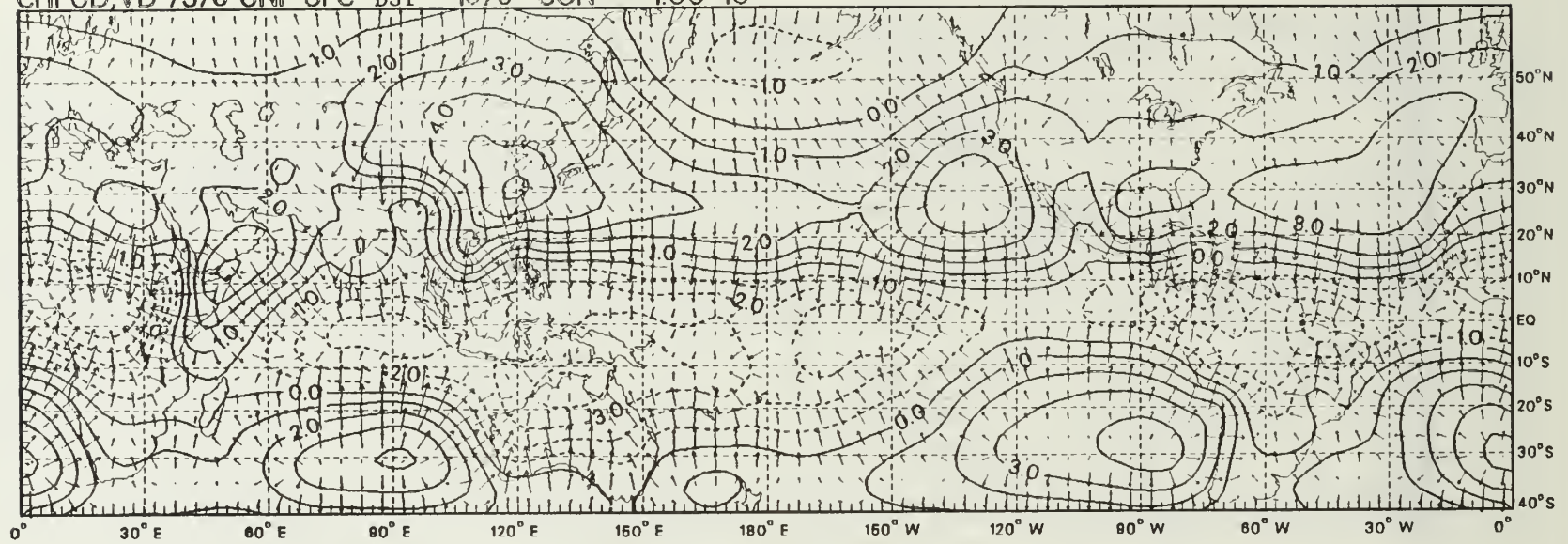
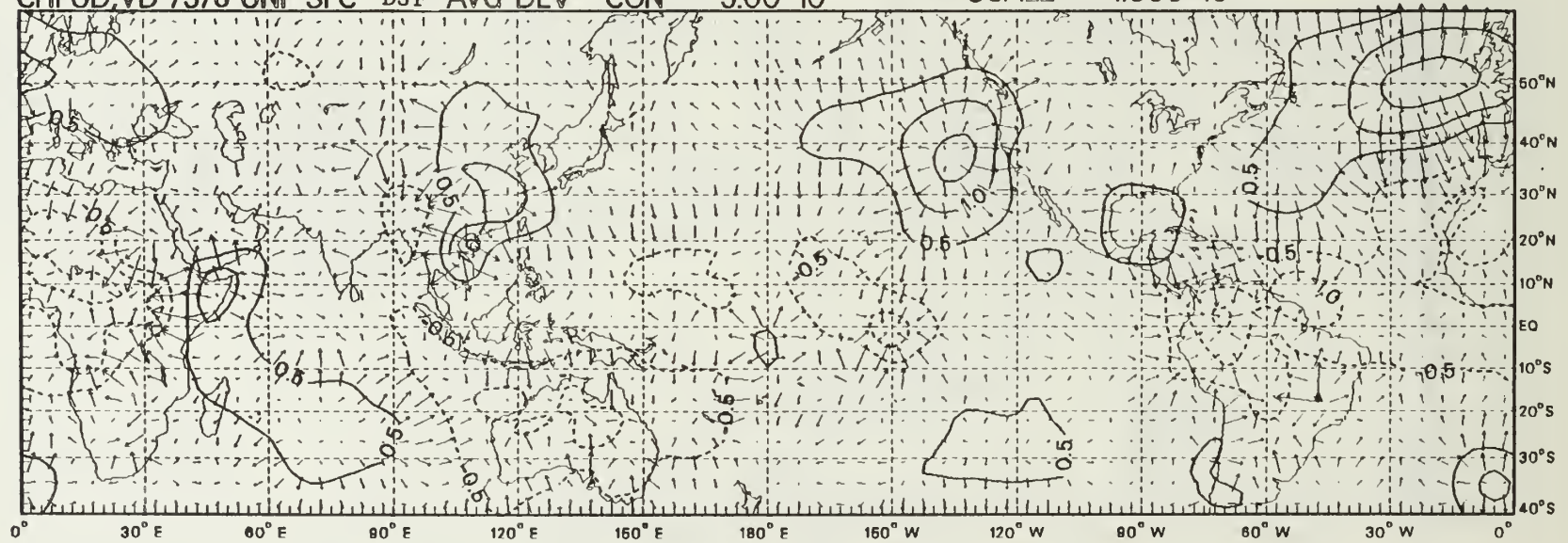


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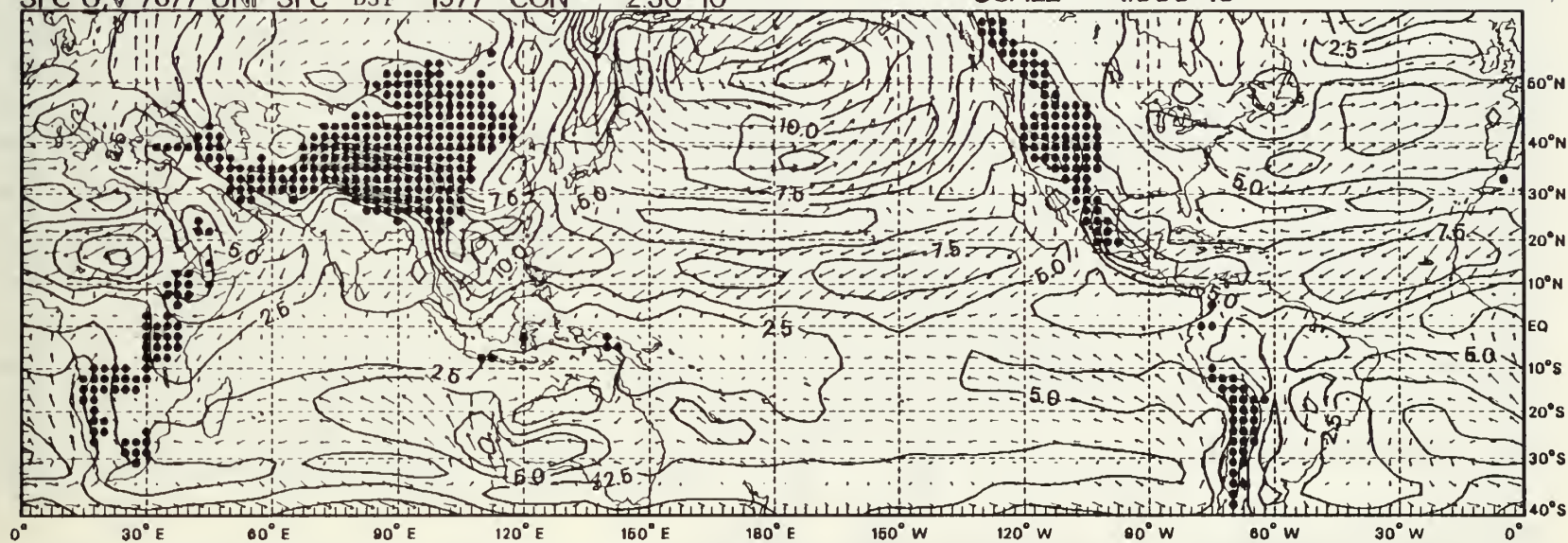
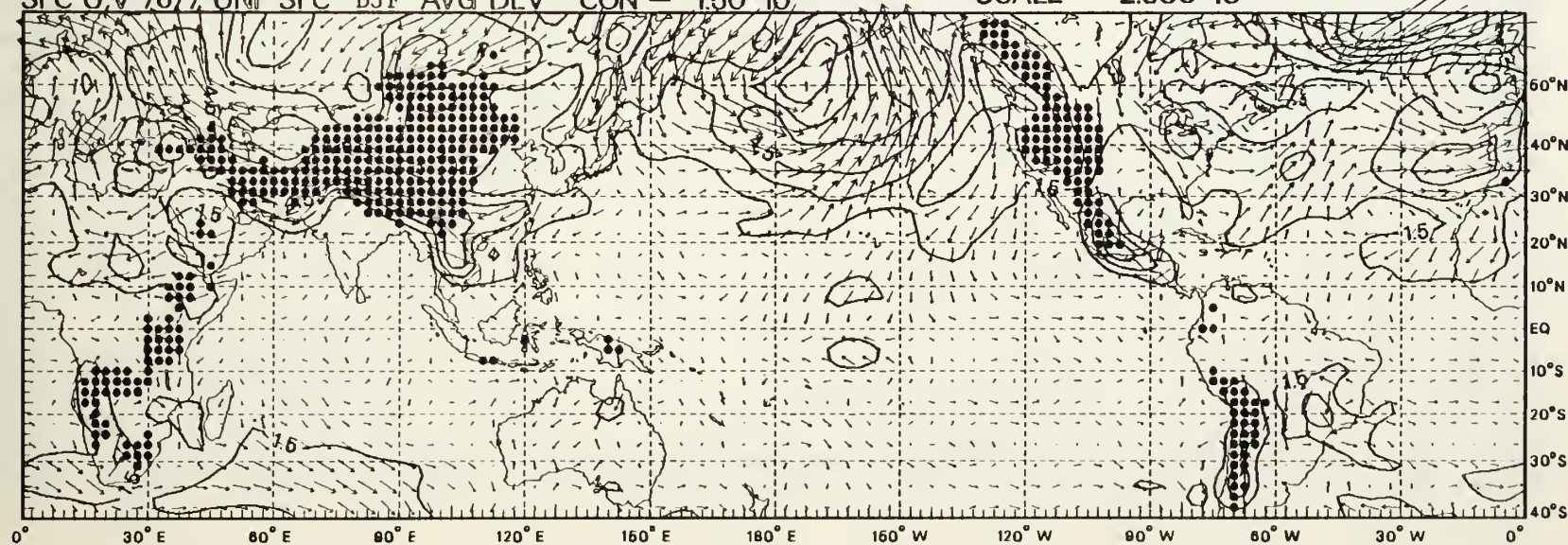


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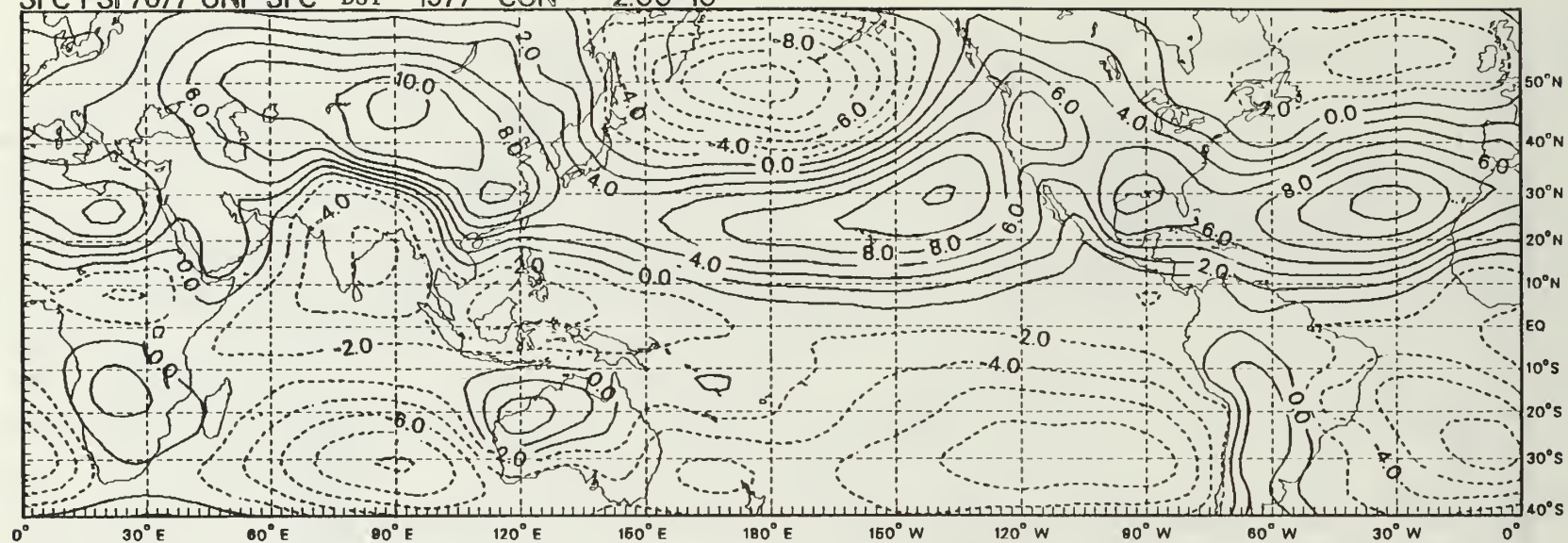


CHI UD,VD 7576 UNF SFC DJF 1976 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$  —CHI UD,VD 7576 UNF SFC DJF AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$  —

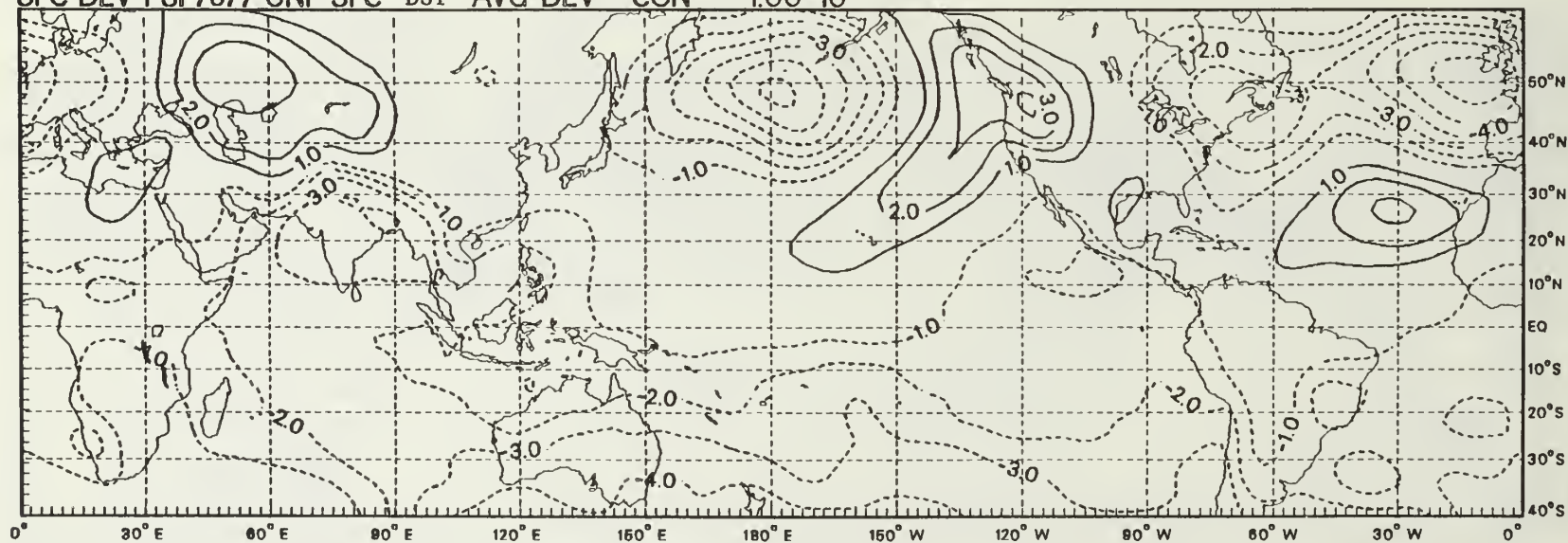


SFC U.V 7677 UNF SFC DJF 1977 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U.V 7677 UNF SFC DJF AVG DEV CON =  $1.50 \times 10^0$ SCALE =  $2.500 \times 10^0$  —

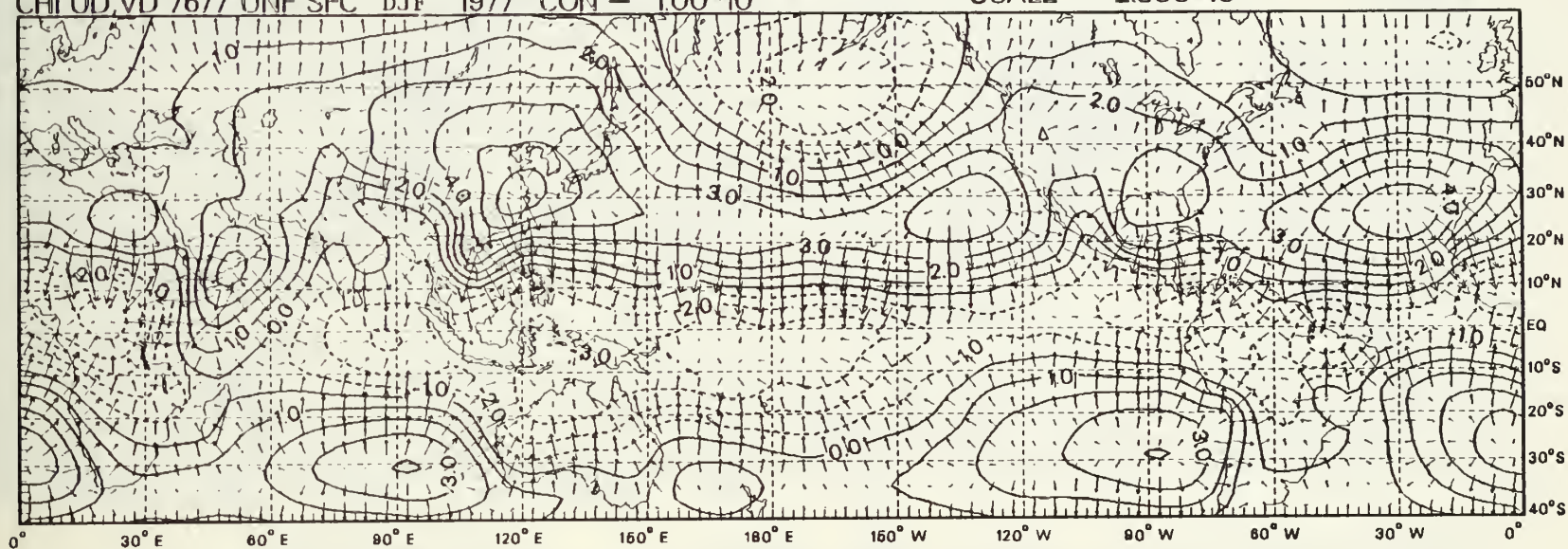
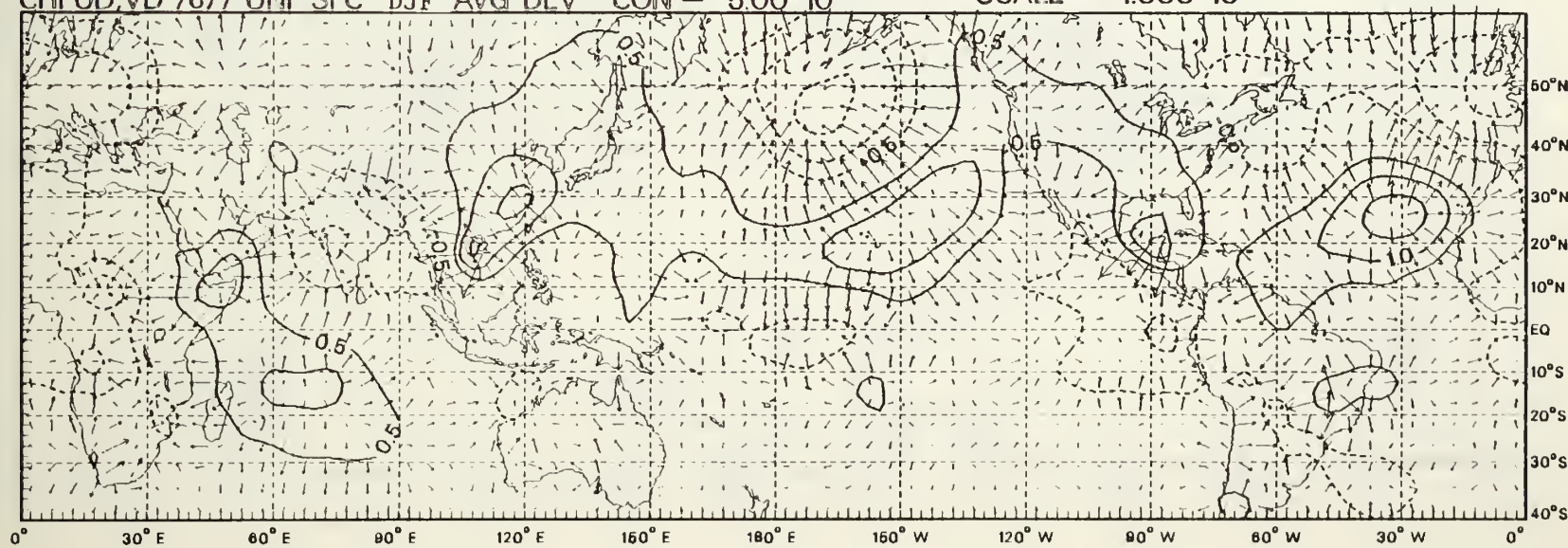
SFC PSI 7677 UNF SFC DJF 1977 CON =  $2.00 \times 10^0$

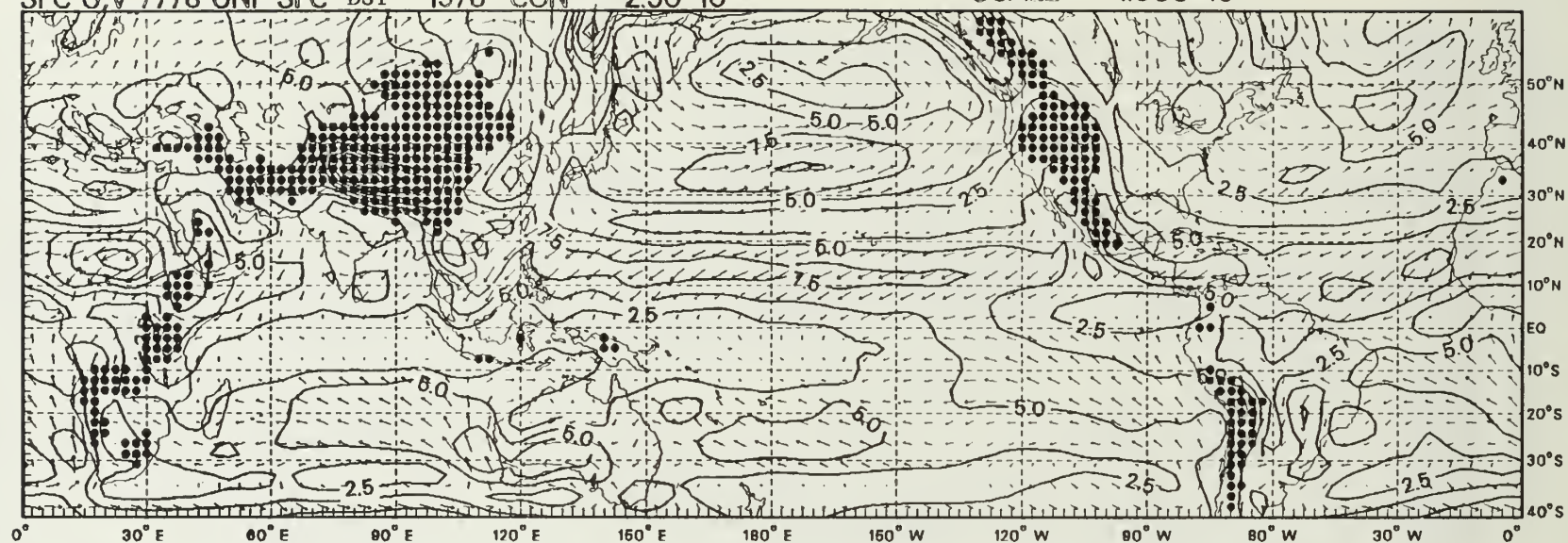
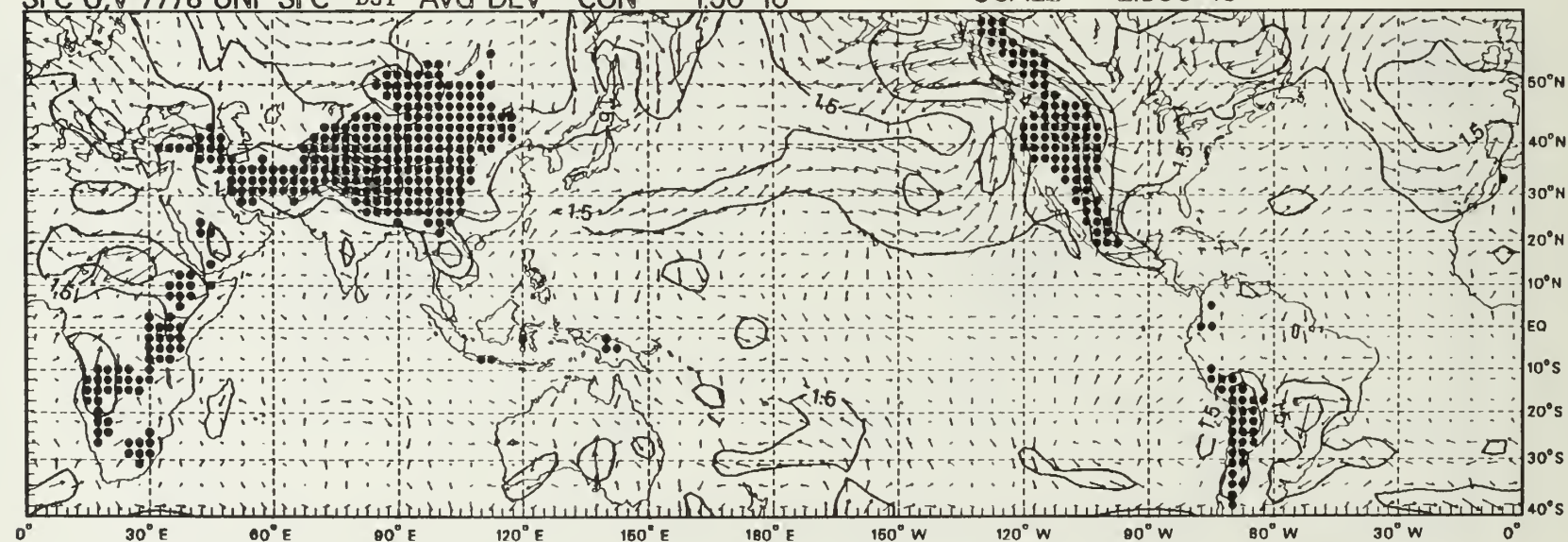


SFC DEV PSI 7677 UNF SFC DJF AVG DEV CON =  $1.00 \times 10^0$

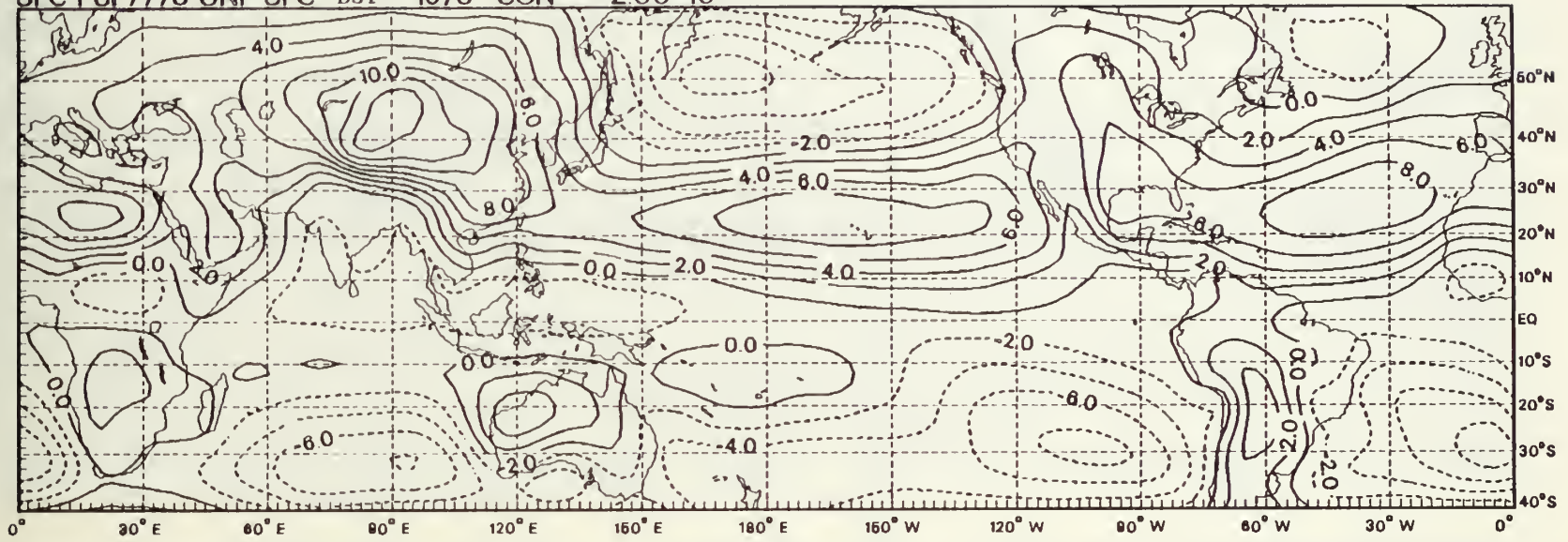
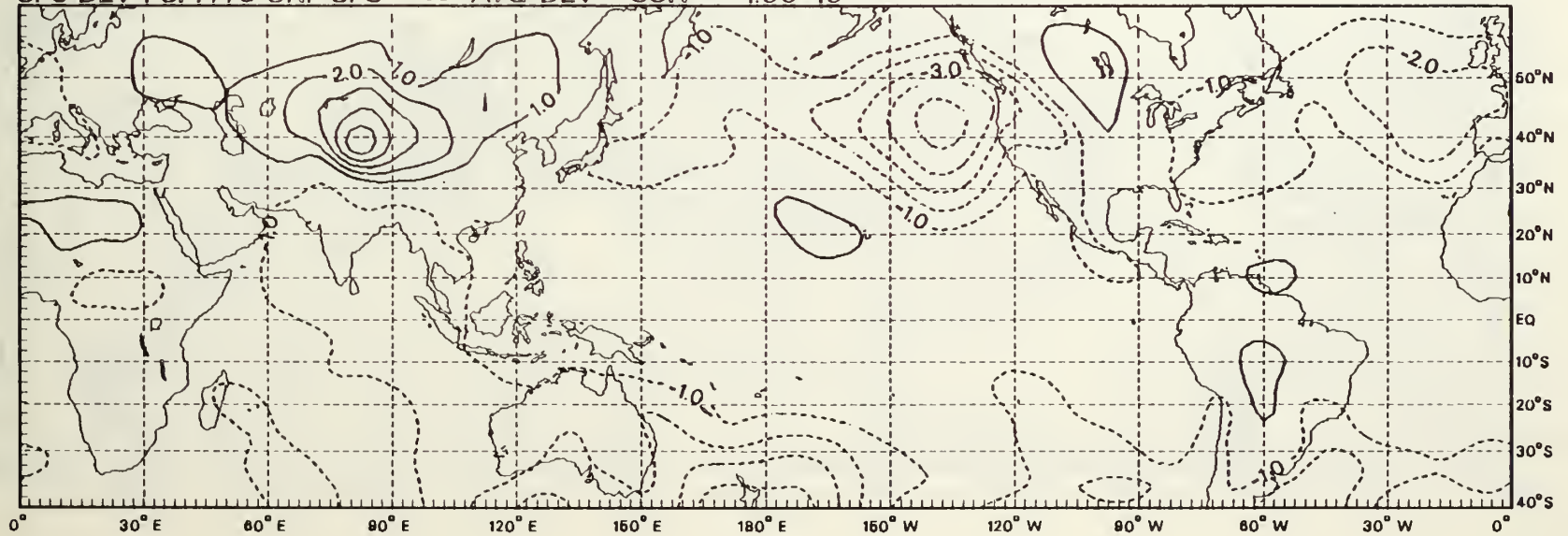


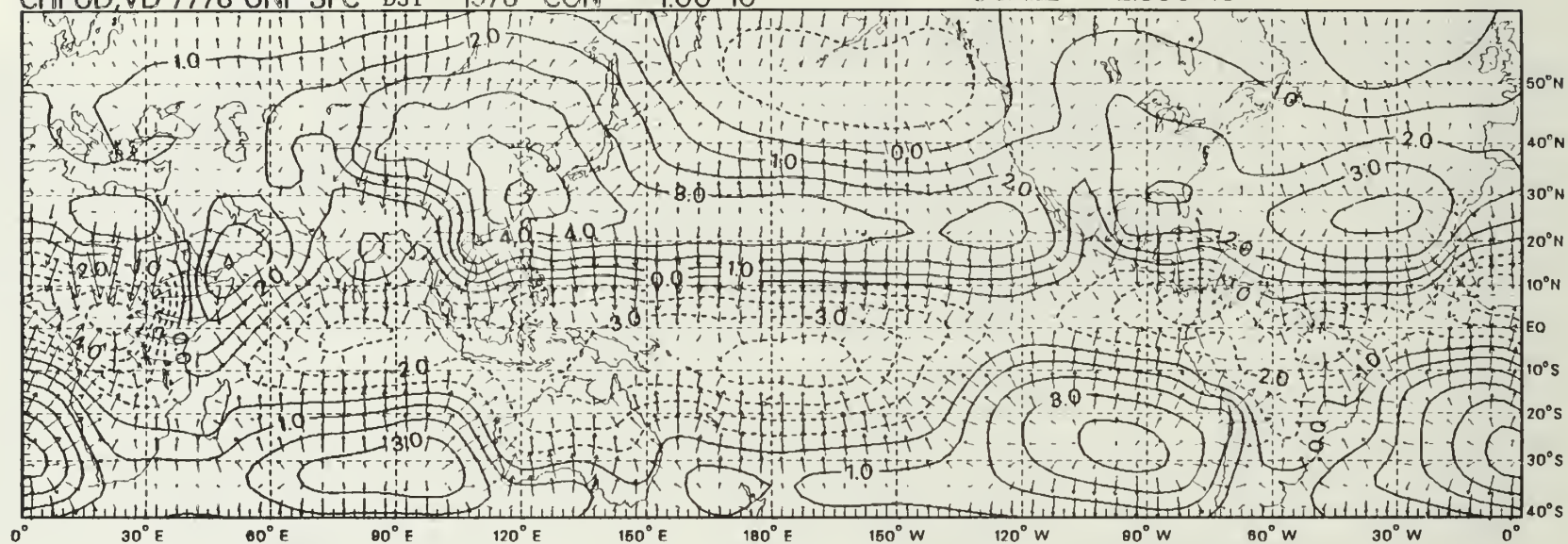
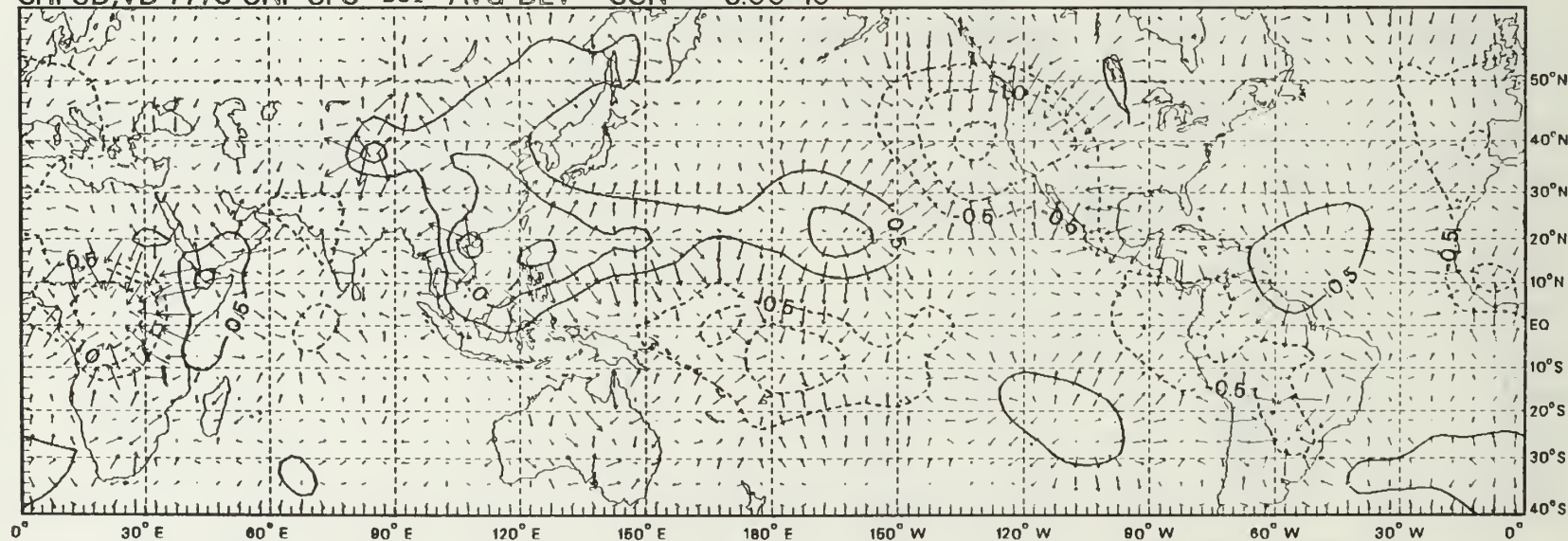


CHI UD.VD 7677 UNF SFC DJF 1977 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$  —CHI UD.VD 7677 UNF SFC DJF AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$  —

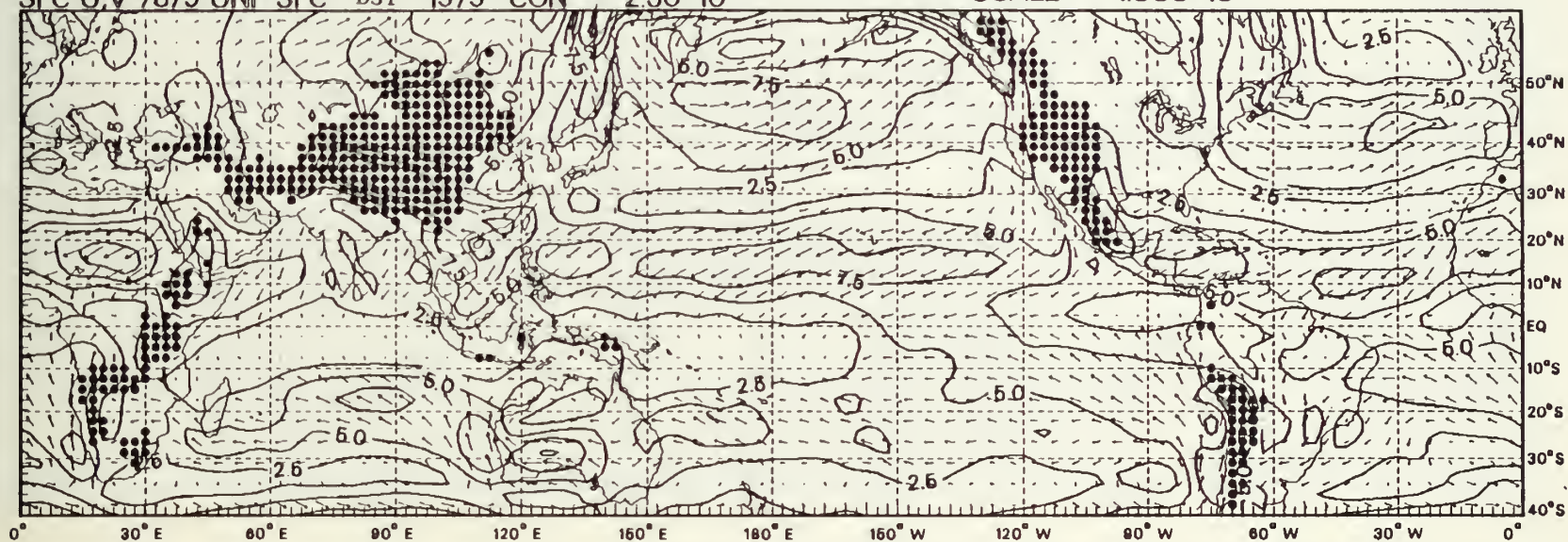
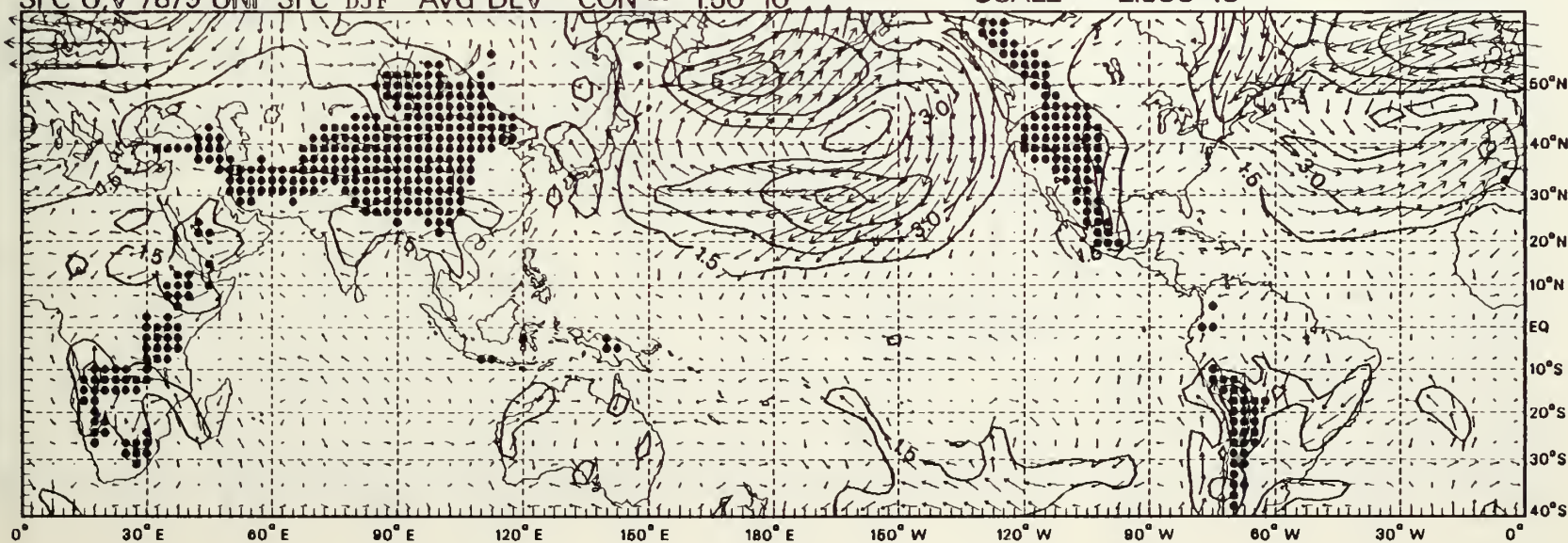
SFC U.V 7778 UNF SFC DJF 1978 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U.V 7778 UNF SFC DJF AVG DEV CON =  $1.50 \times 10^0$ SCALE =  $2.500 \times 10^0$  —



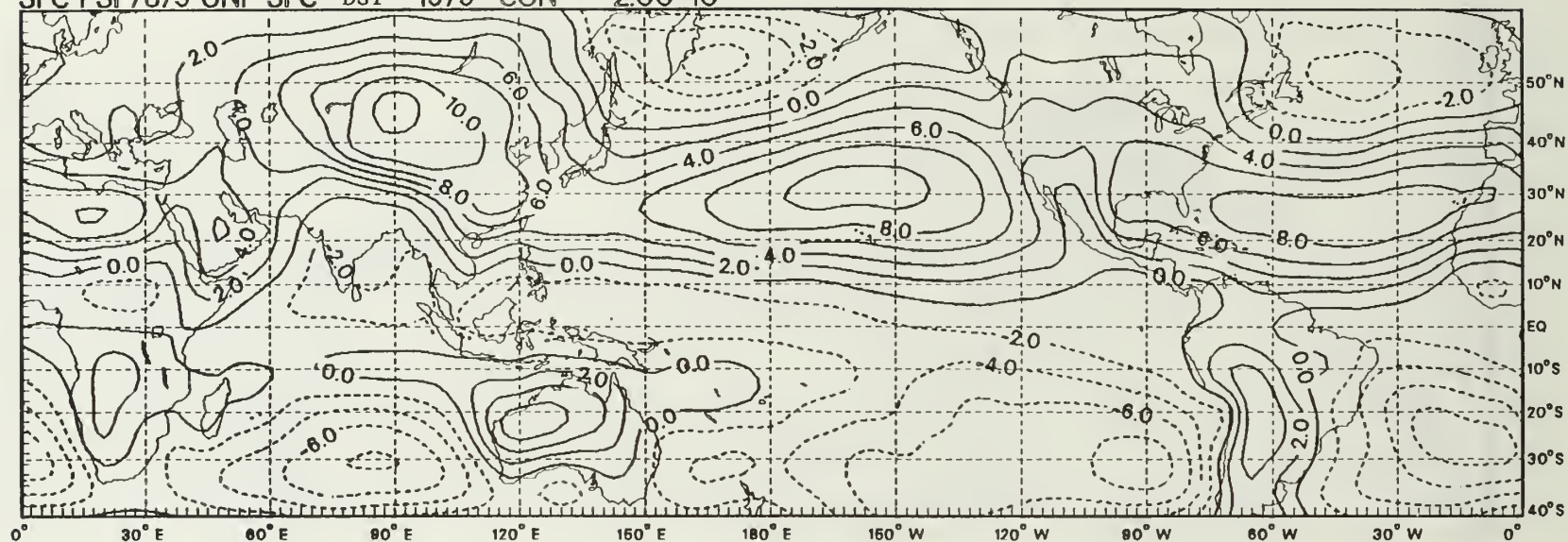
SFC PSI 7778 UNF SFC DJF 1978 CON =  $2.00 \times 10^0$ SFC DEV PSI 7778 UNF SFC DJF AVG DEV CON =  $1.00 \times 10^0$ 

CHI UD,VD 7778 UNF SFC DJF 1978 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$  —CHI UD,VD 7778 UNF SFC DJF AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$  —

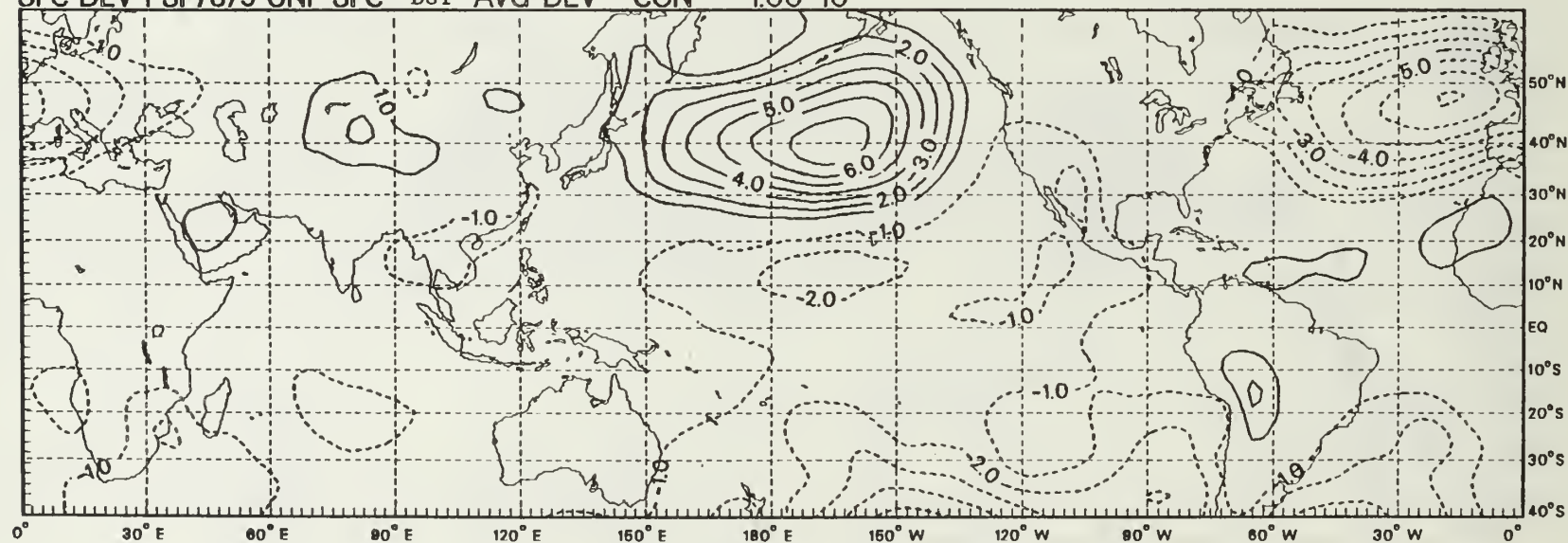


SFC U,V 7879 UNF SFC DJF 1979 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U,V 7879 UNF SFC DJF AVG DEV CON =  $1.50 \times 10^0$ SCALE =  $2.500 \times 10^0$  —

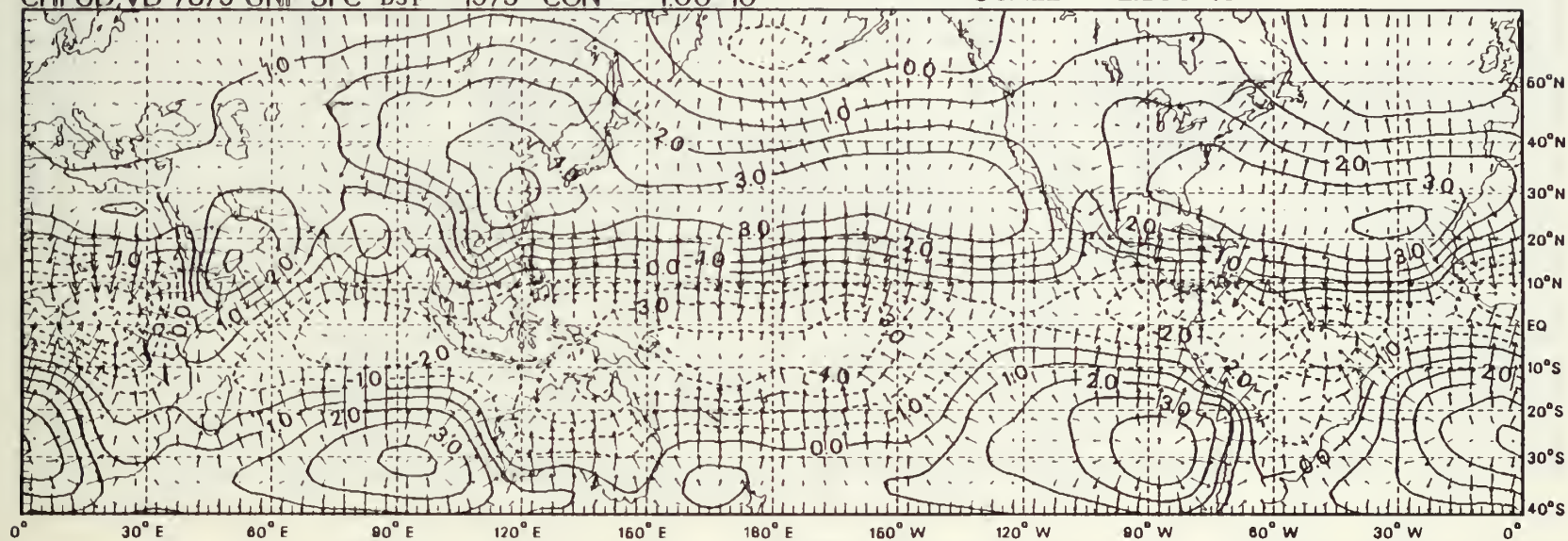
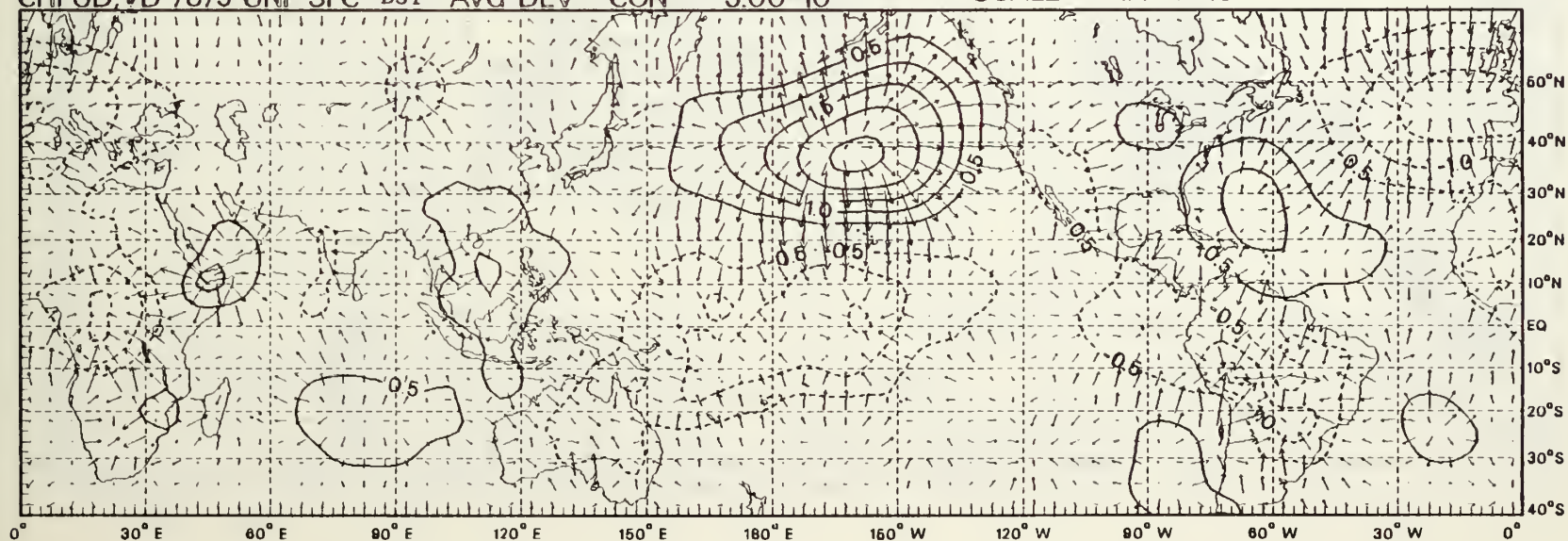
SFC PSI 7879 UNF SFC DJF 1979 CON =  $2.00 \times 10^0$



SFC DEV PSI 7879 UNF SFC DJF AVG DEV CON =  $1.00 \times 10^0$



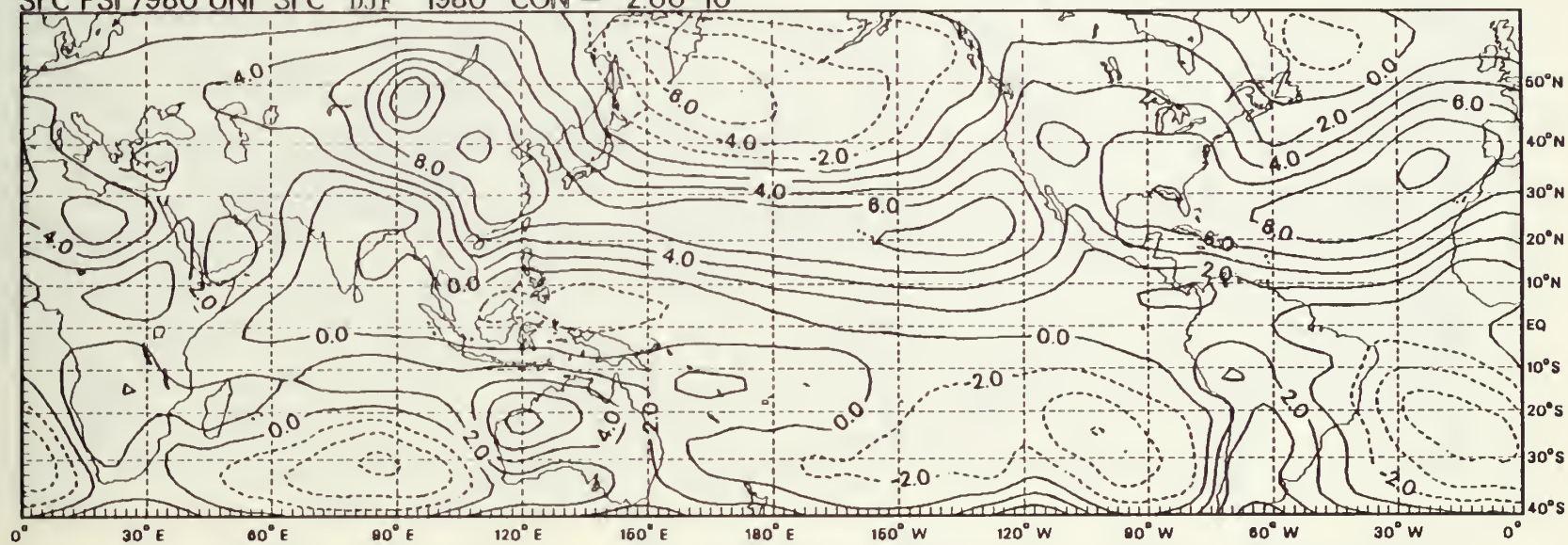


CHI UD.VD 7879 UNF SFC DJF 1979 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$  —CHI UD.VD 7879 UNF SFC DJF AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$  —

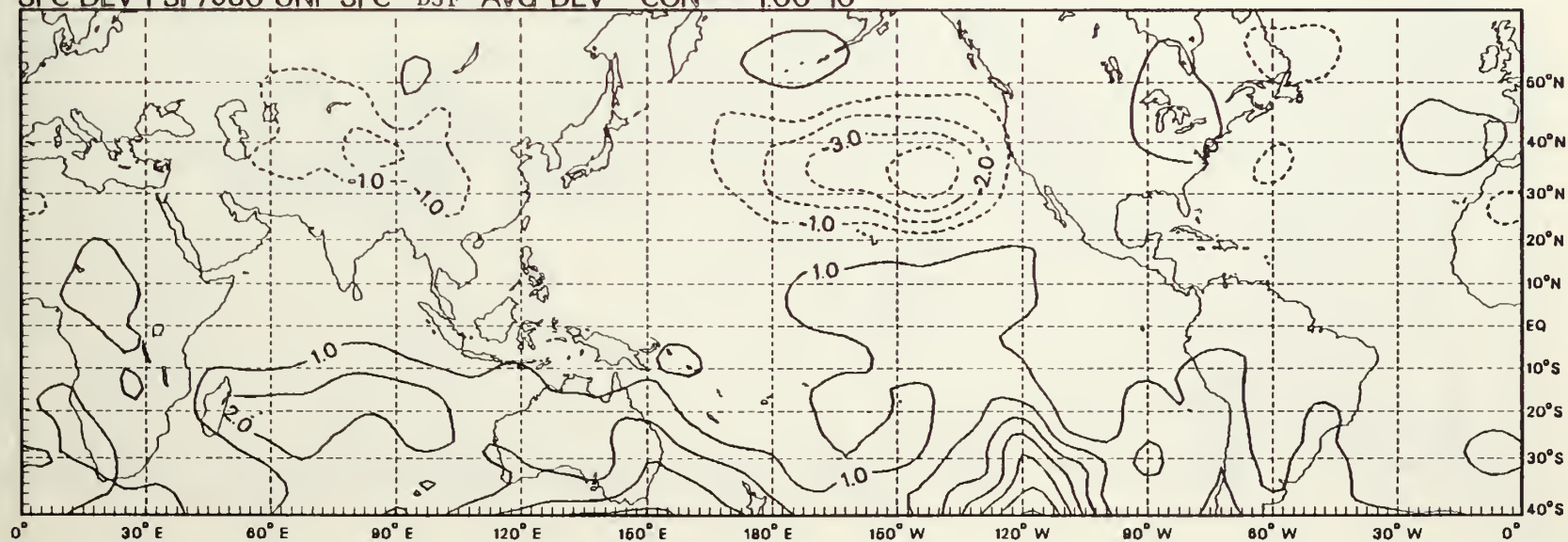




SFC PSI 7980 UNF SFC DJF 1980 CON =  $2.00 \times 10^0$

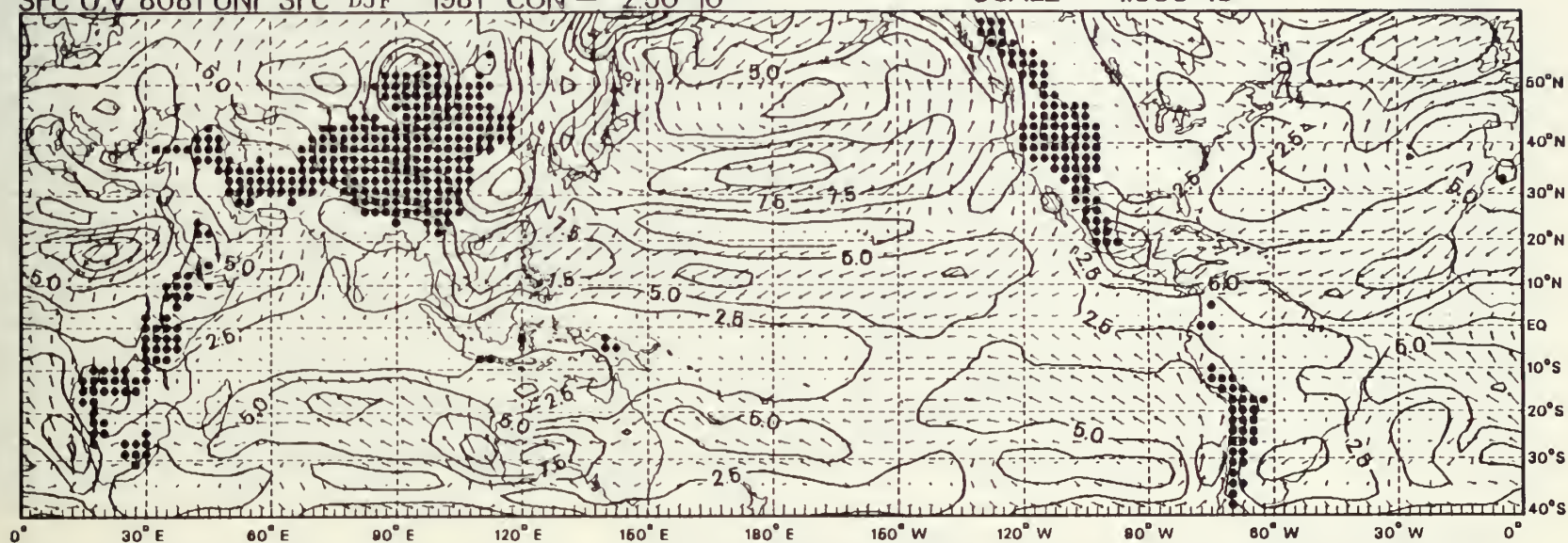
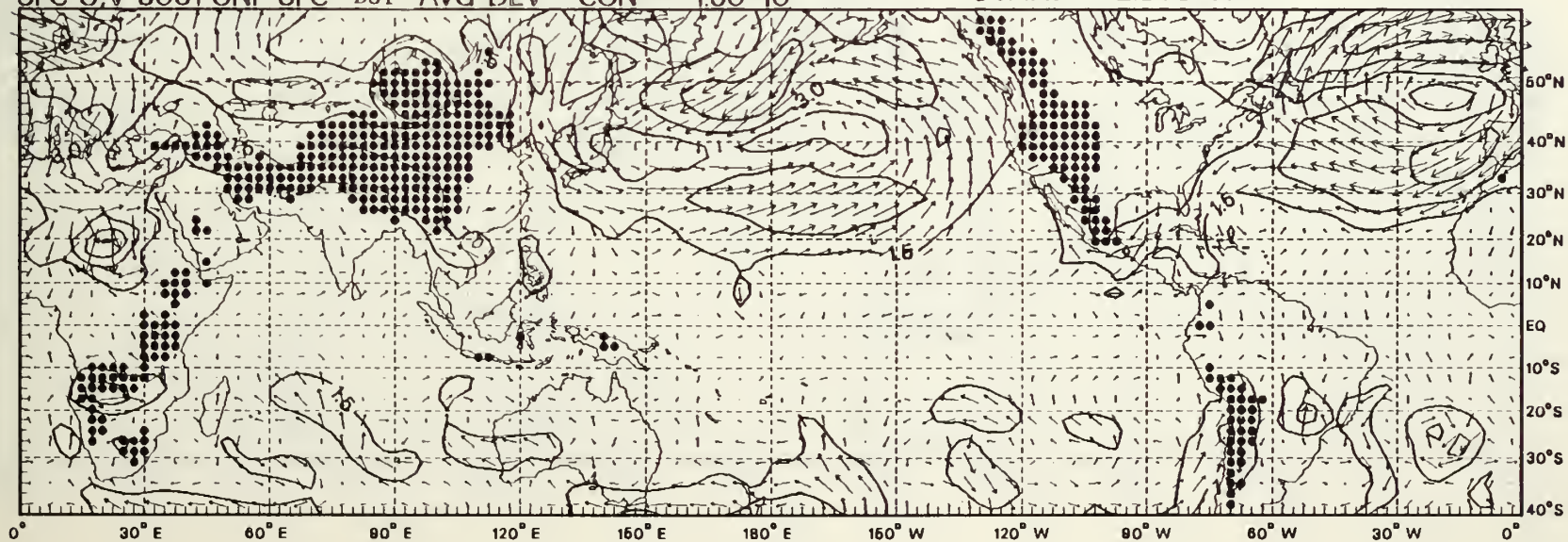


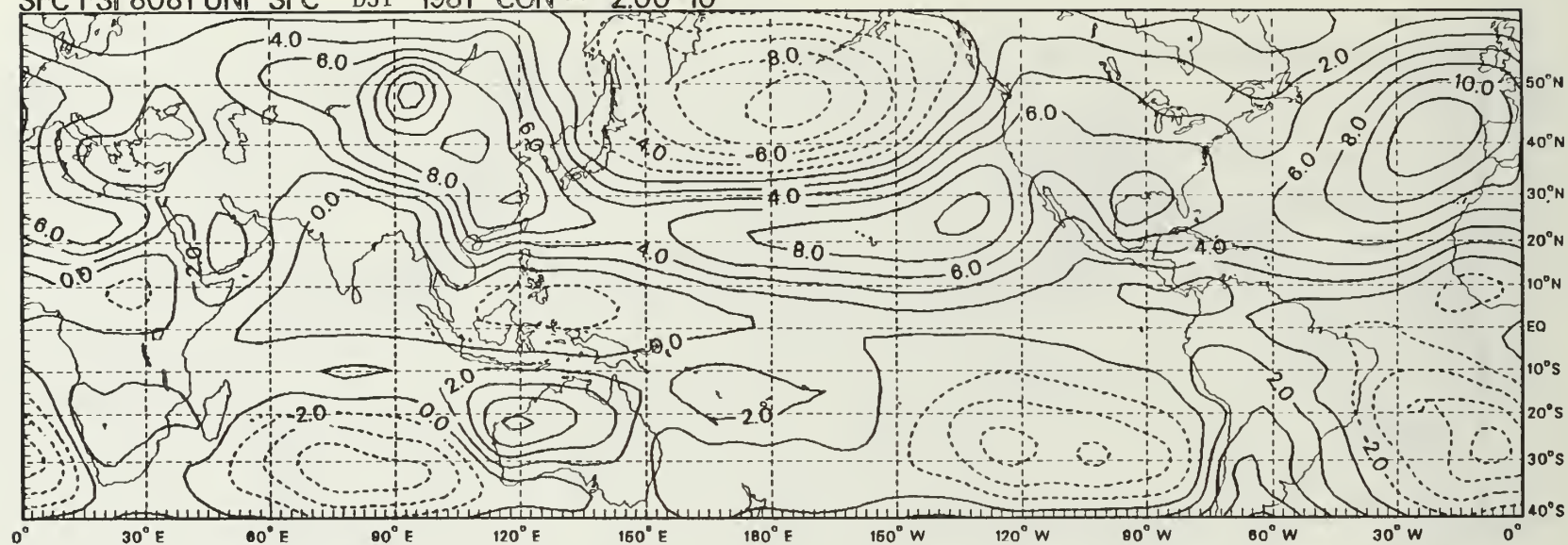
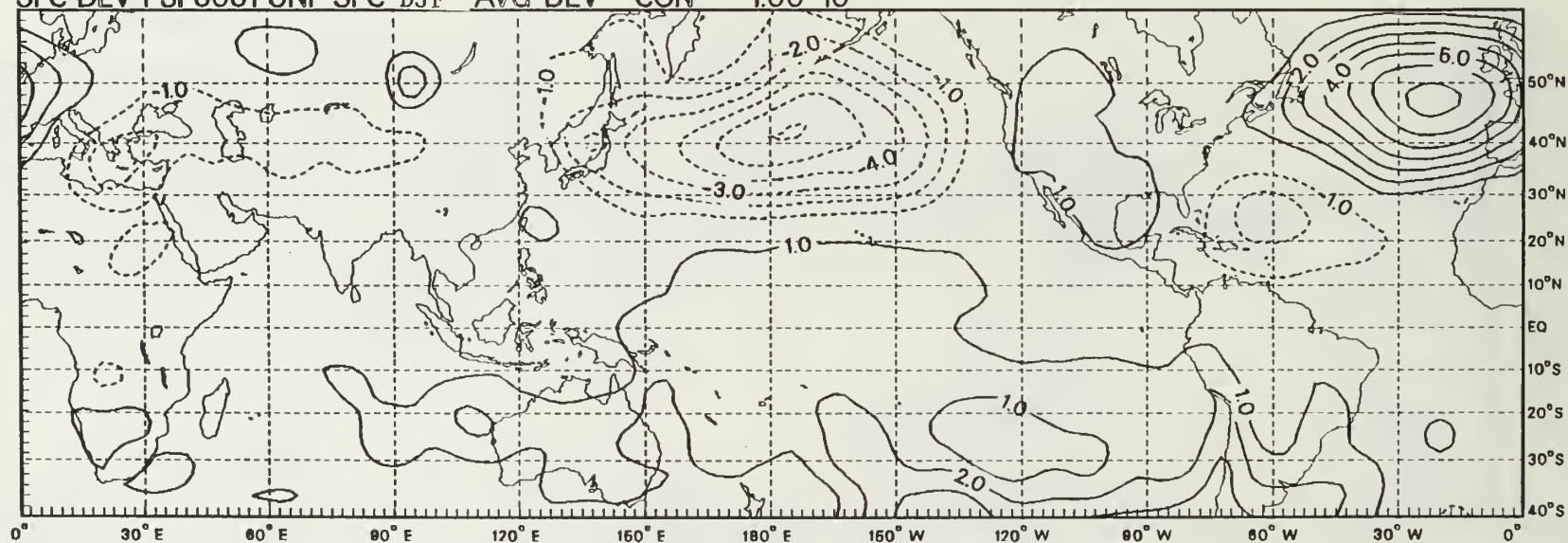
SFC DEV PSI 7980 UNF SFC DJF AVG DEV CON =  $1.00 \times 10^0$



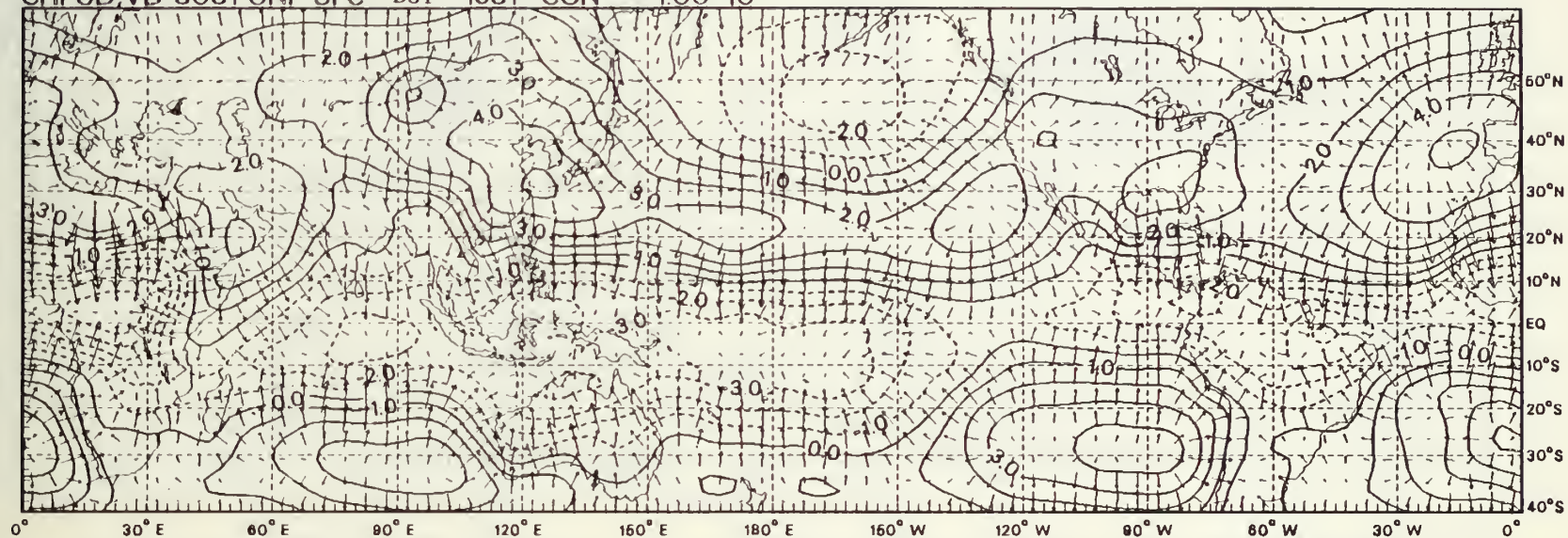
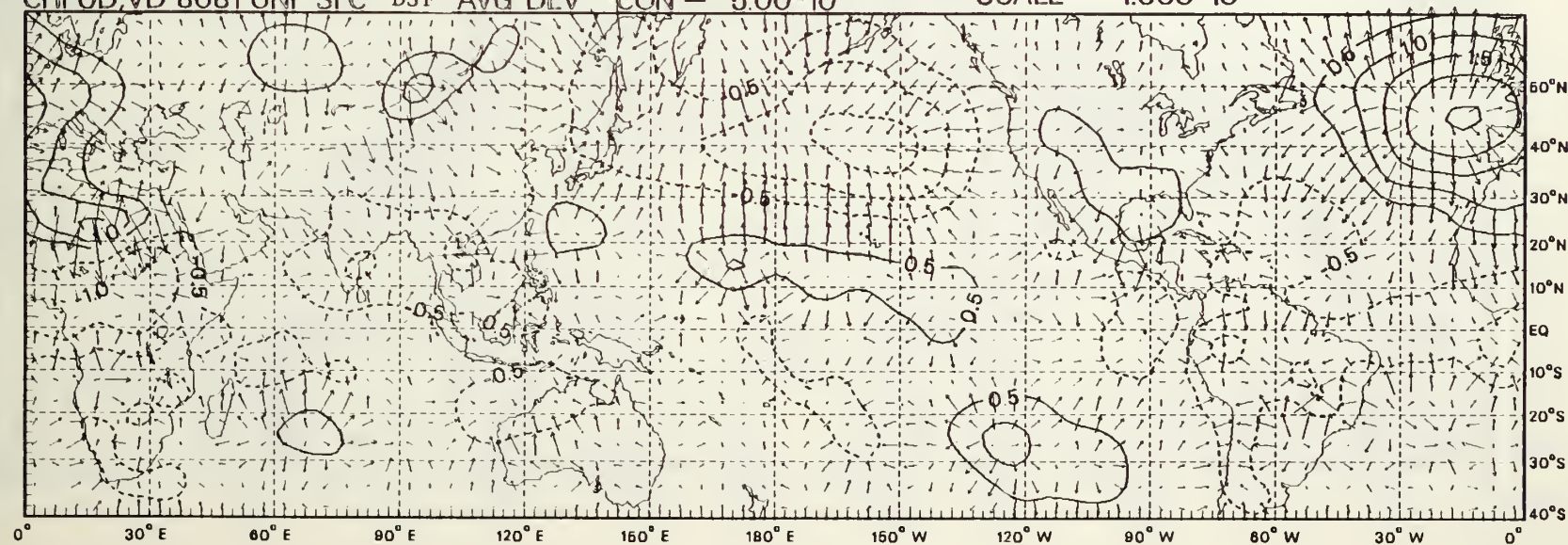




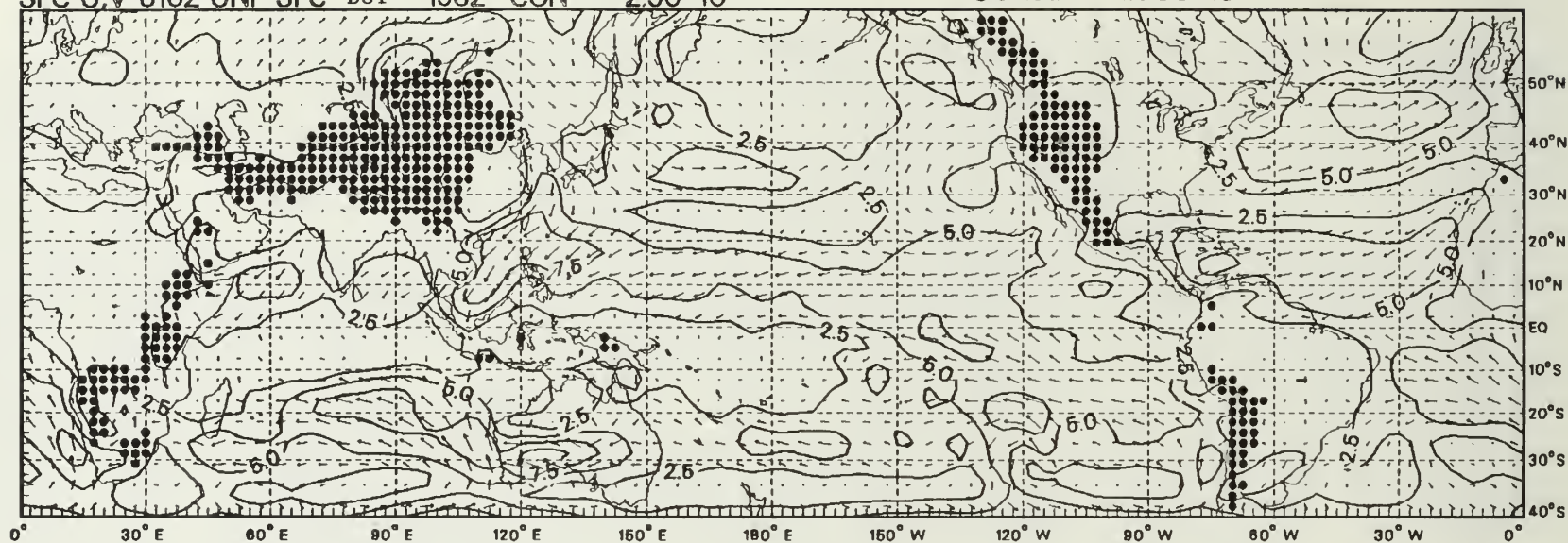
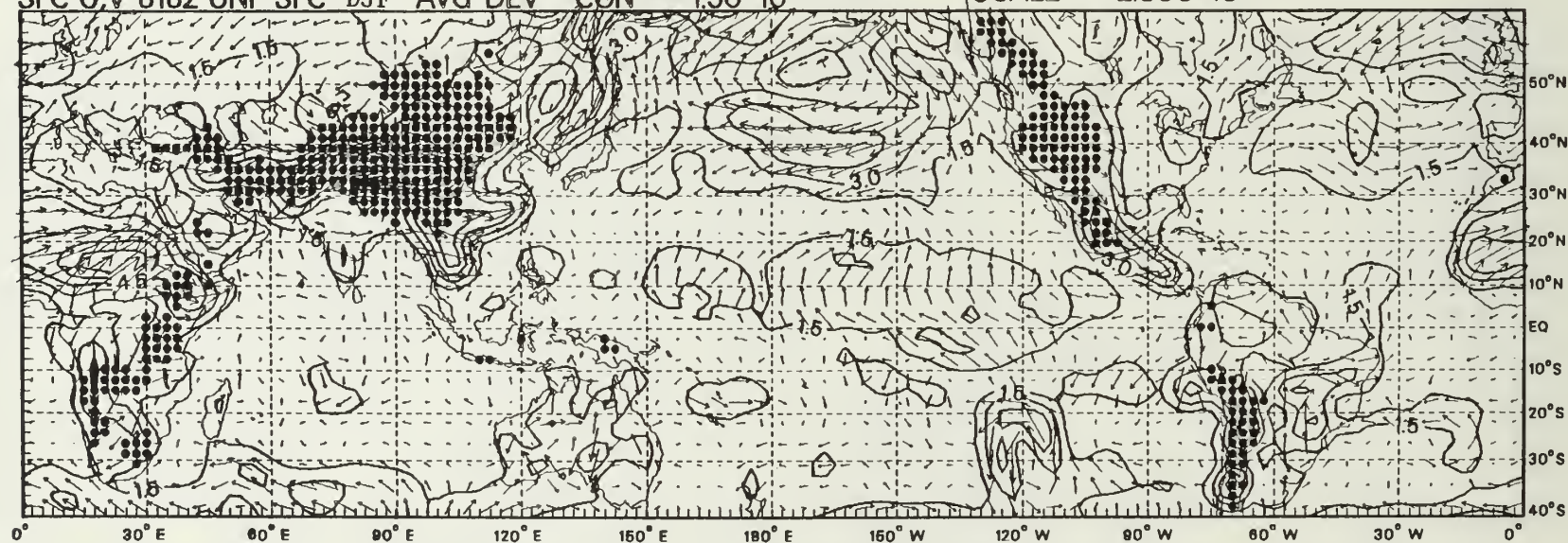
SFC U.V 8081 UNF SFC DJF 1981 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U.V 8081 UNF SFC DJF AVG DEV CON =  $1.50 \times 10^0$ SCALE =  $2.500 \times 10^0$  —

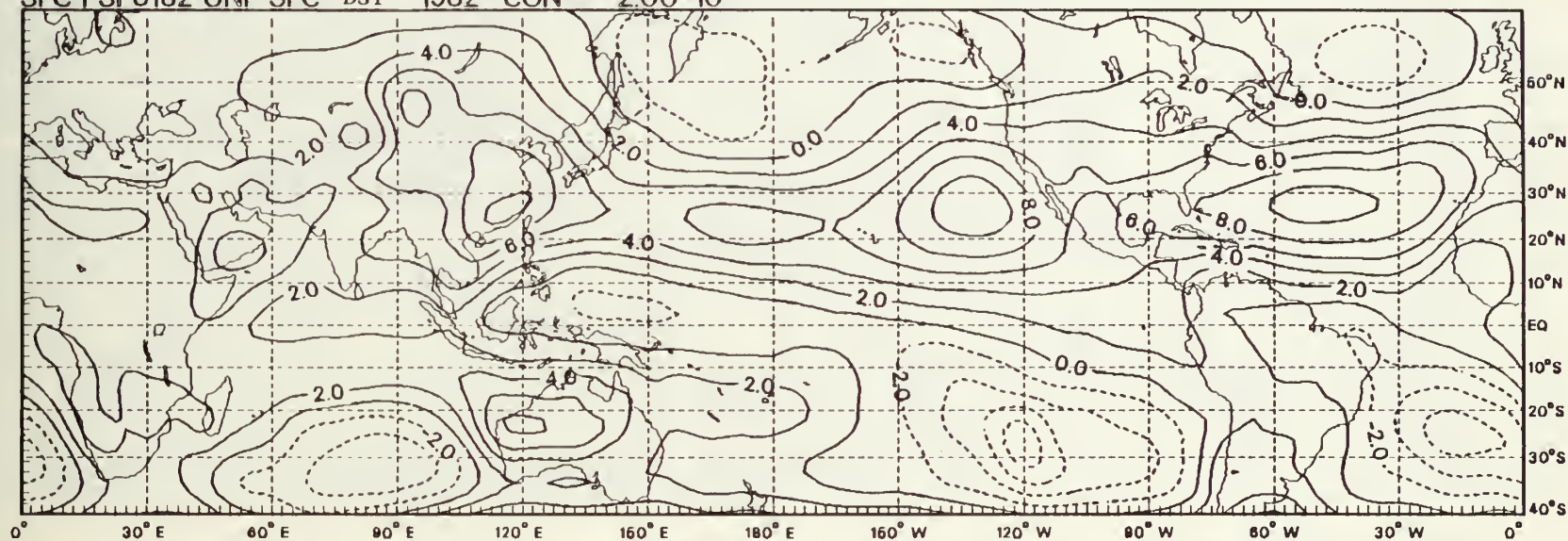
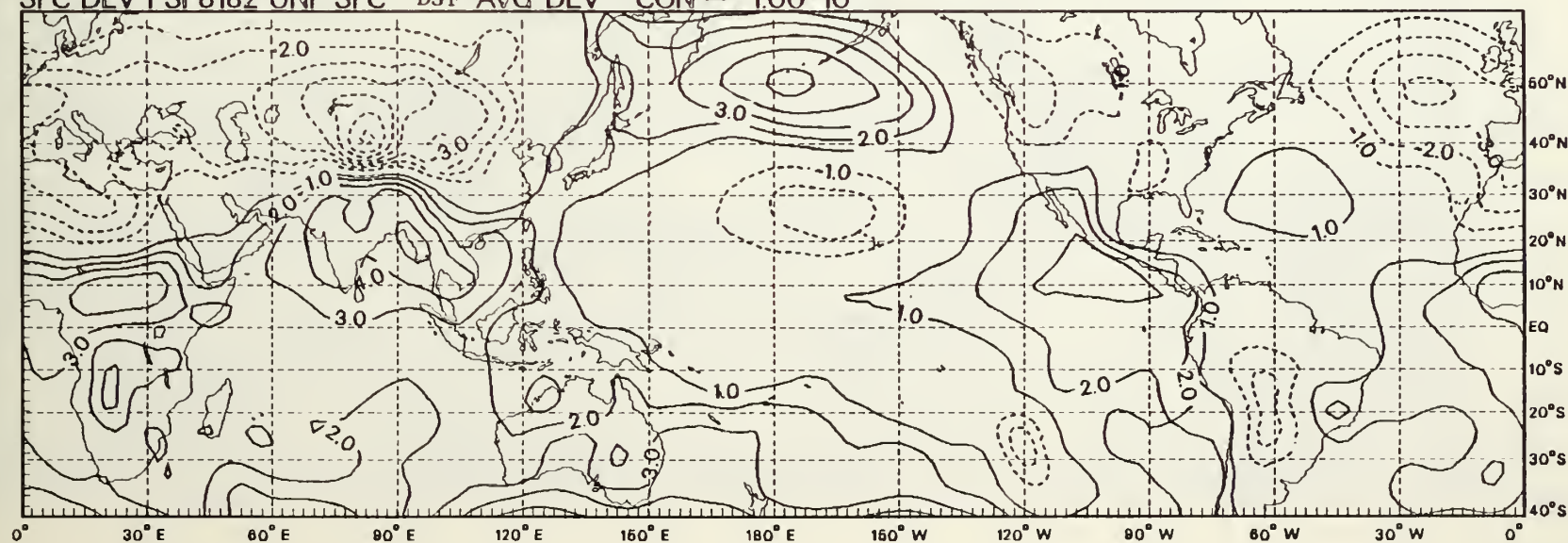
SFC PSI 8081 UNF SFC DJF 1981 CON =  $2.00 \times 10^0$ SFC DEV PSI 8081 UNF SFC DJF AVG DEV CON =  $1.00 \times 10^0$ 



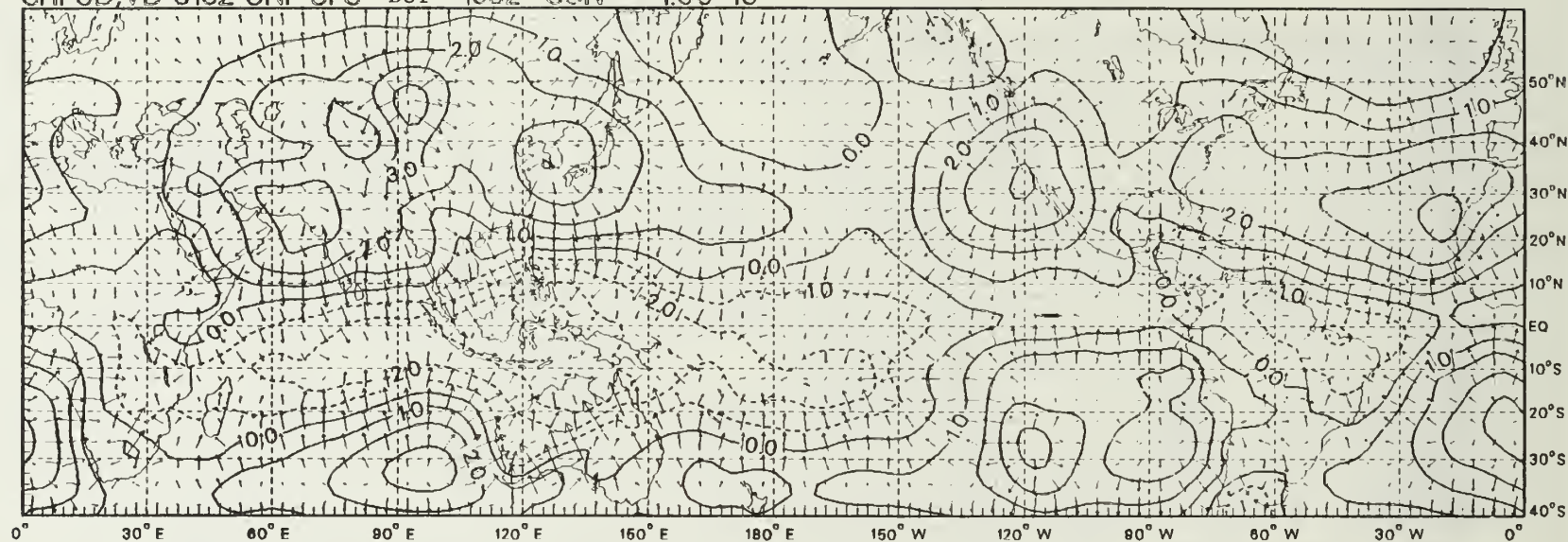
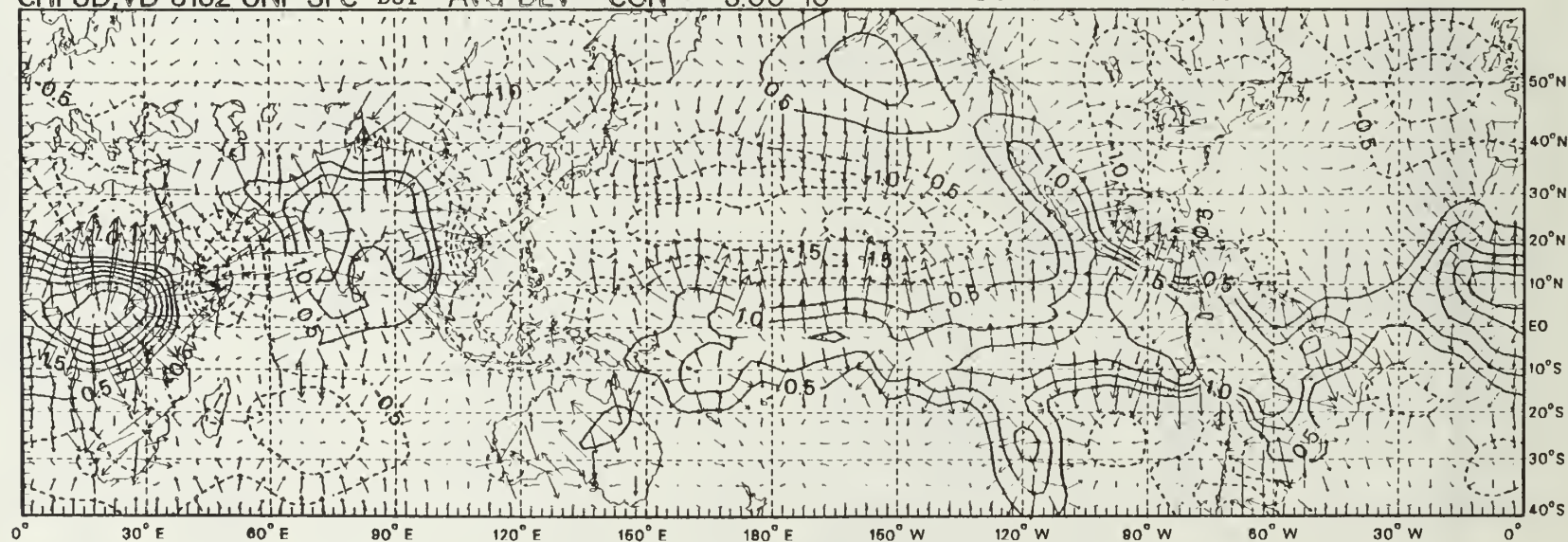
CHI UD,VD 8081 UNF SFC DJF 1981 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$  —CHI UD,VD 8081 UNF SFC DJF AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$  —



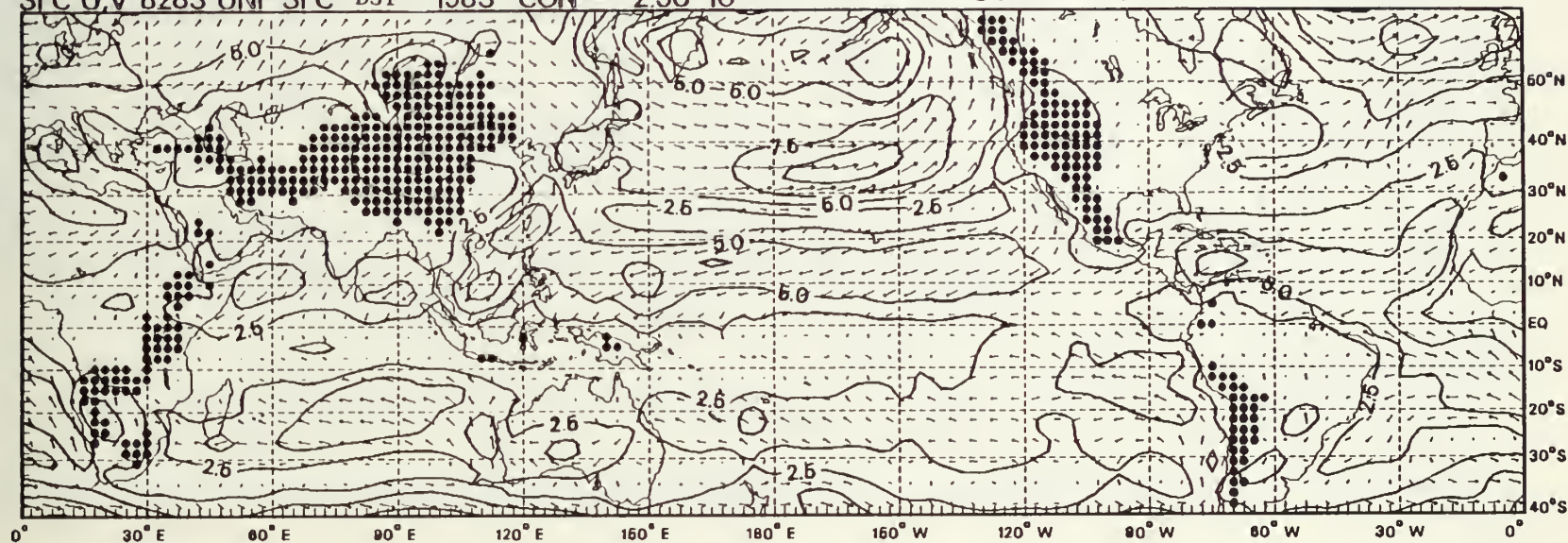
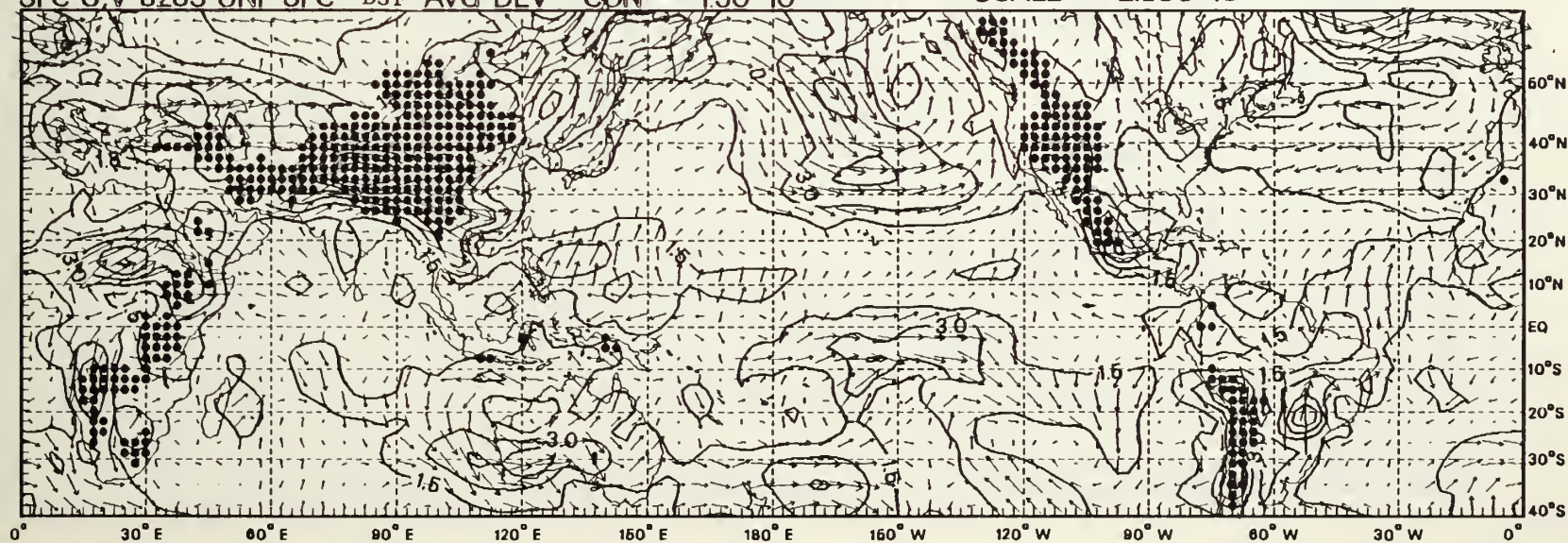
SFC U,V 8182 UNF SFC DJF 1982 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U,V 8182 UNF SFC DJF AVG DEV CON =  $1.50 \times 10^0$ SCALE =  $2.500 \times 10^0$  —

SFC PSI 8182 UNF SFC DJF 1982 CON =  $2.00 \times 10^0$ SFC DEV PSI 8182 UNF SFC DJF AVG DEV CON =  $1.00 \times 10^0$ 

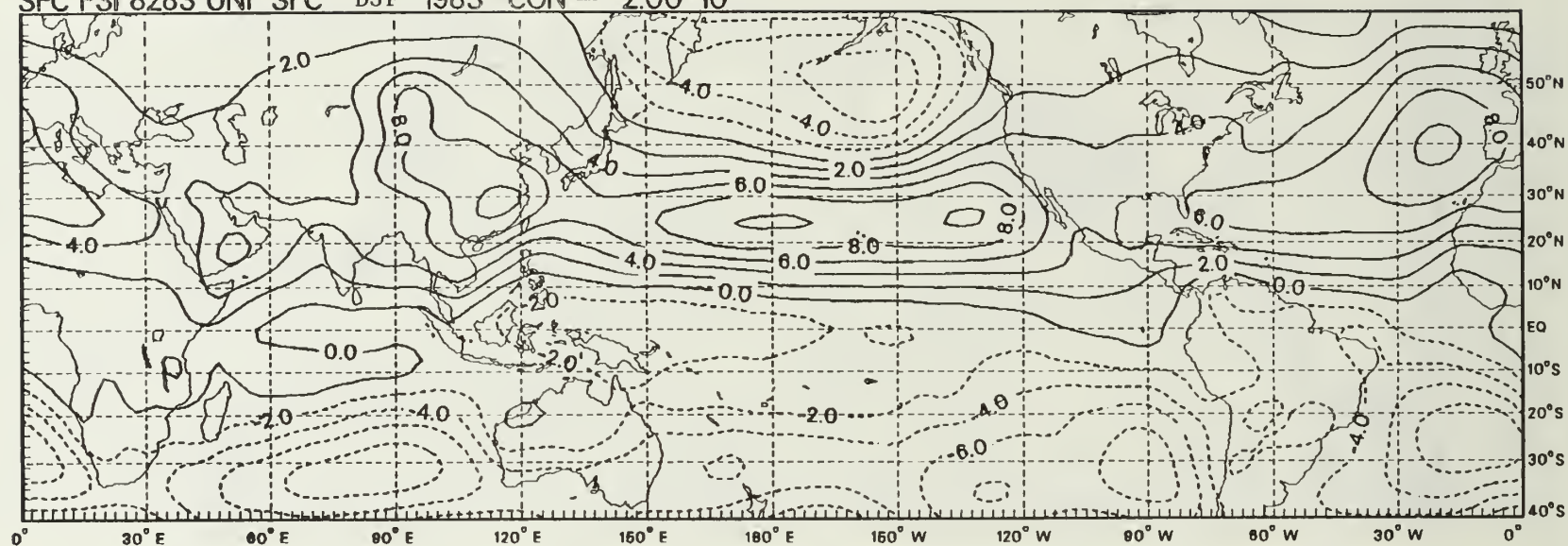


CHI UD,VD 8182 UNF SFC DJF 1982 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$  —CHI UD,VD 8182 UNF SFC DJF AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$  —

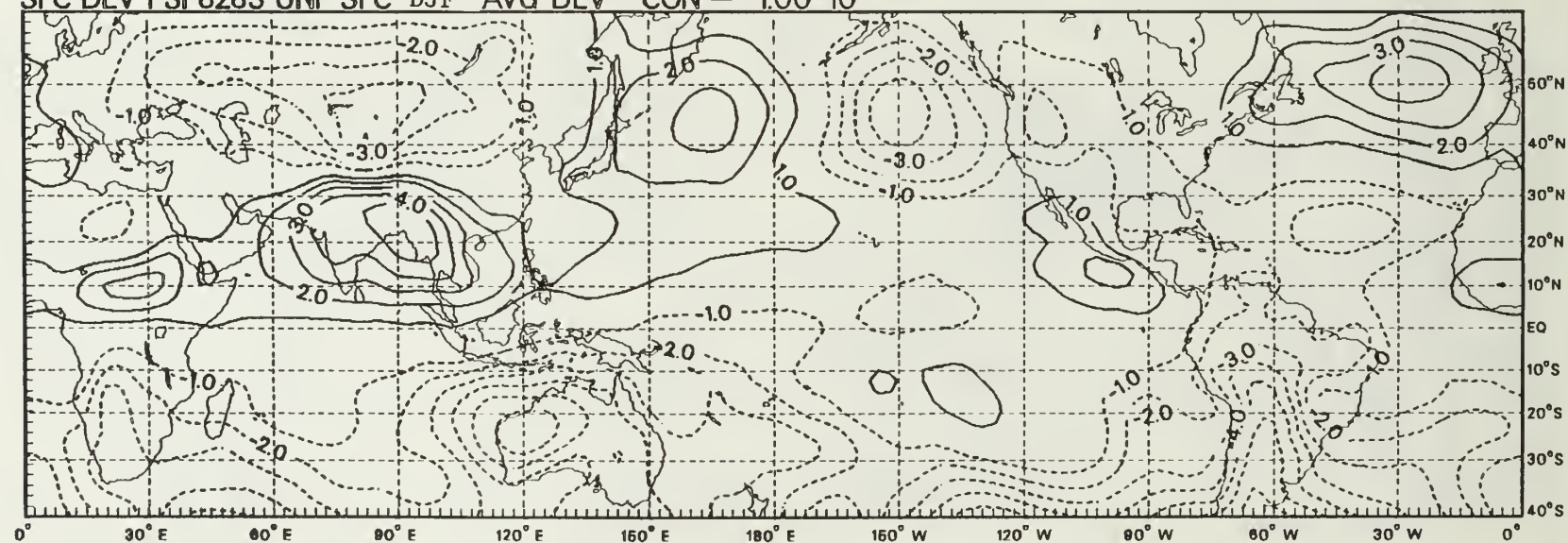


SFC U,V 8283 UNF SFC DJF 1983 CON =  $250 \cdot 10^0$ SCALE =  $1000 \cdot 10^1$  —SFC U,V 8283 UNF SFC DJF AVG DEV CON =  $150 \cdot 10^0$ SCALE =  $2500 \cdot 10^0$  —

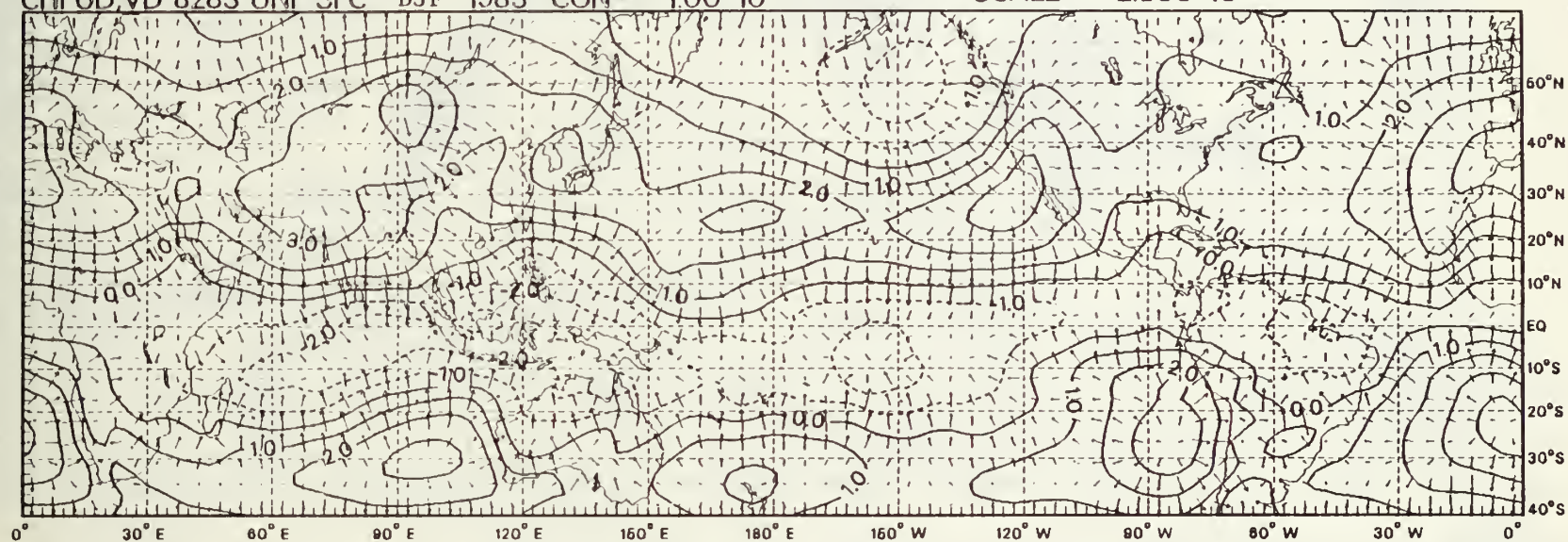
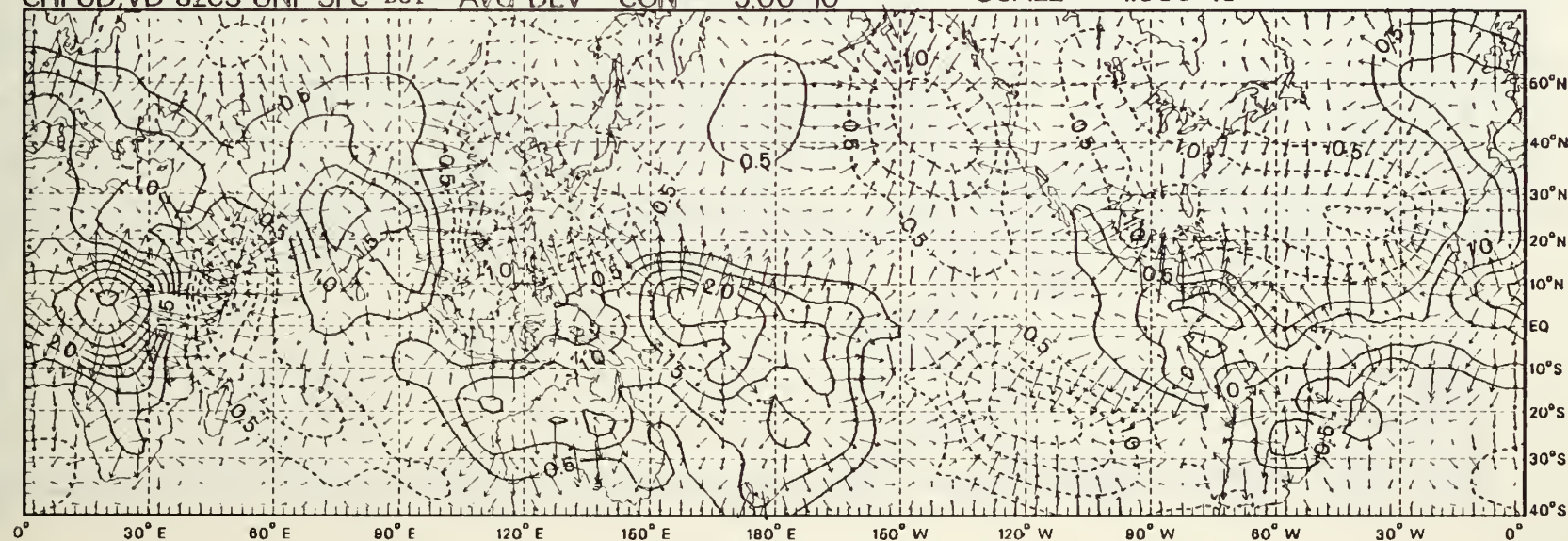
SFC PSI 8283 UNF SFC DJF 1983 CON =  $2.00 \times 10^0$



SFC DEV PSI 8283 UNF SFC DJF AVG DEV CON =  $1.00 \times 10^0$



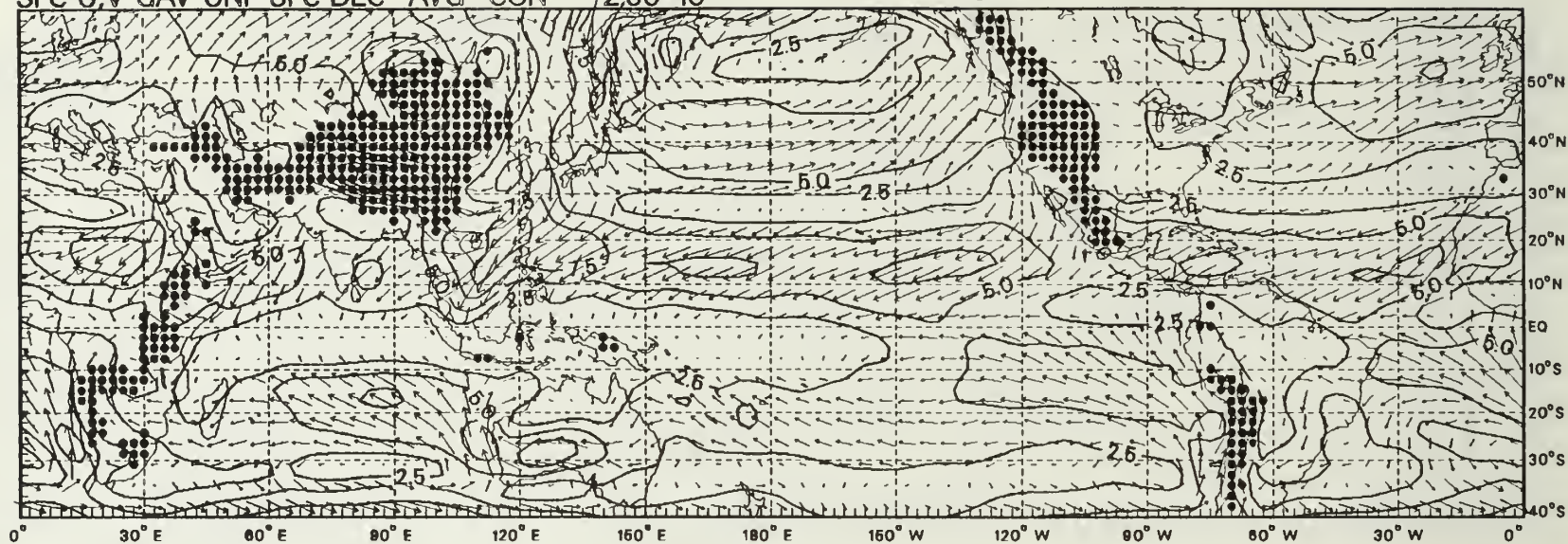


CHI UD.VD 8283 UNF SFC DJF 1983 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$  —CHI UD.VD 8283 UNF SFC DJF AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$  —

SFC U,V GAV UNF SFC DEC AVG CON =  $2.50 \times 10^0$

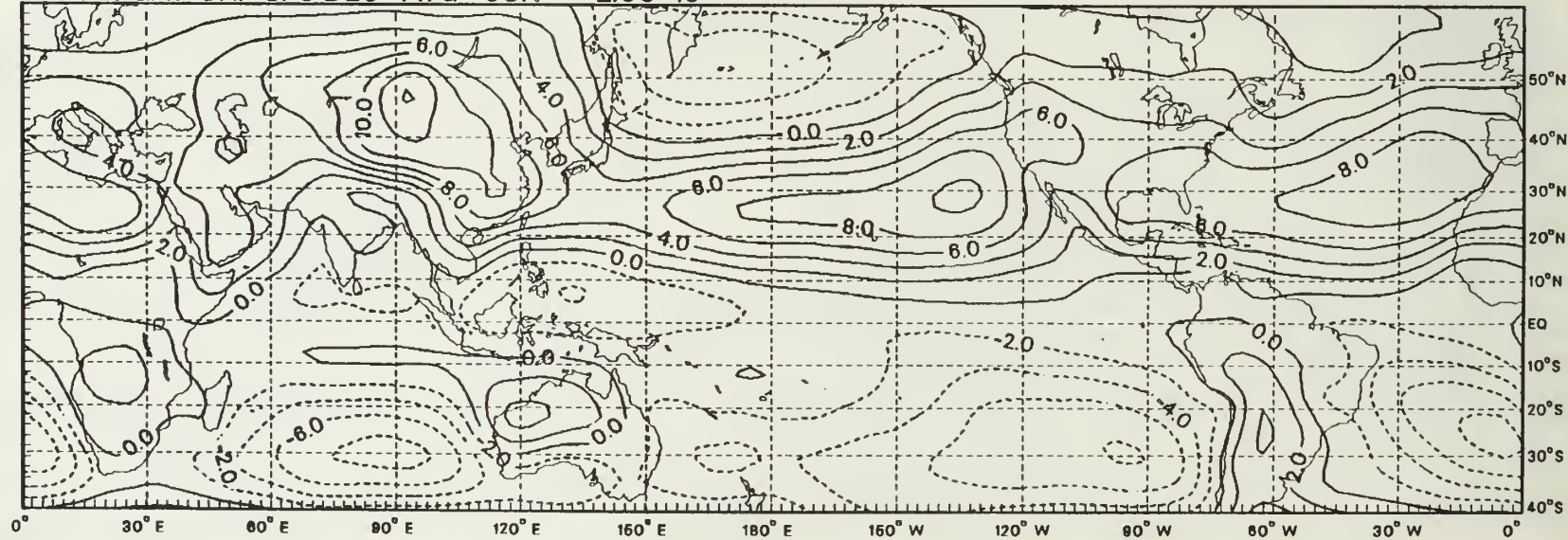
SCALE =  $5.000 \times 10^0$  —

C1



SFC PSI GAV UNF SFC DEC AVG CON =  $2.00 \times 10^0$

C2

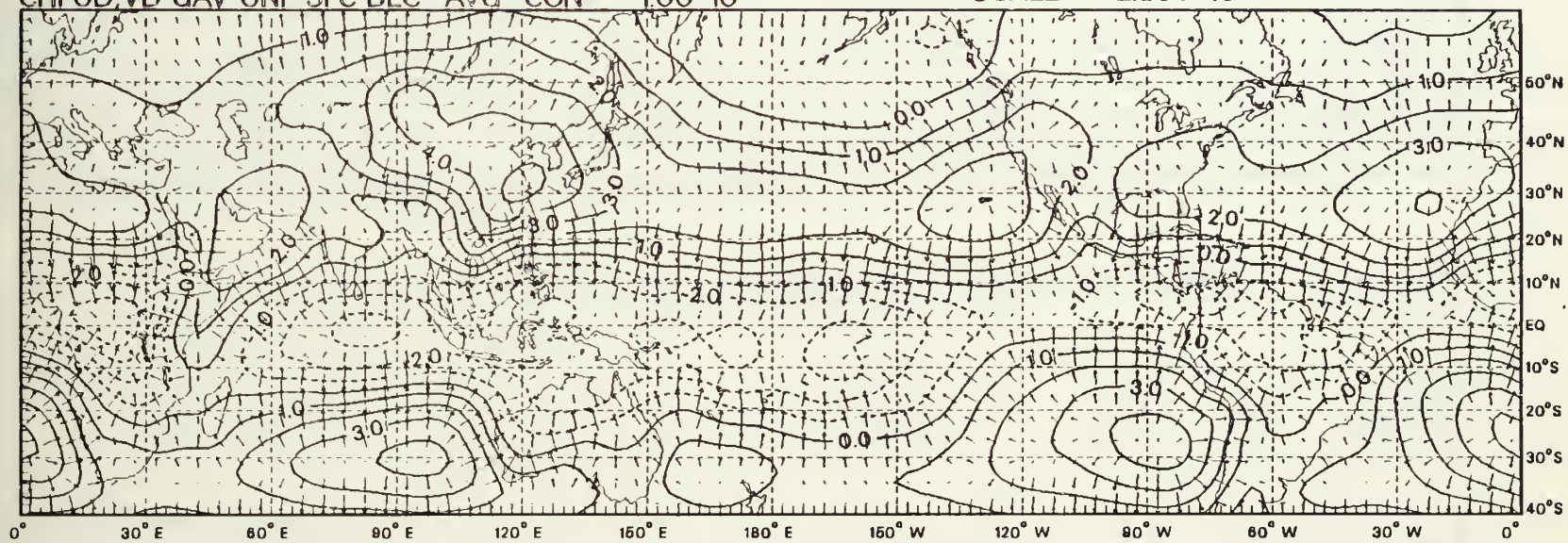




CHI UD,VD GAV UNF SFC DEC AVG CON =  $1.00 \times 10^0$

SCALE =  $2.500 \times 10^0$  —

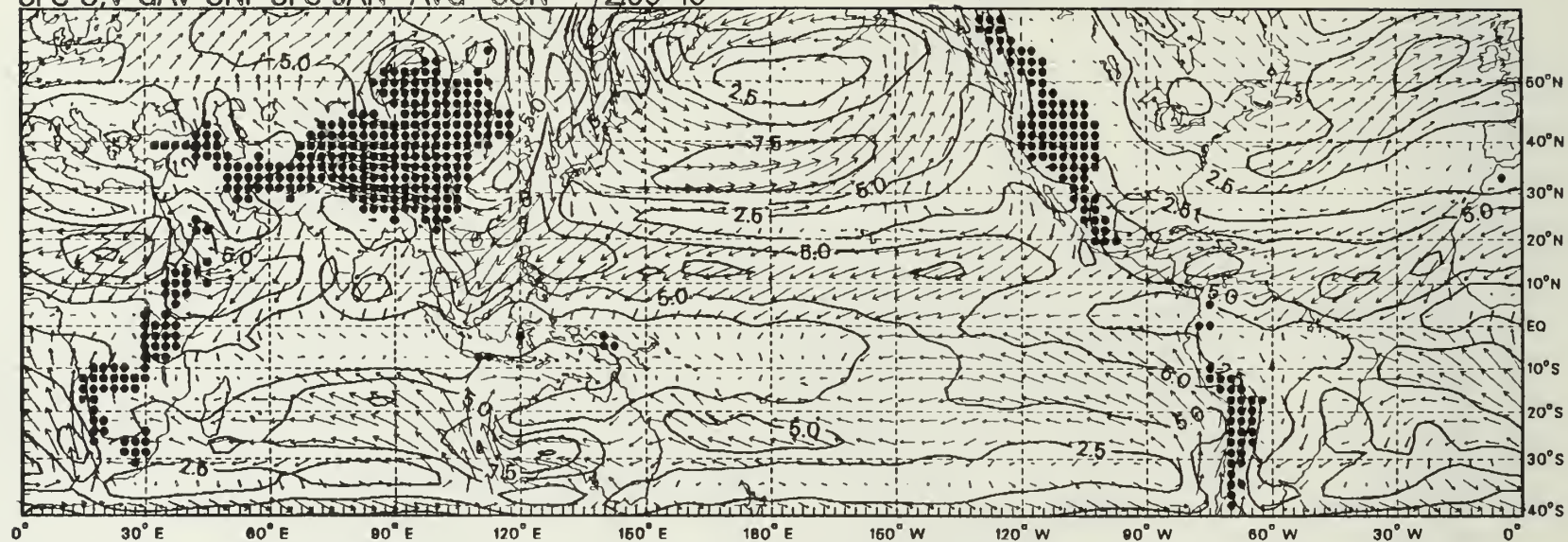
C3



SFC U,V GAV UNF SFC JAN AVG CON =  $2.50 \times 10^0$

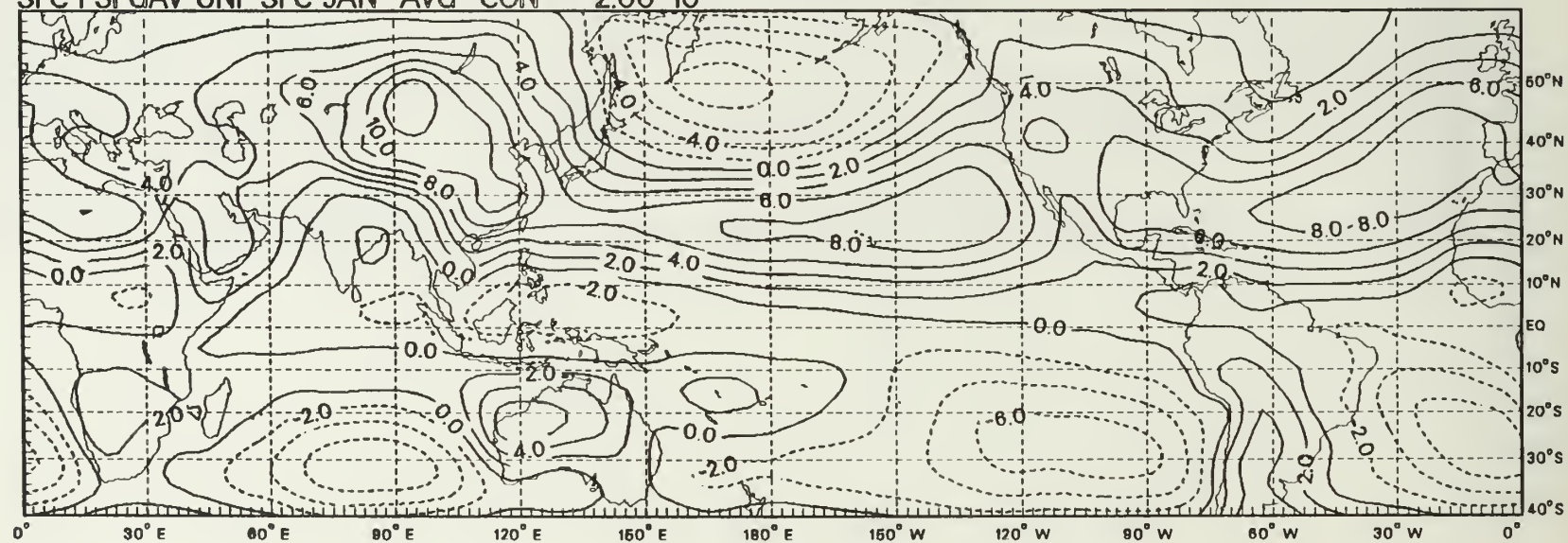
SCALE =  $5.000 \times 10^0$  —

C4



SFC PSI GAV UNF SFC JAN AVG CON =  $2.00 \times 10^0$

C5

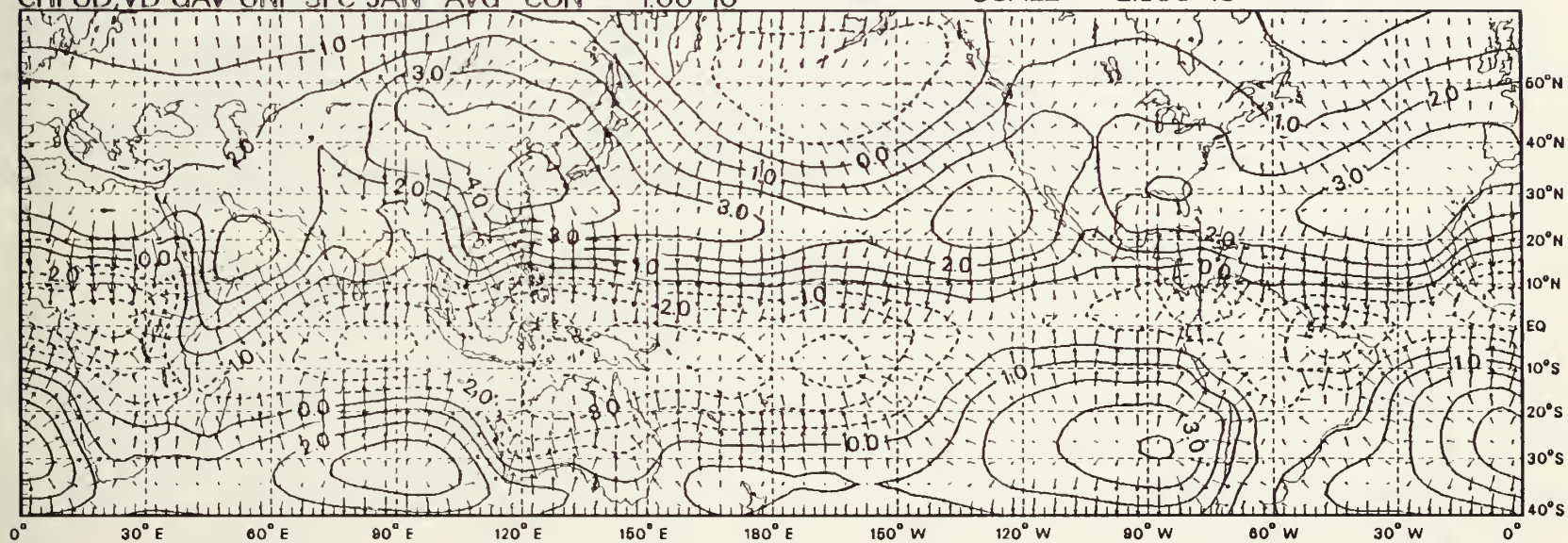




CHI UD, VD GAV UNF SFC JAN AVG CON =  $1.00 \times 10^0$

SCALE =  $2.500 \times 10^0$  —

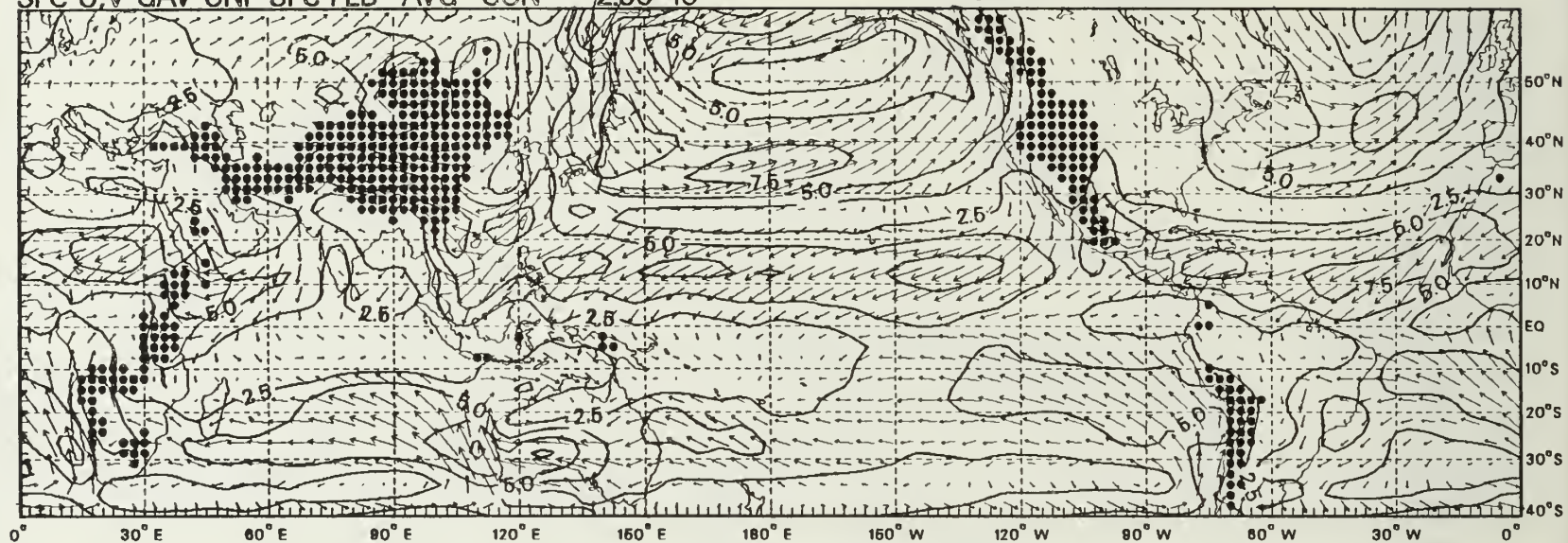
C6



SFC U,V GAV UNF SFC FEB AVG CON =  $2.50 \times 10^0$

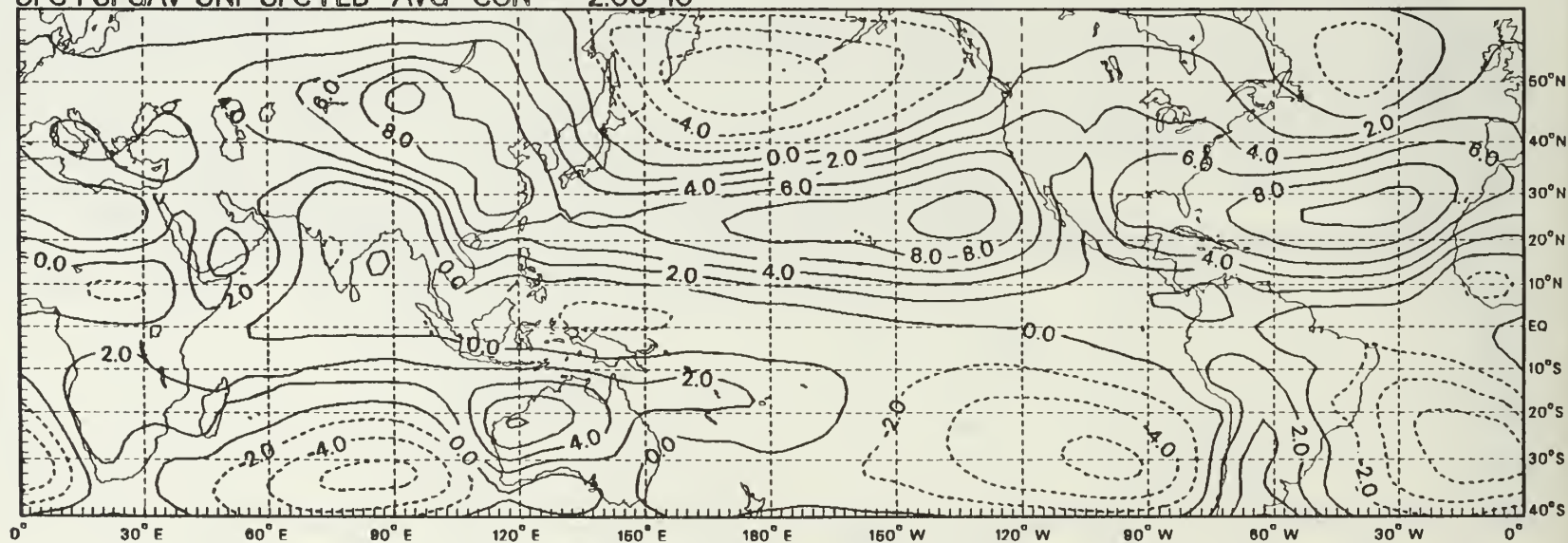
SCALE =  $5.000 \times 10^0$  —

C7



SFC PSI GAV UNF SFC FEB AVG CON =  $2.00 \times 10^0$

C8

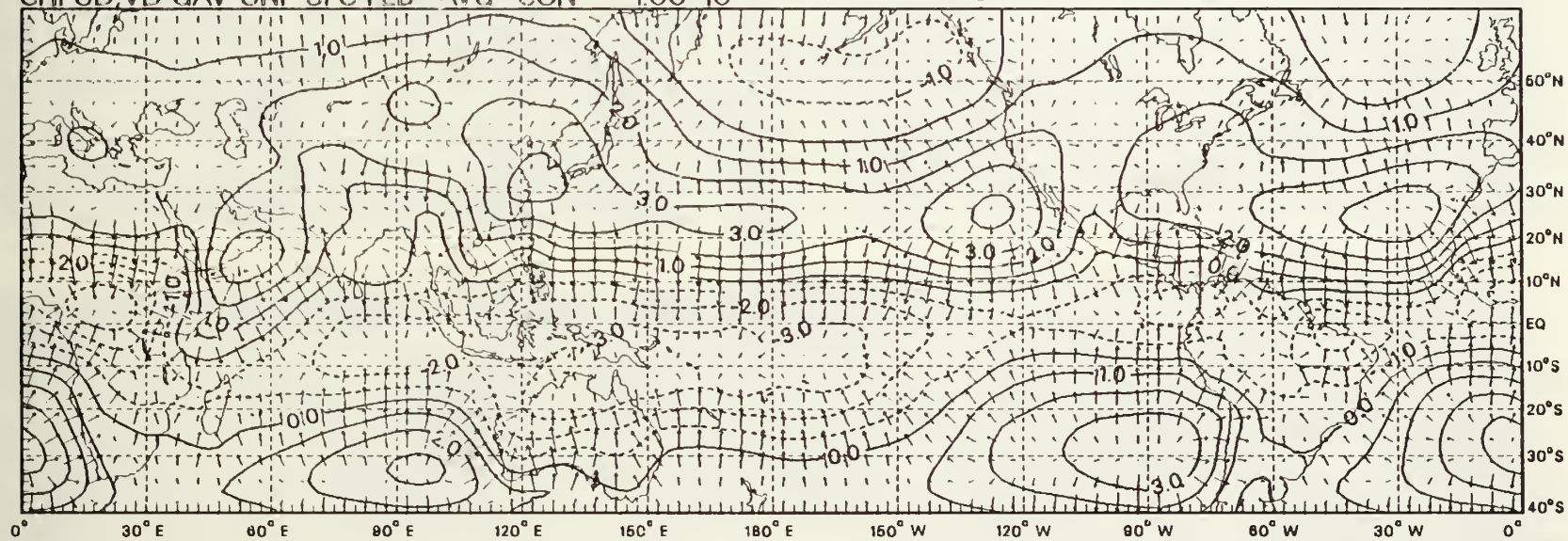




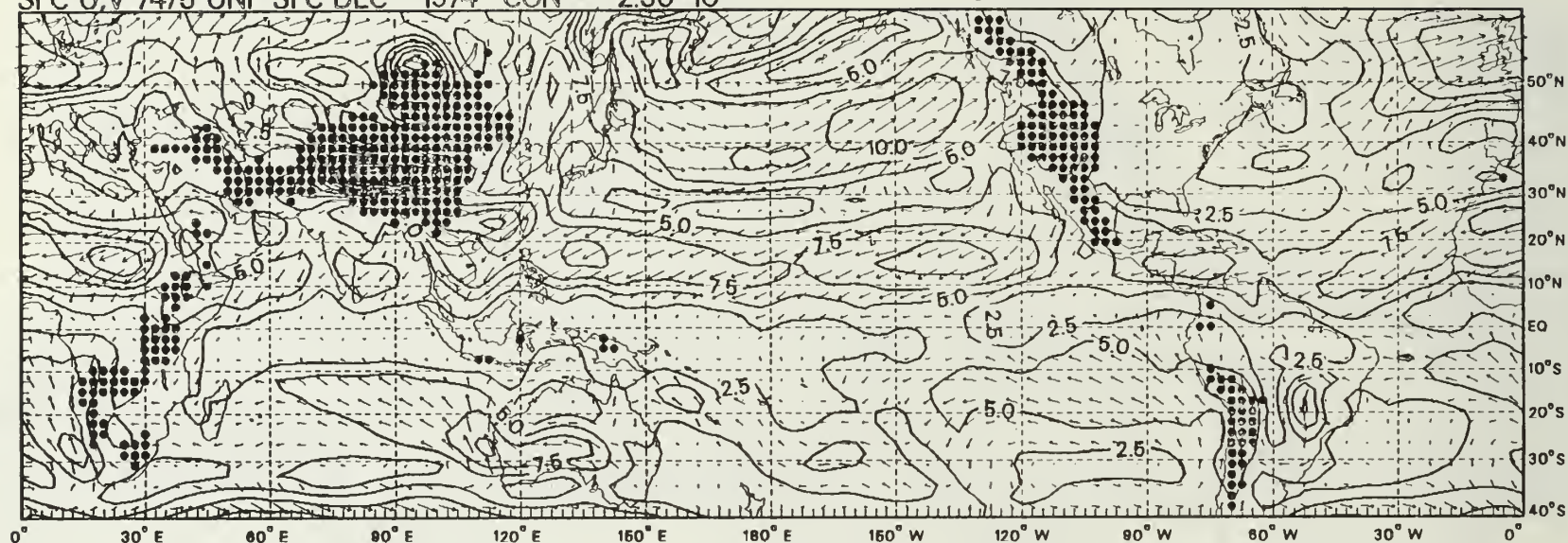
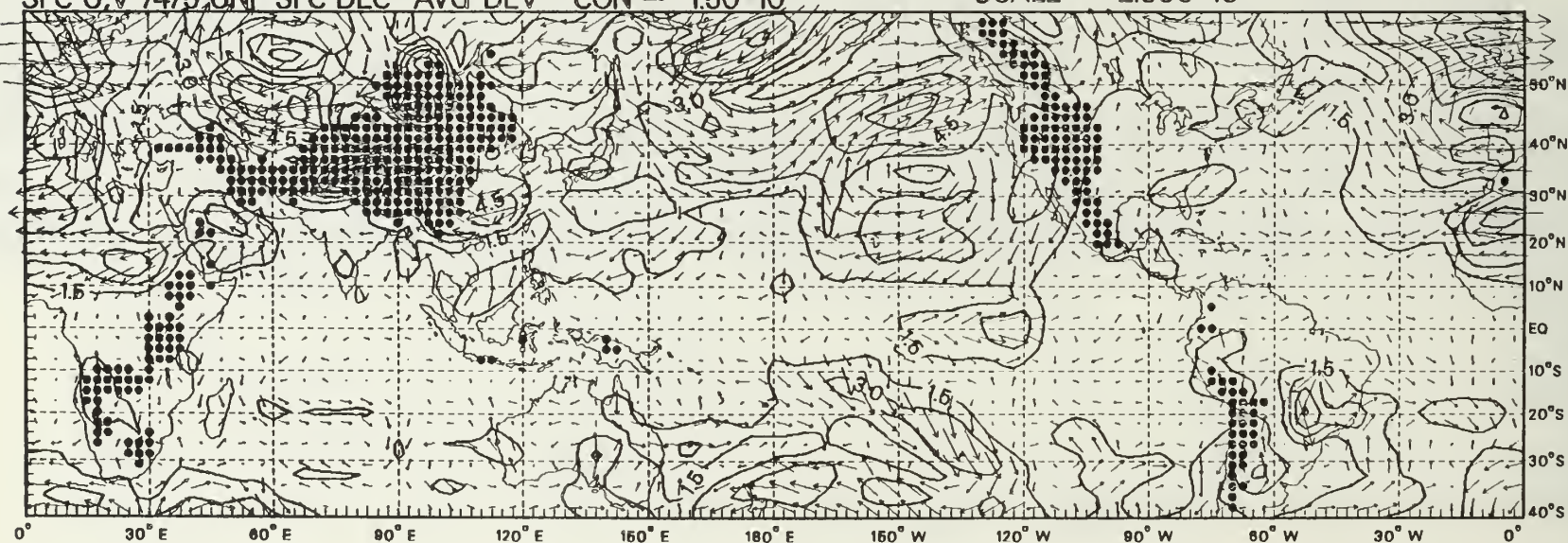
CHI UD,VD GAV UNF SFC FEB AVG CON =  $1.00 \times 10^0$

SCALE =  $2.500 \times 10^0$  —

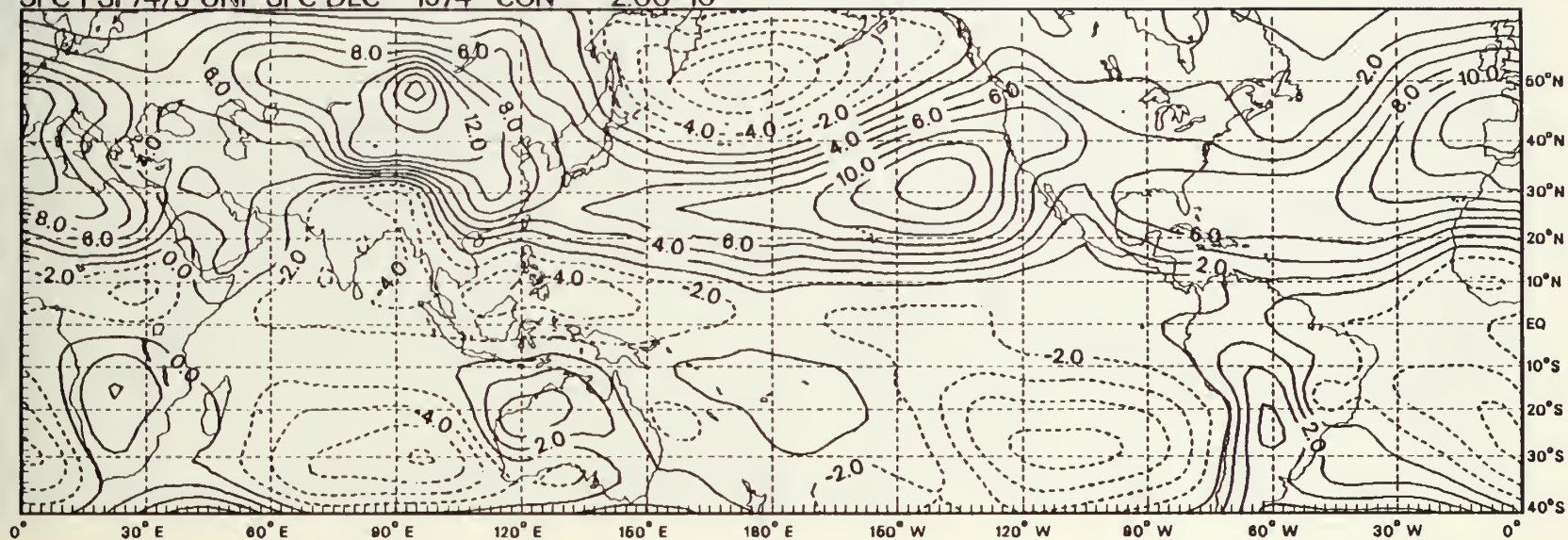
C9



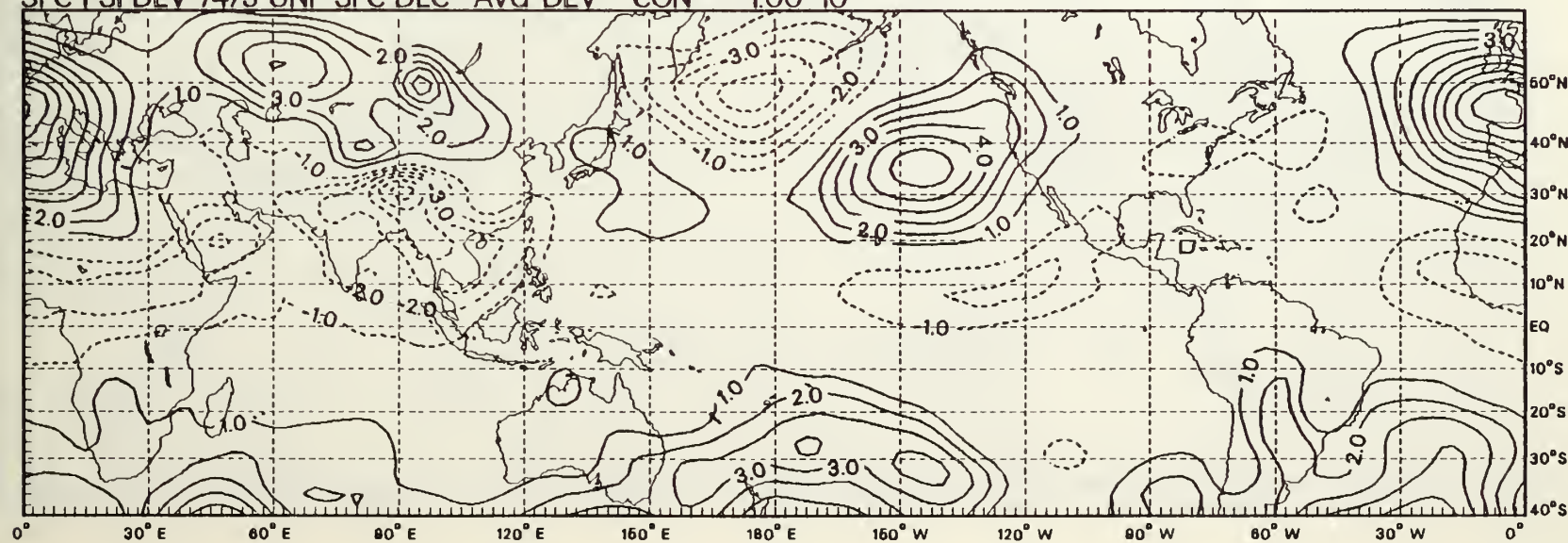


SFC U,V 7475 UNF SFC DEC 1974 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U,V 7475 UNF SFC DEC AVG DEV CON =  $1.50 \times 10^0$ SCALE =  $2.500 \times 10^0$  —

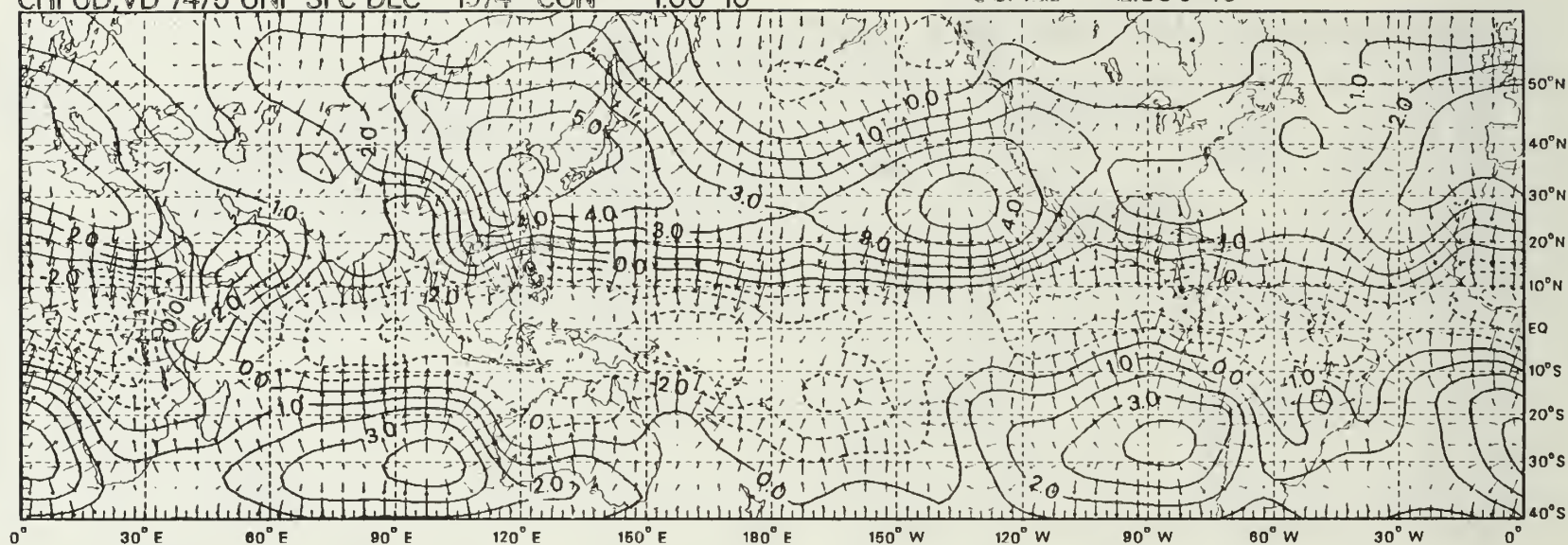
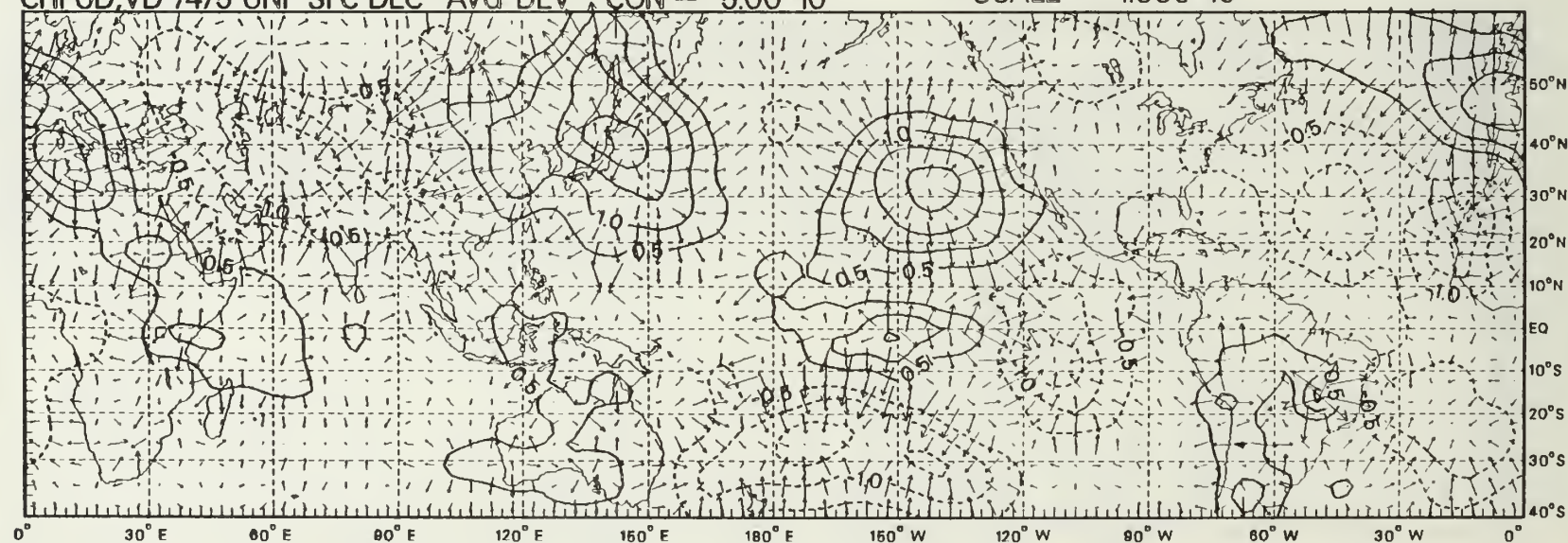
SFC PSI 7475 UNF SFC DEC 1974 CON =  $2.00 \times 10^0$



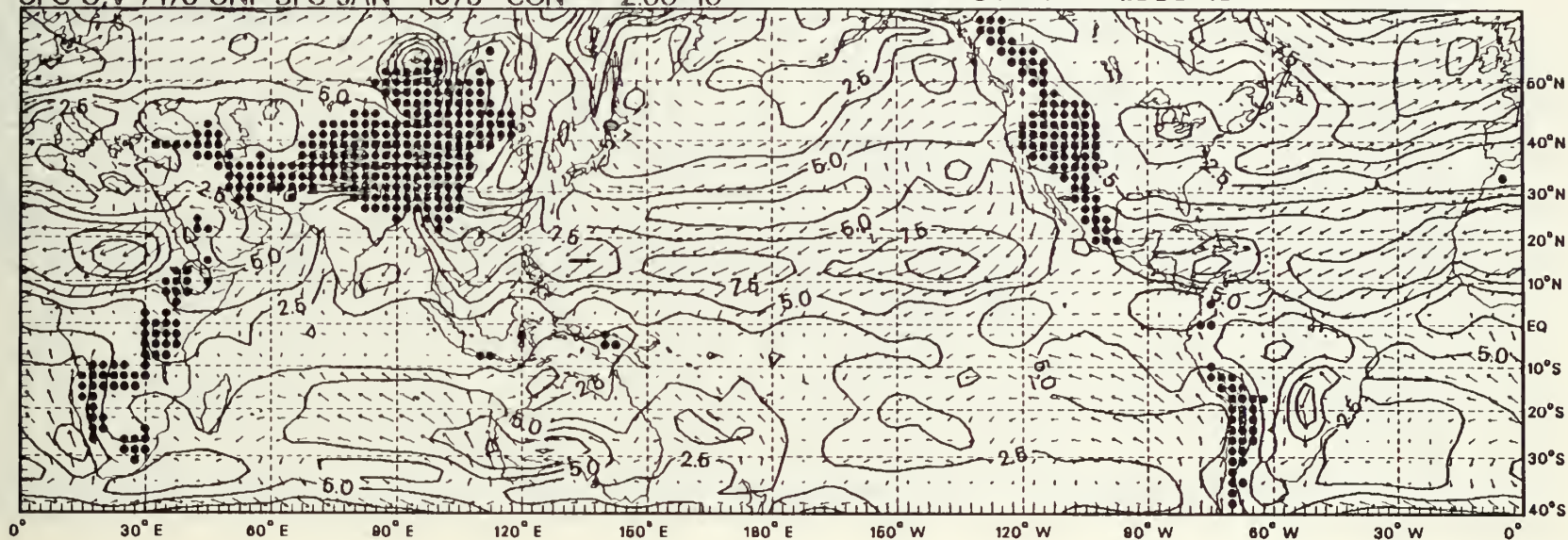
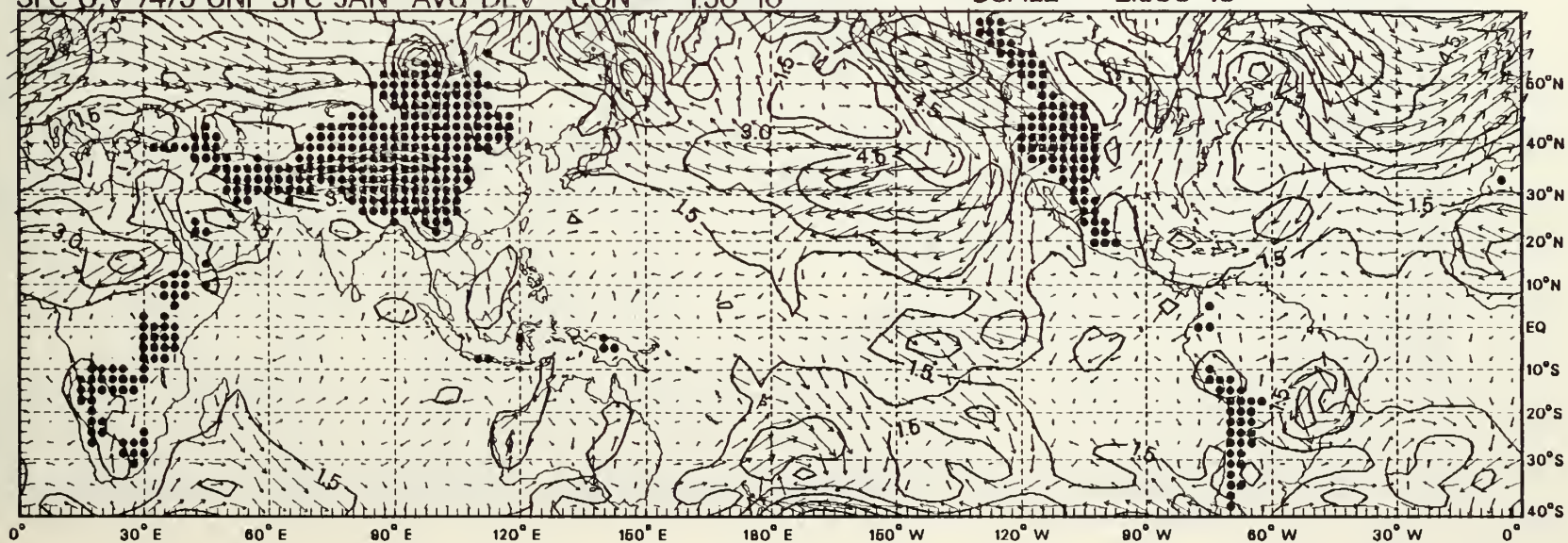
SFC PSI DEV 7475 UNF SFC DEC AVG DEV CON =  $1.00 \times 10^0$



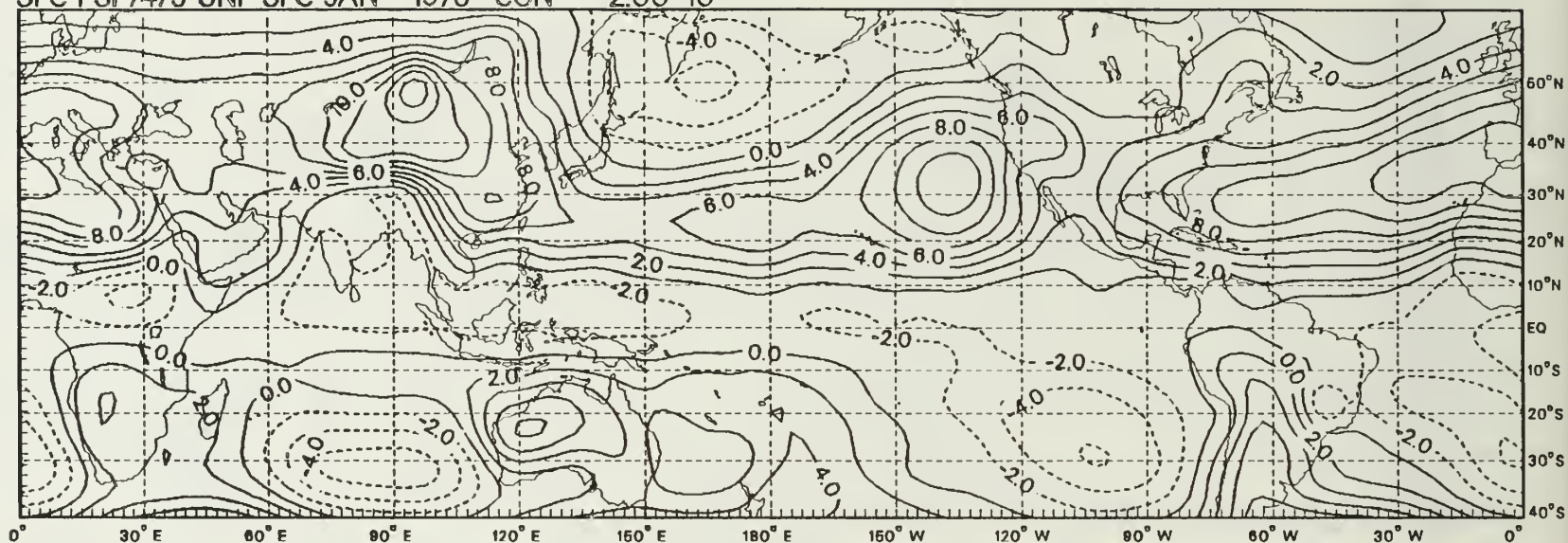


CHI UD,VD 7475 UNF SFC DEC 1974 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$  —CHI UD,VD 7475 UNF SFC DEC AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$  —

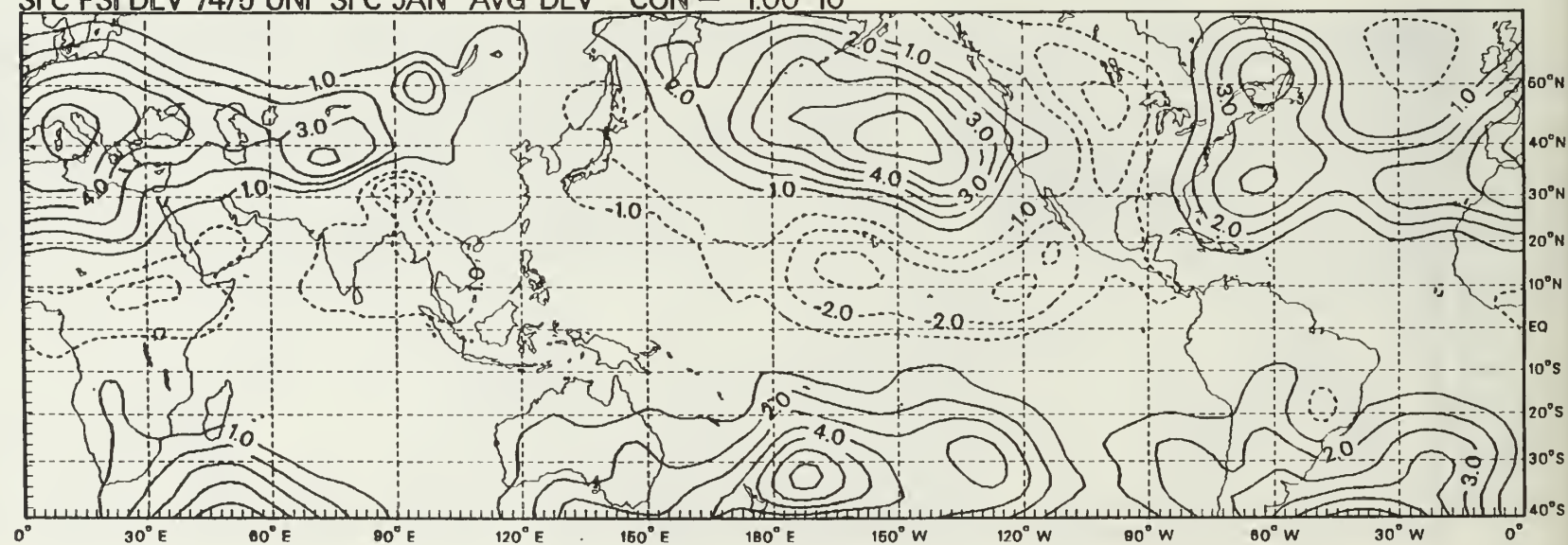


SFC U,V 7475 UNF SFC JAN 1975 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U,V 7475 UNF SFC JAN AVG DEV CON =  $1.50 \times 10^0$ SCALE =  $2.500 \times 10^0$  —

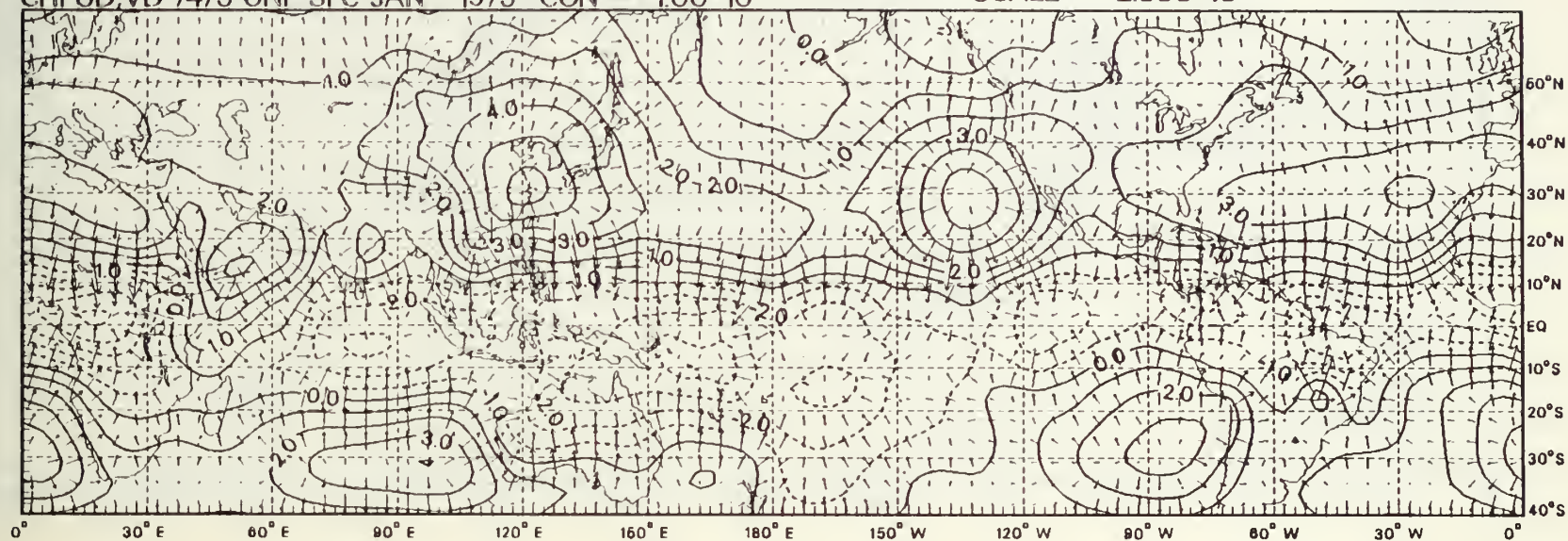
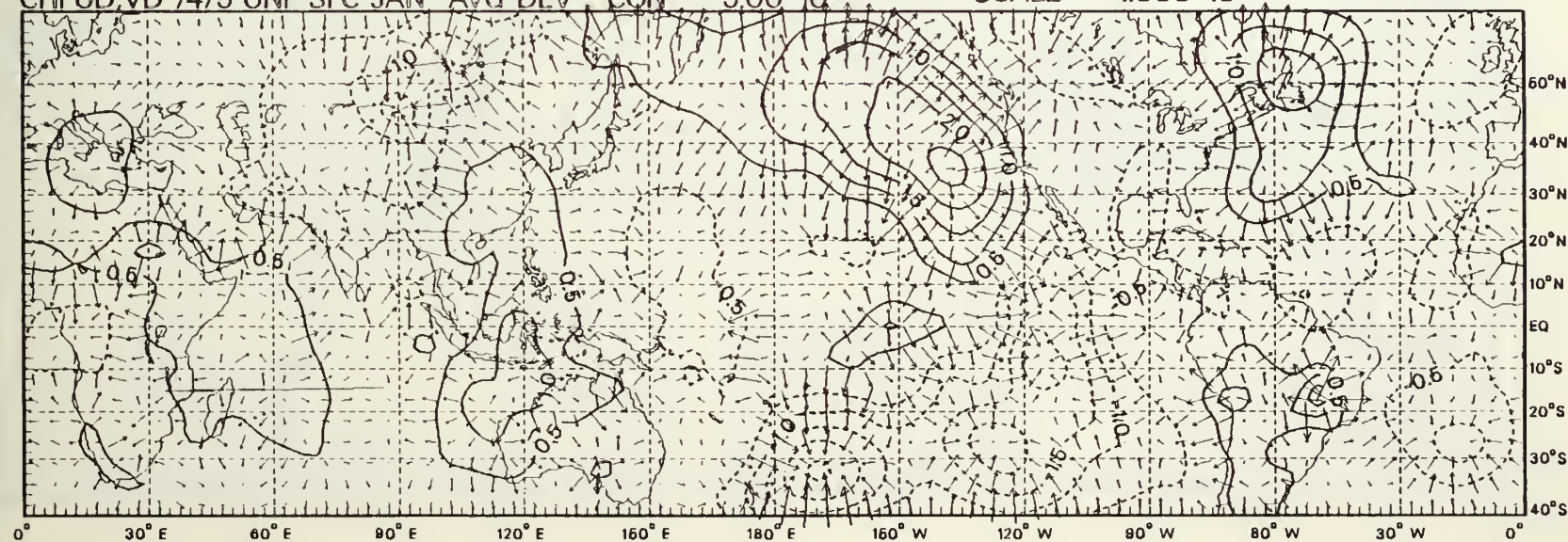
SFC PSI 7475 UNF SFC JAN 1975 CON =  $2.00 \times 10^0$



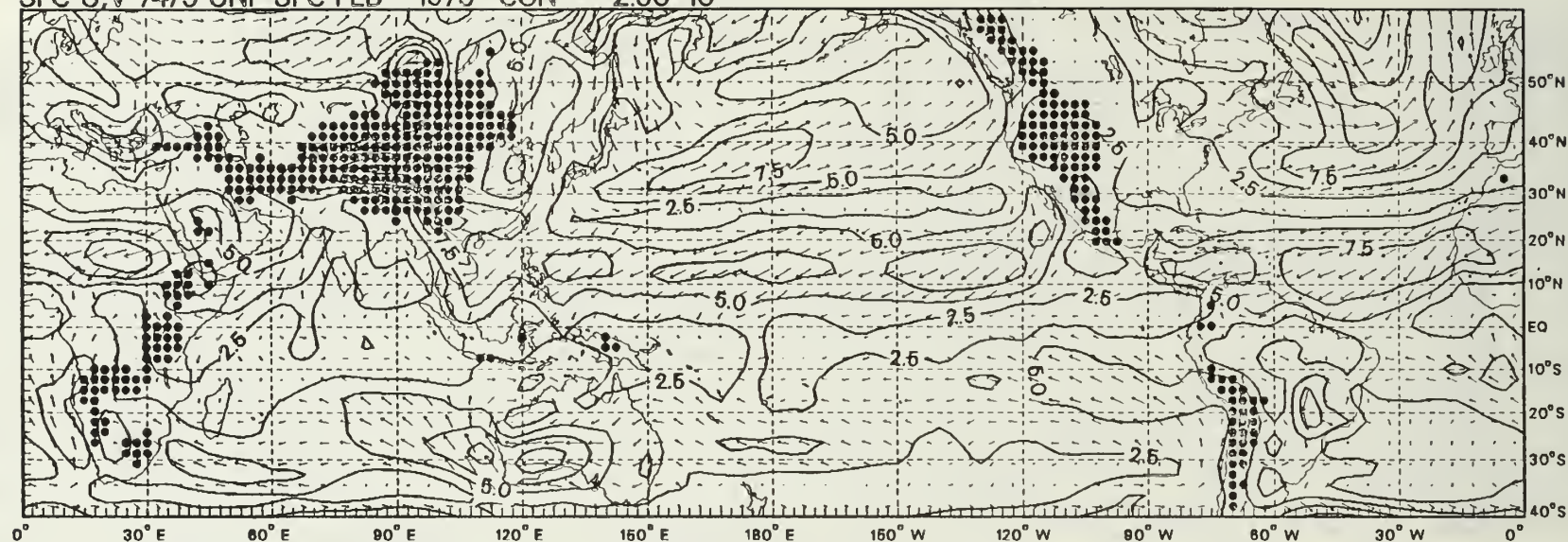
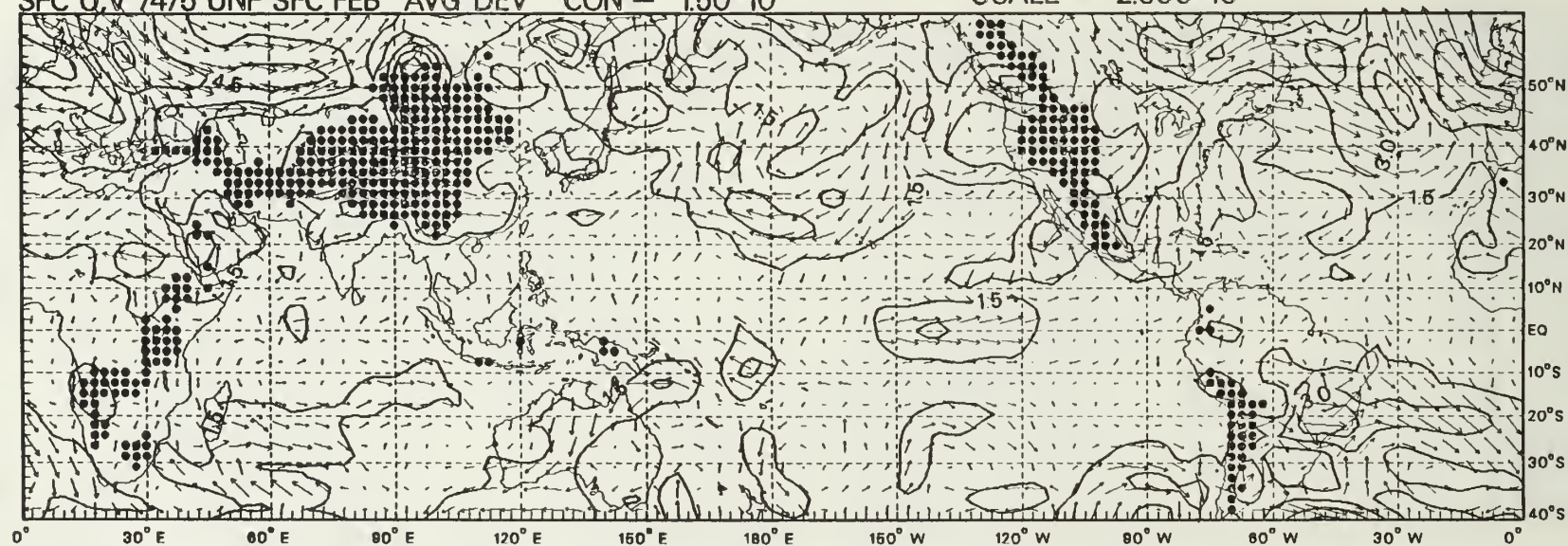
SFC PSI DEV 7475 UNF SFC JAN AVG DEV CON =  $1.00 \times 10^0$

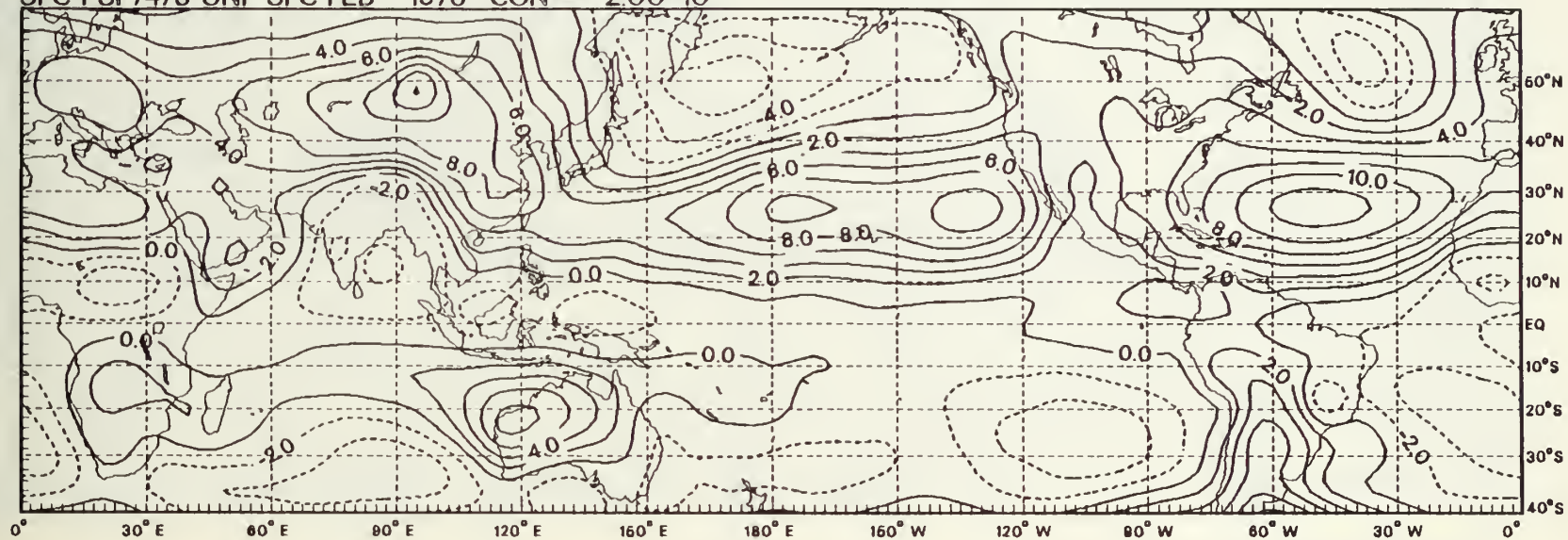
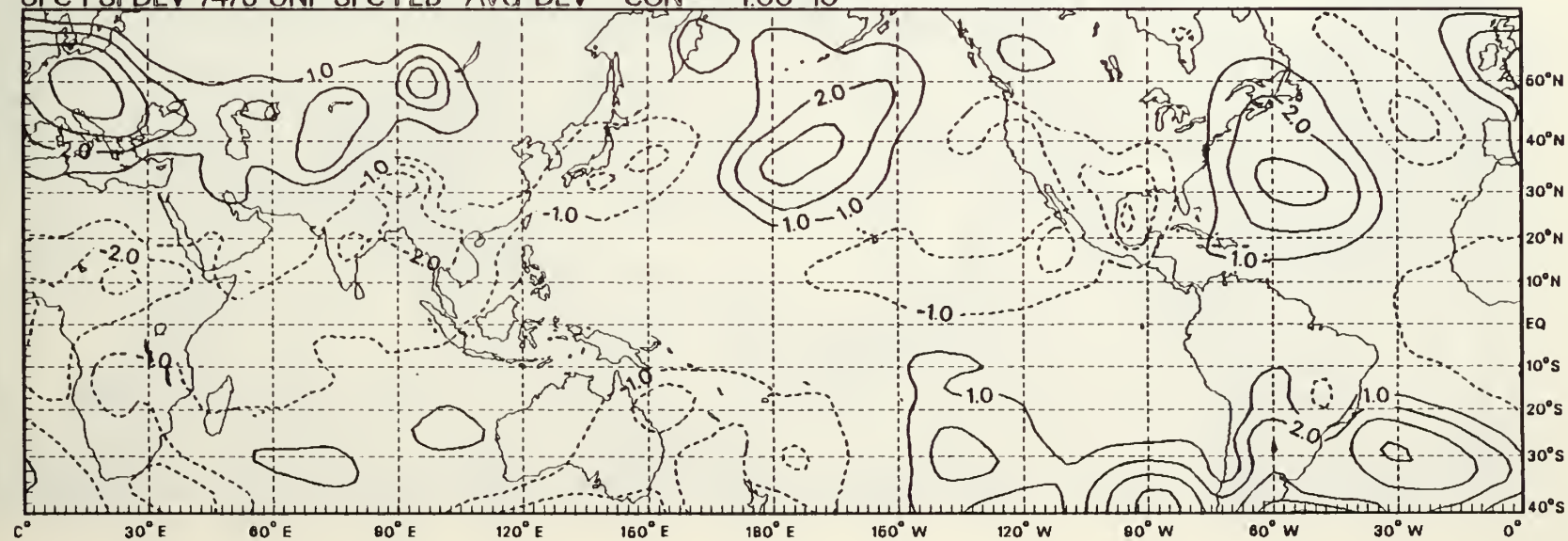




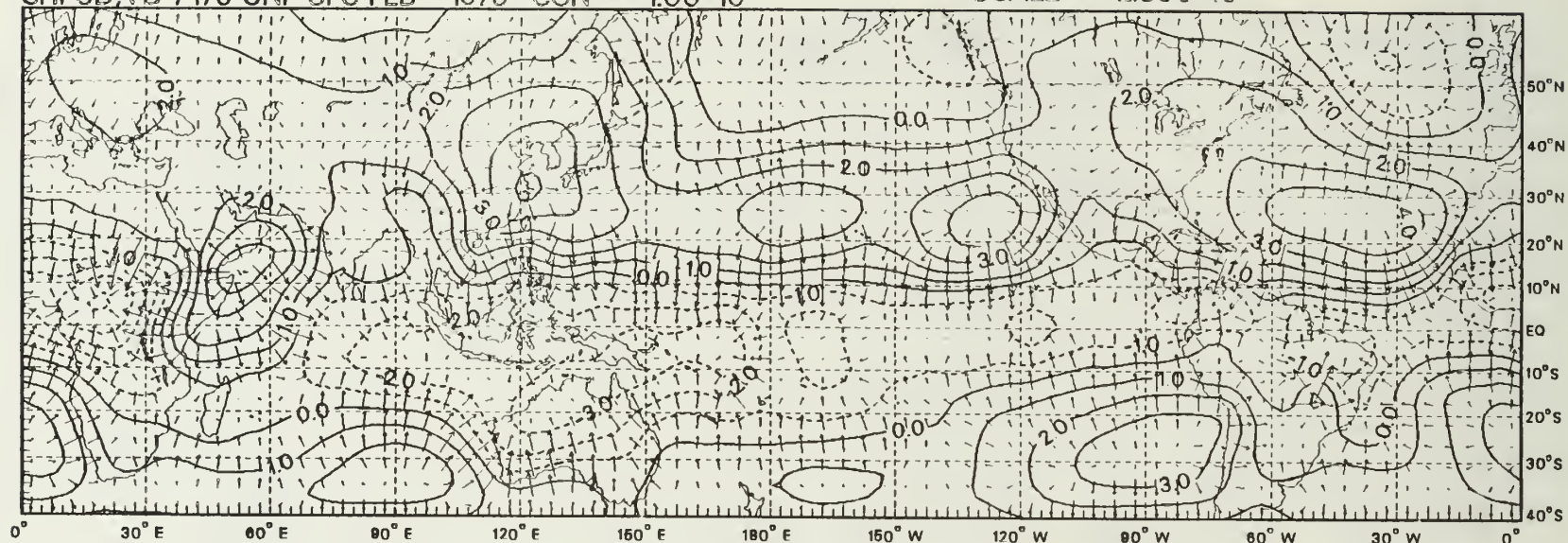
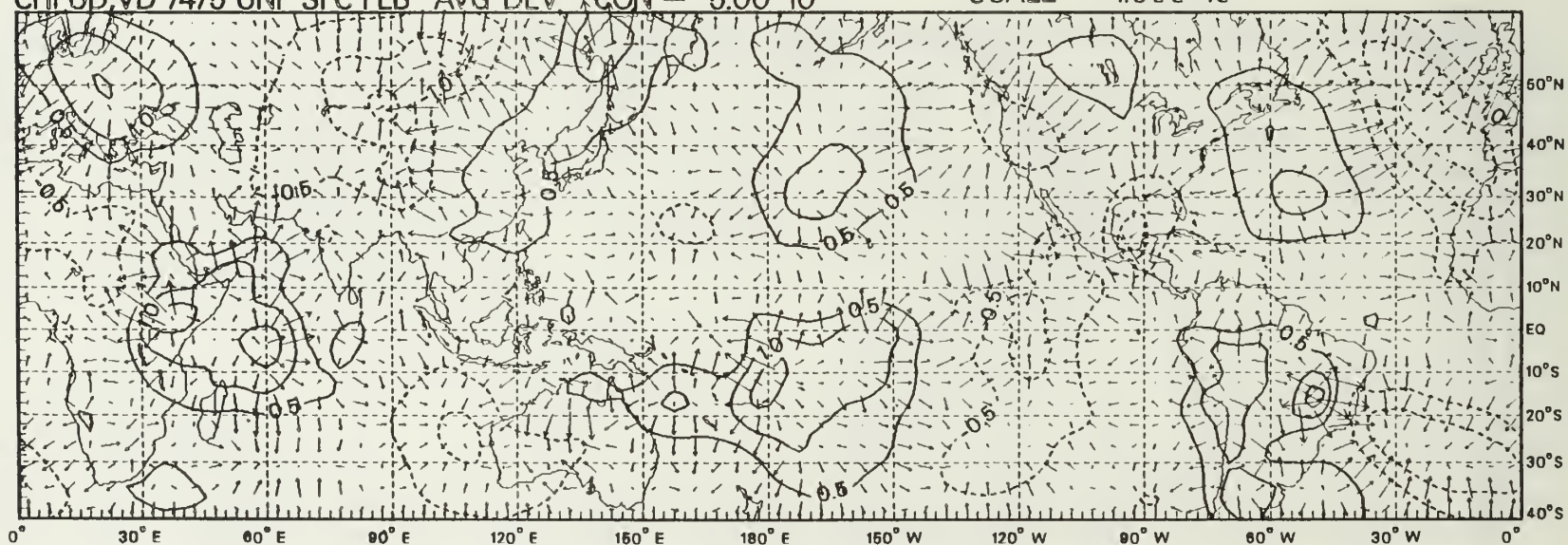
CHI UD.VD 7475 UNF SFC JAN 1975 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$  —CHI UD.VD 7475 UNF SFC JAN AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$  —



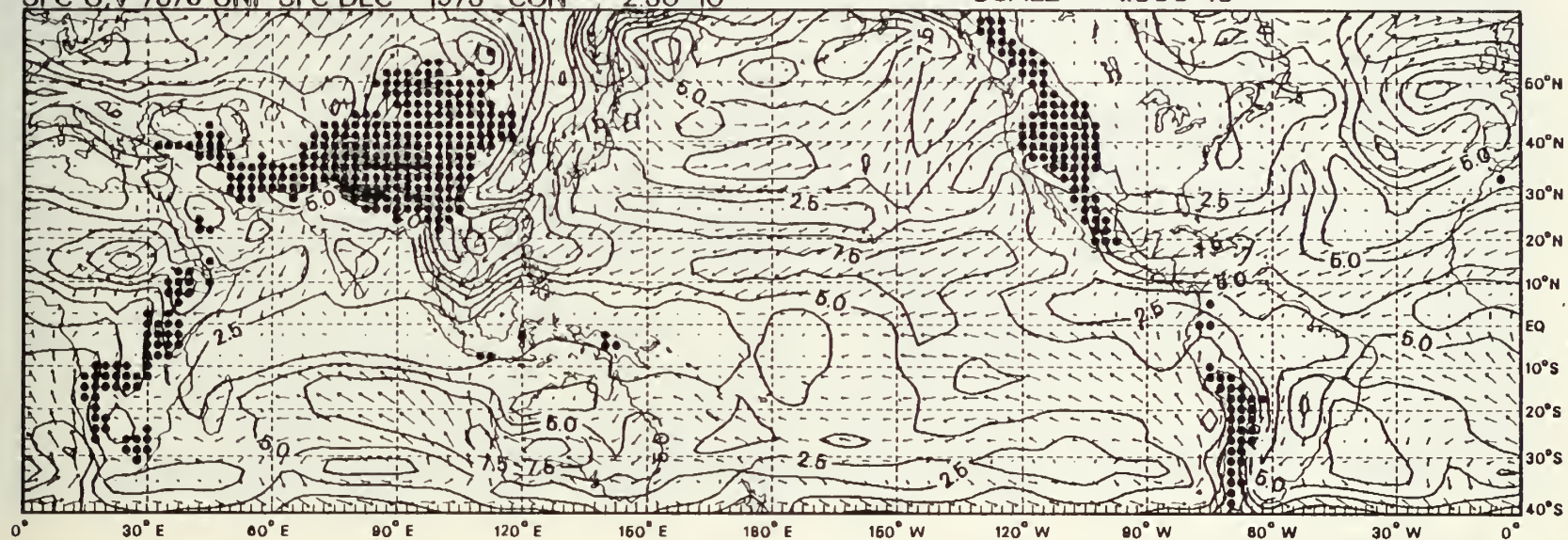
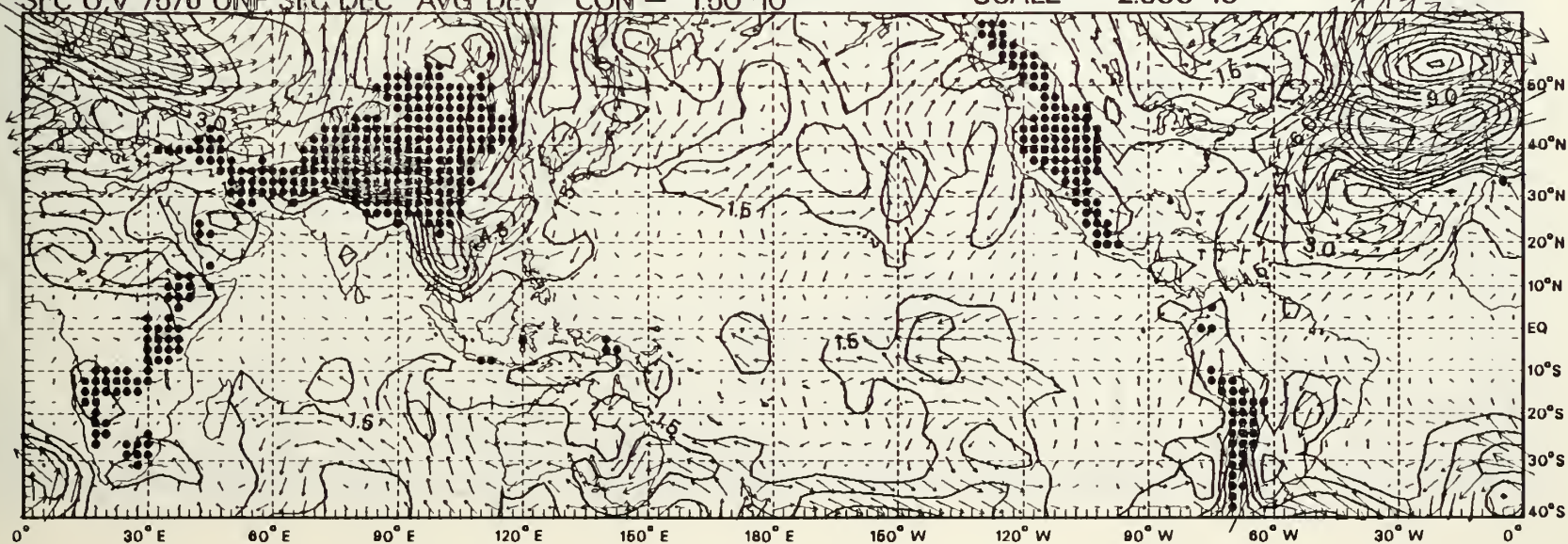
SFC U,V 7475 UNF SFC FEB 1975 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U,V 7475 UNF SFC FEB AVG DEV CON =  $1.50 \times 10^0$ SCALE =  $2.500 \times 10^0$  —

SFC PSI 7475 UNF SFC FEB 1975 CON =  $2.00 \times 10^0$ SFC PSI DEV 7475 UNF SFC FEB AVG DEV CON =  $1.00 \times 10^0$ 

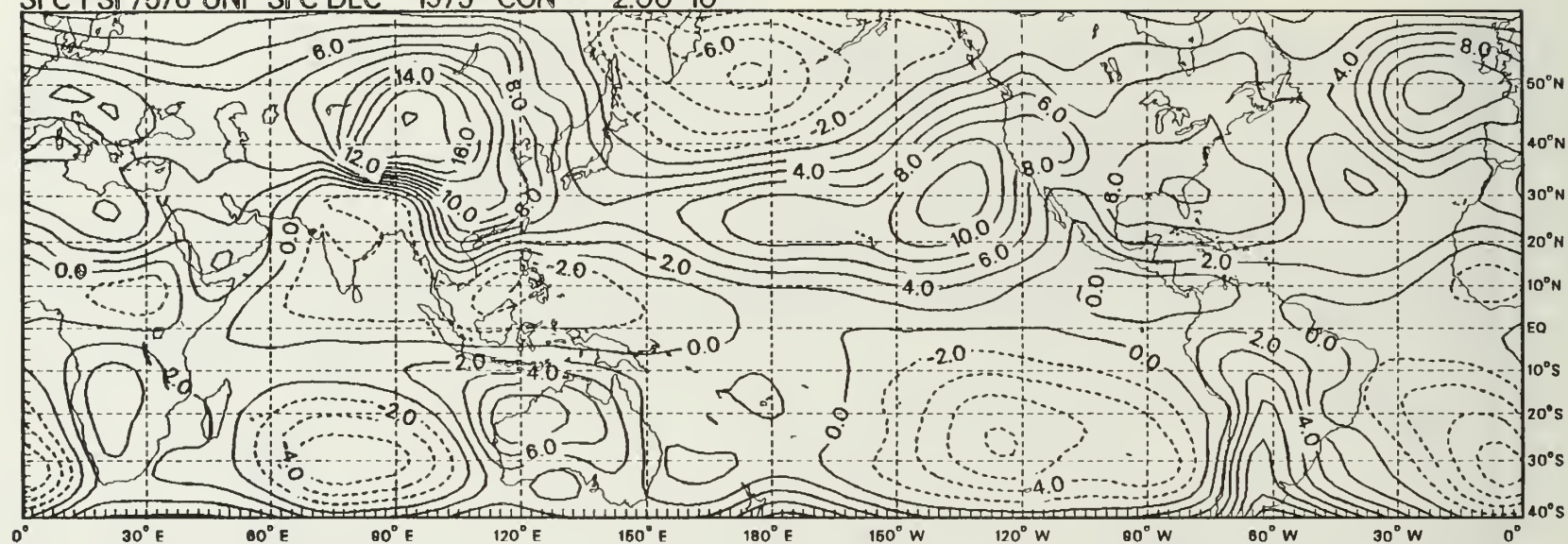


CHI UD, VD 7475 UNF SFC FEB 1975 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$  —CHI UD, VD 7475 UNF SFC FEB AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$  —

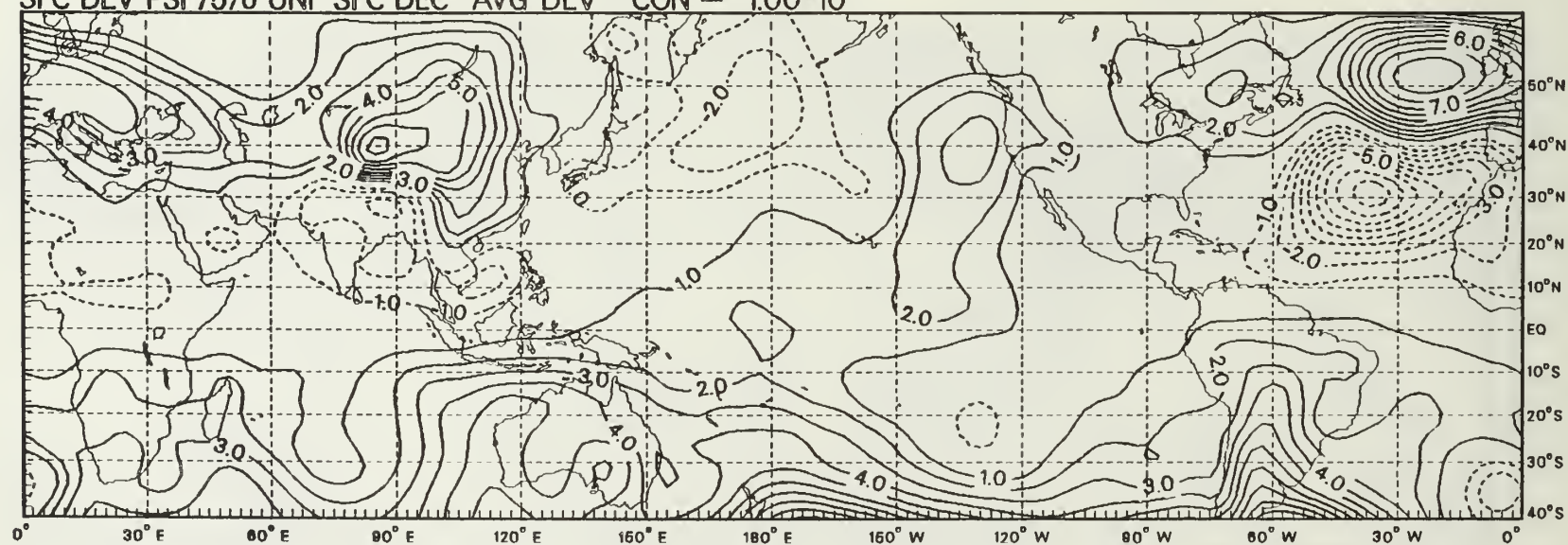


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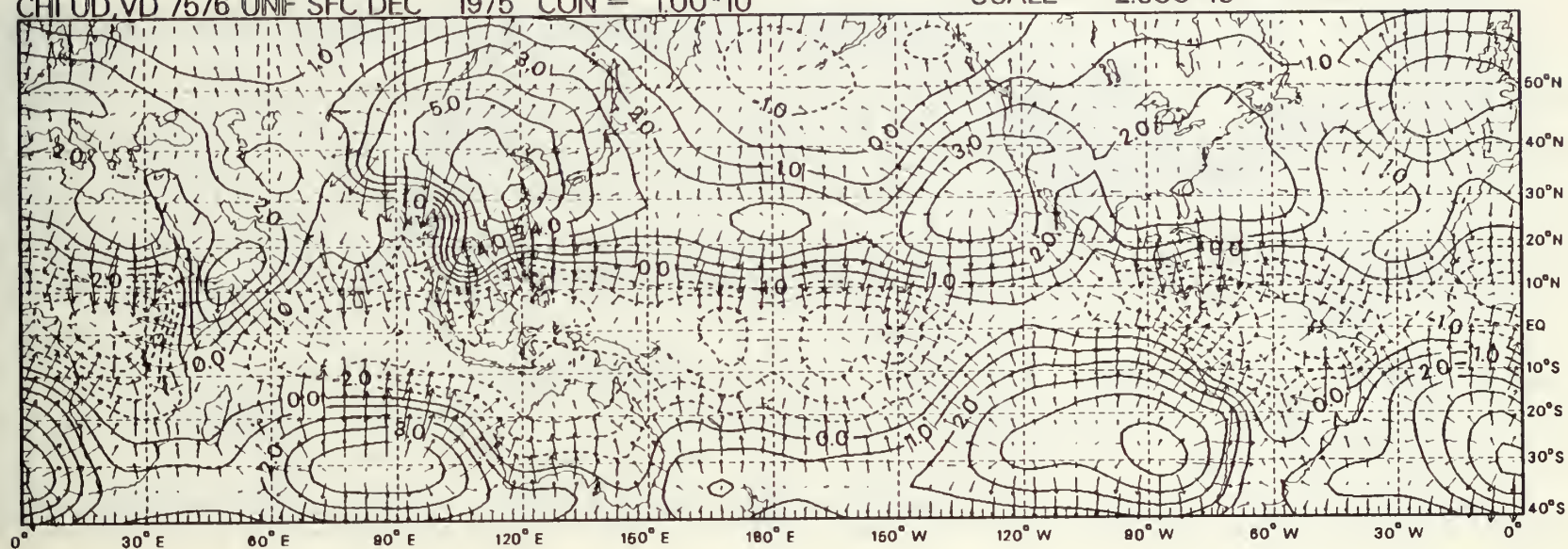
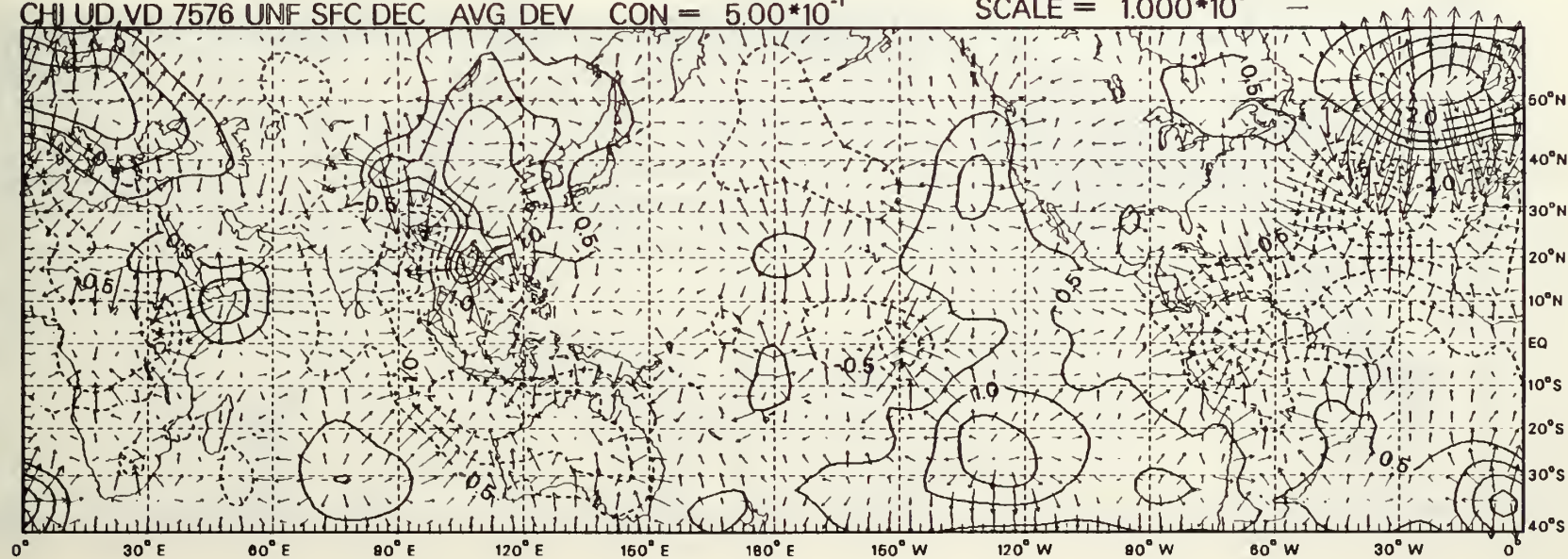
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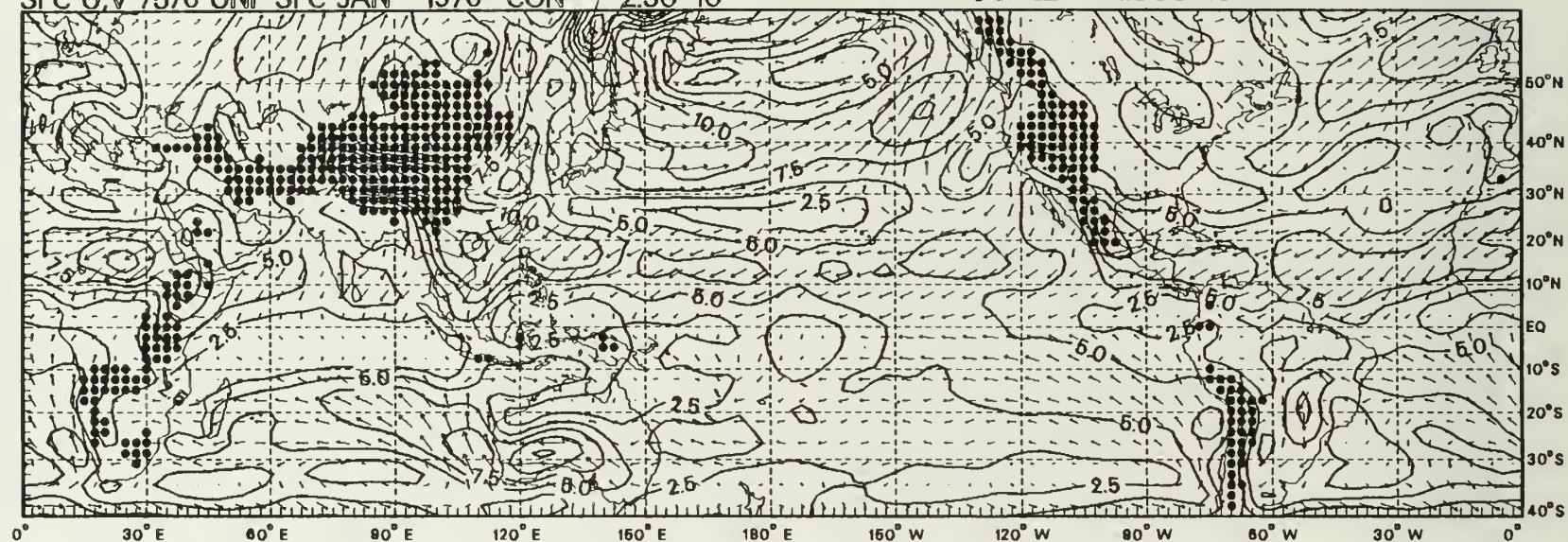
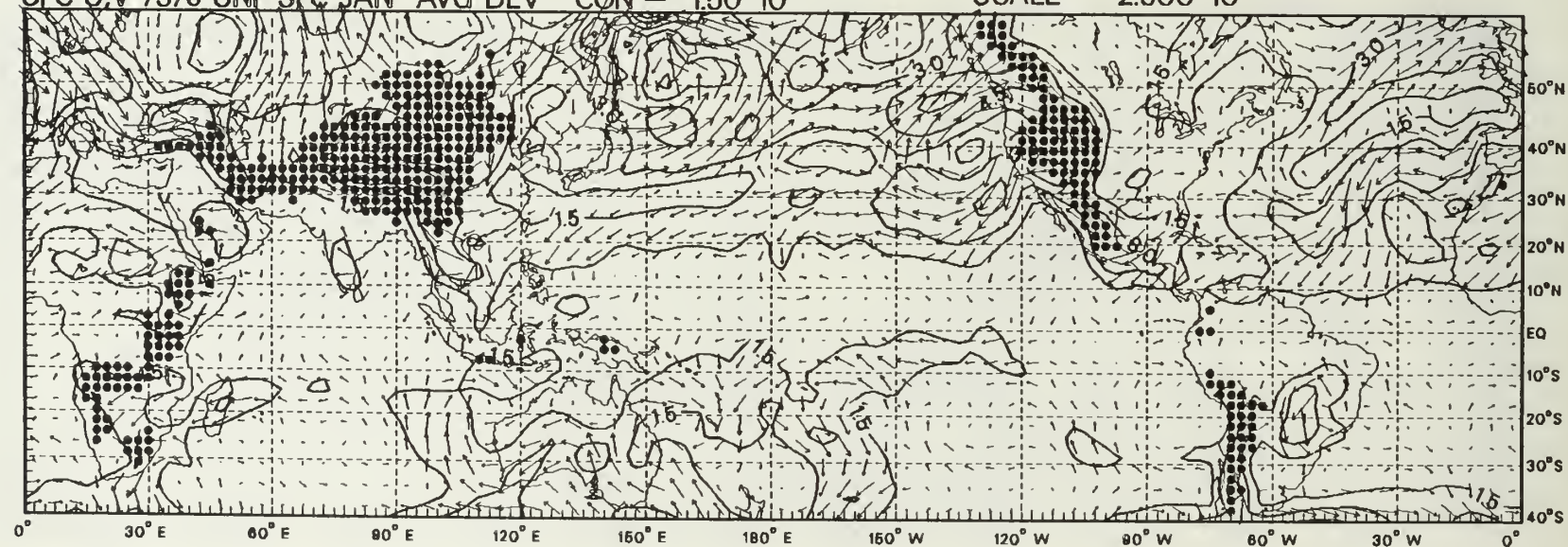
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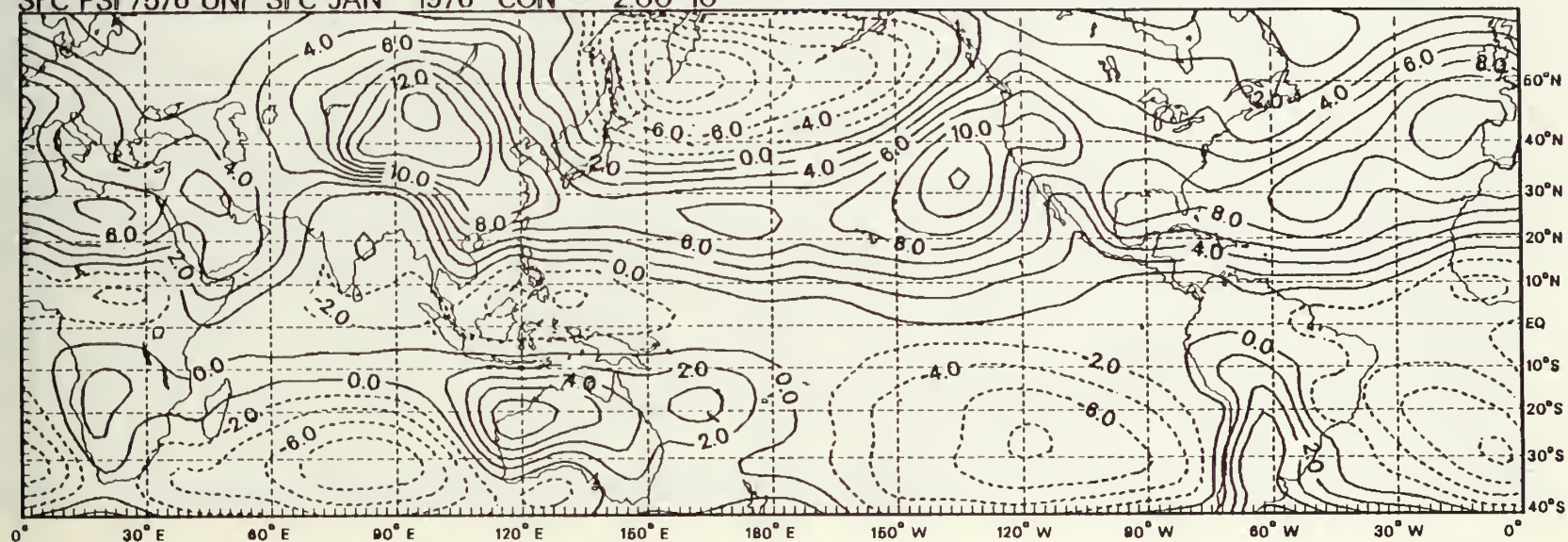


CHI UD.VD 7576 UNF SFC DEC 1975 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$  —CHI UD.VD 7576 UNF SFC DEC AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$  —

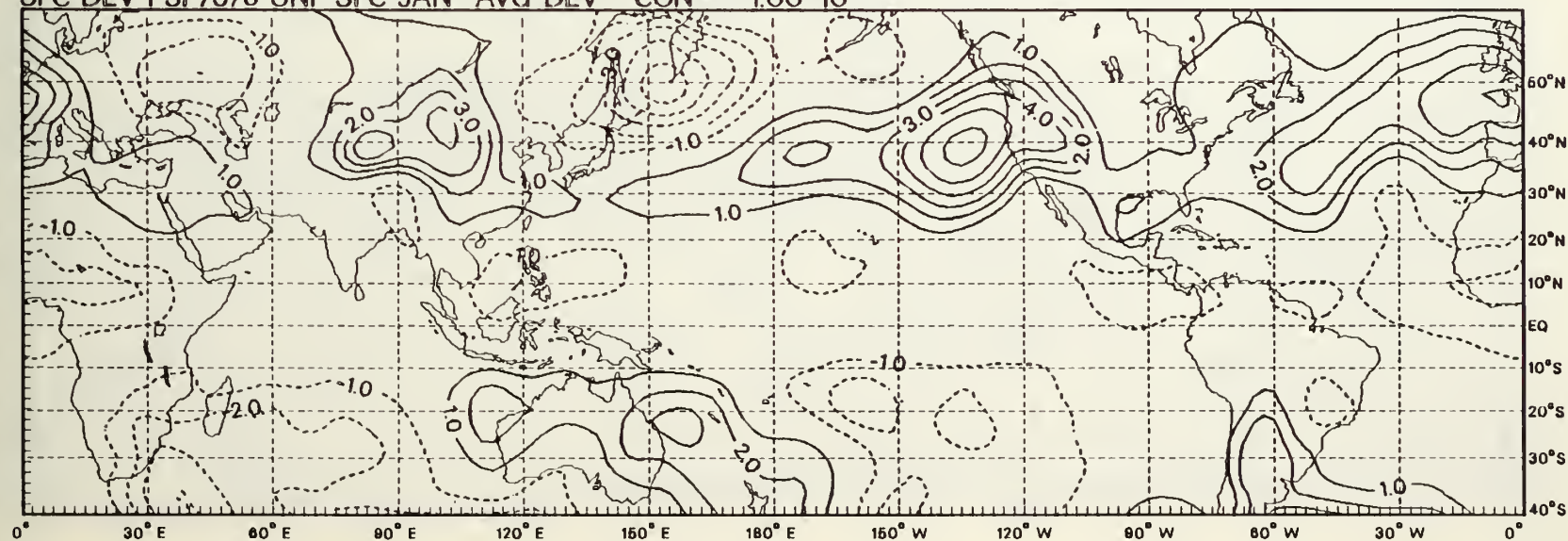


SFC U.V 7576 UNF SFC JAN 1976 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U.V 7576 UNF SFC JAN AVG DEV CON =  $1.50 \times 10^0$ SCALE =  $2.500 \times 10^0$  —

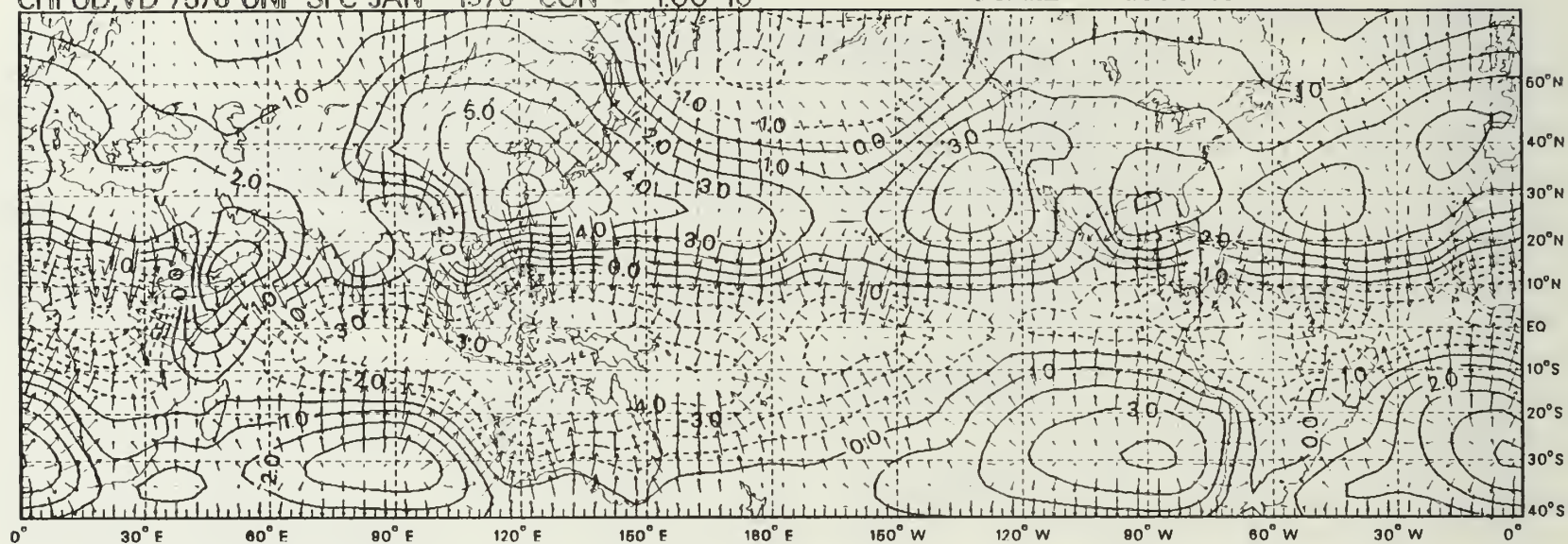
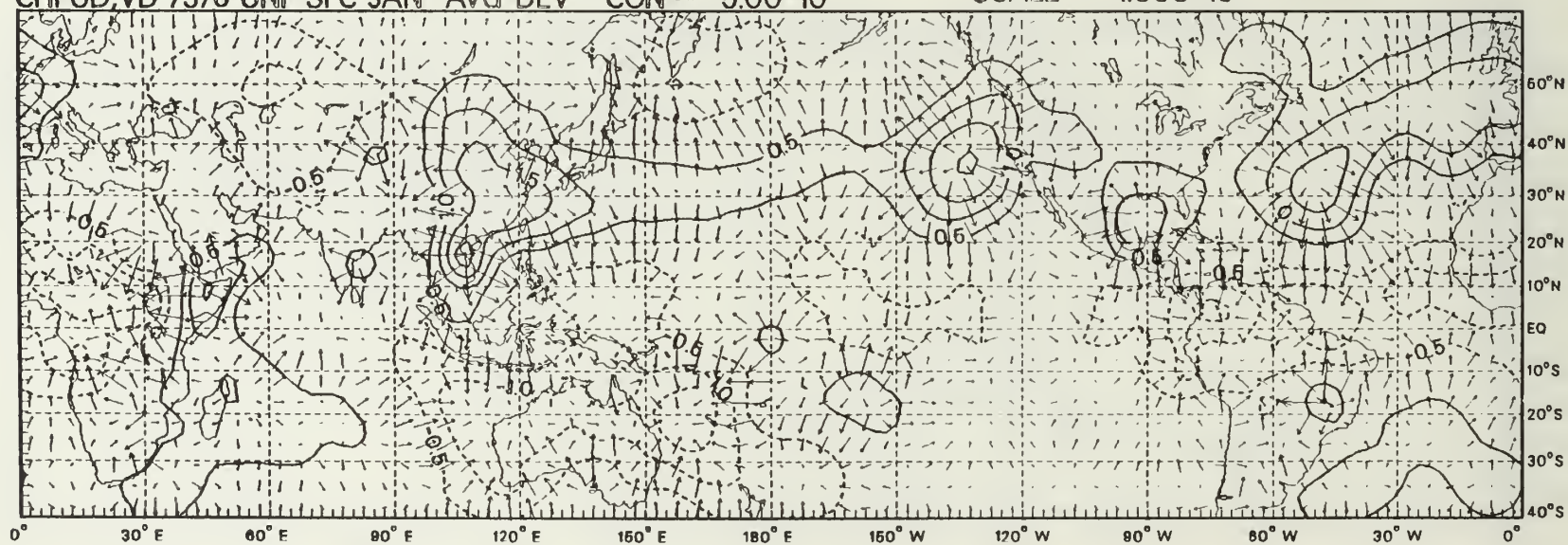
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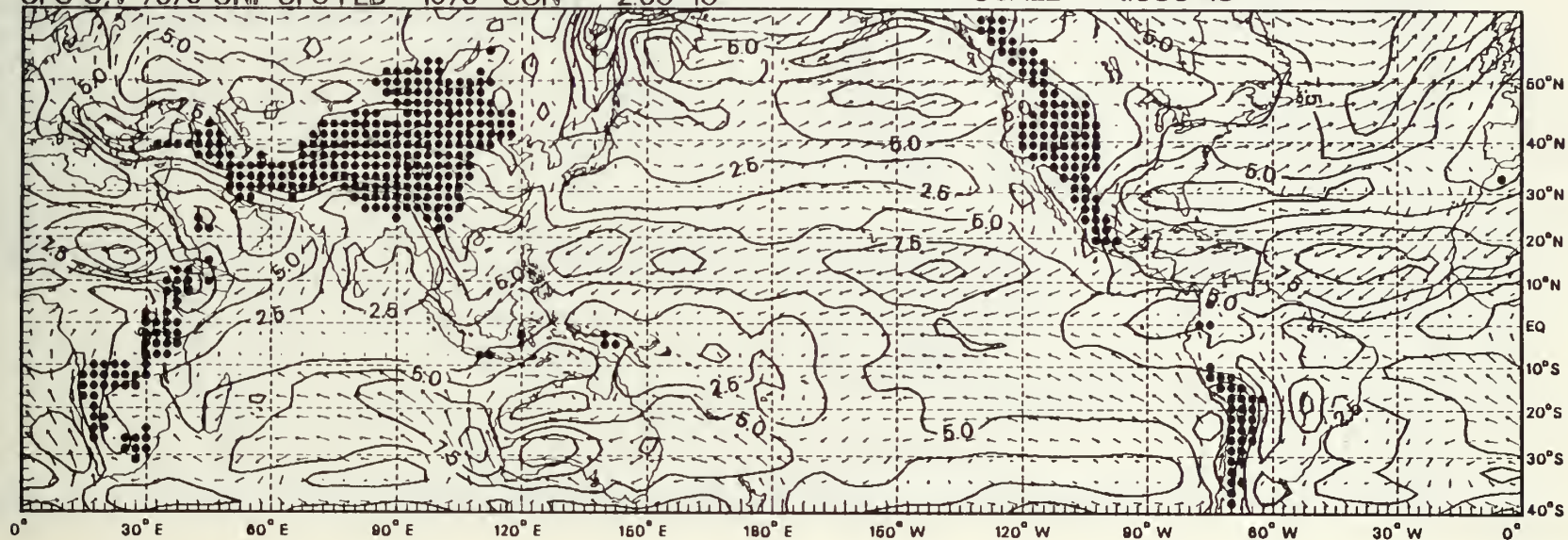
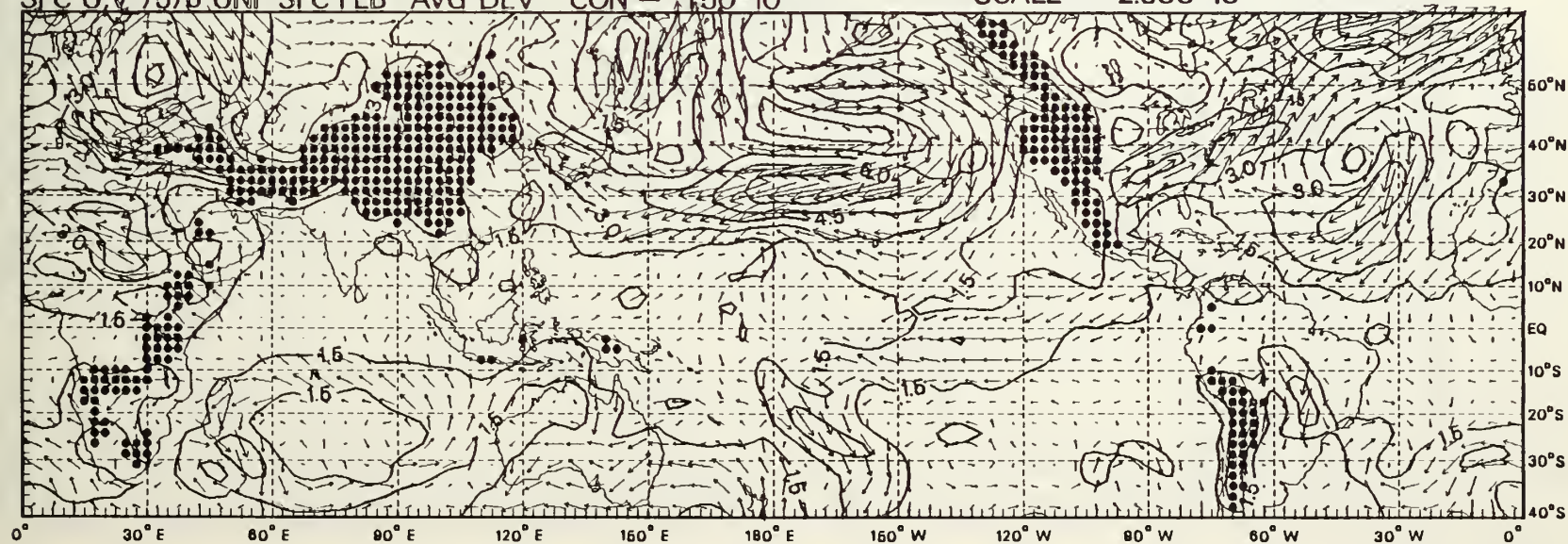
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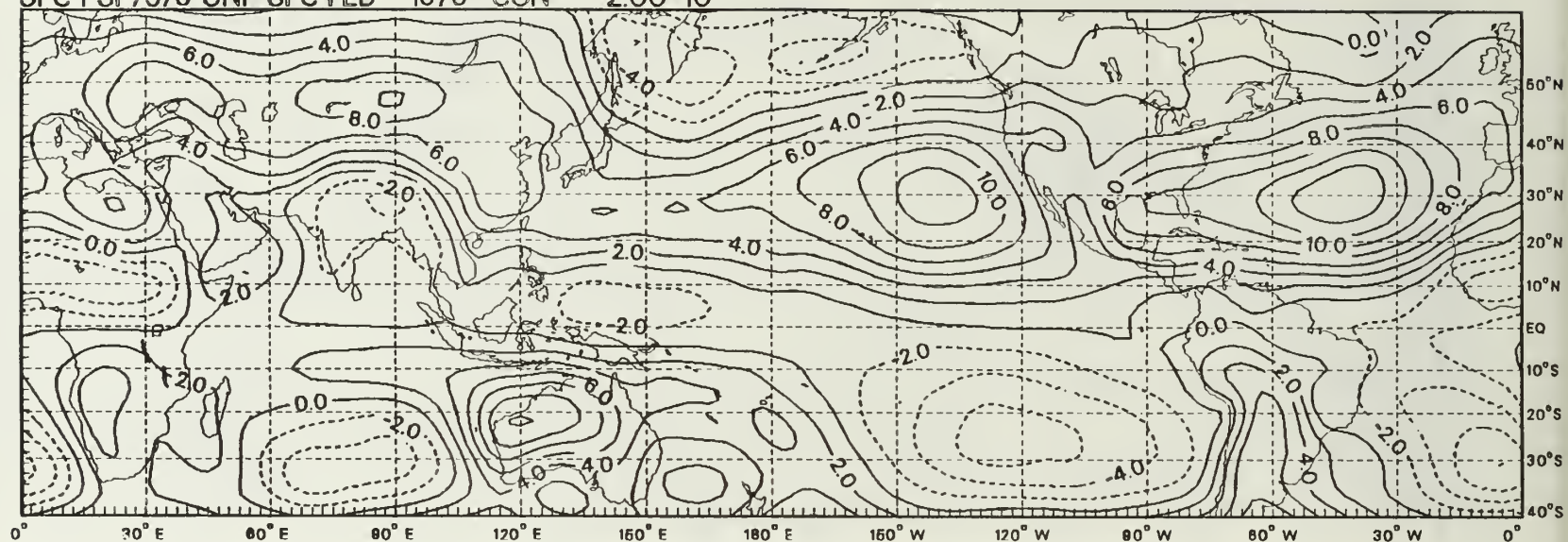


CHI UD,VD 7576 UNF SFC JAN 1976 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$  —CHI UD,VD 7576 UNF SFC JAN AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$  —

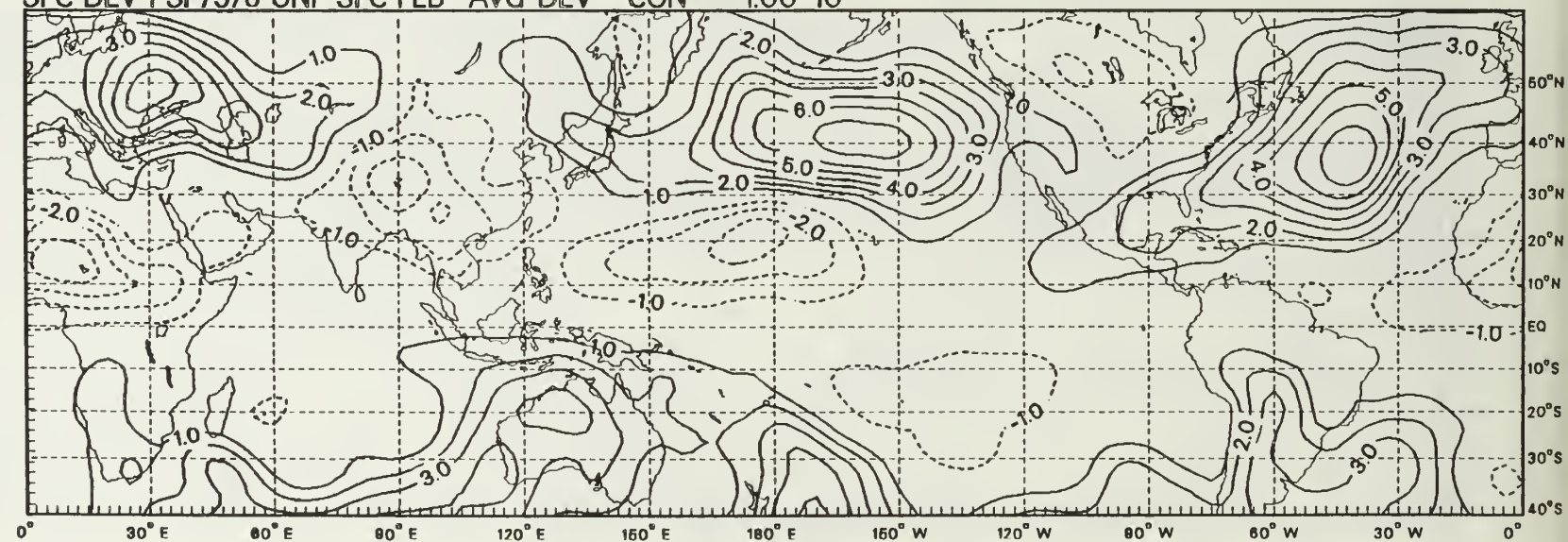


SFC U.V 7576 UNF SFC FEB 1976 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U.V 7576 UNF SFC FEB AVG DEV CON =  $1.50 \times 10^0$ SCALE =  $2.500 \times 10^0$  —

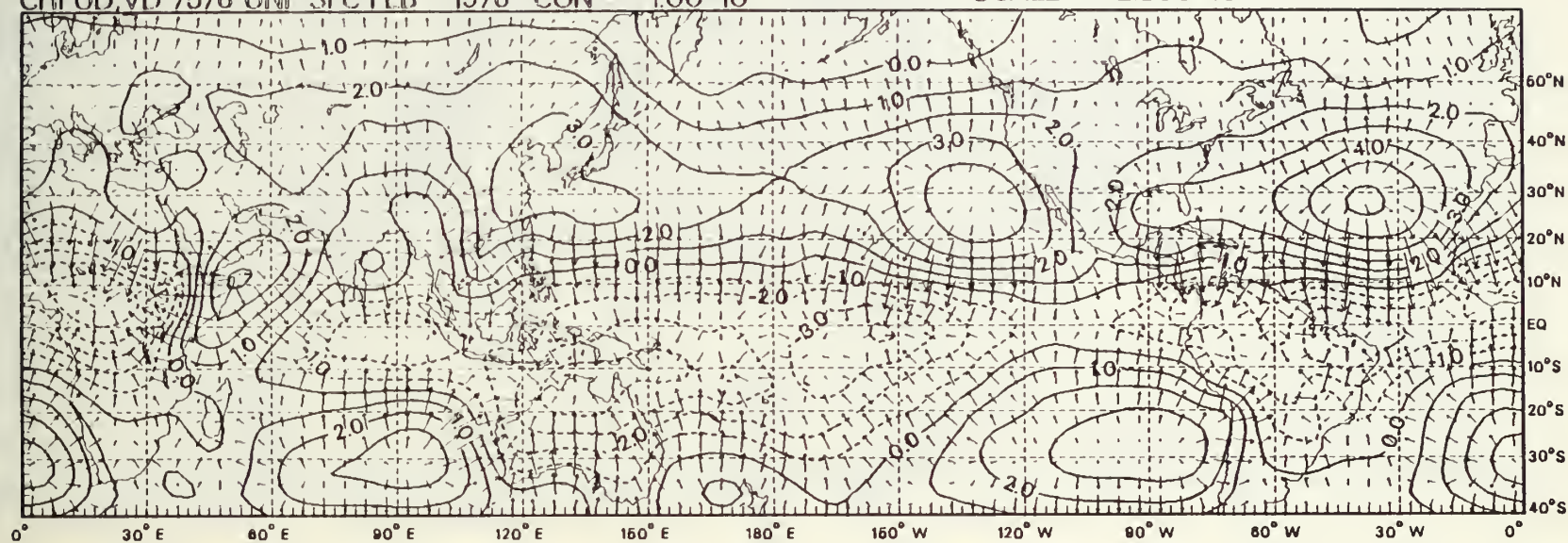
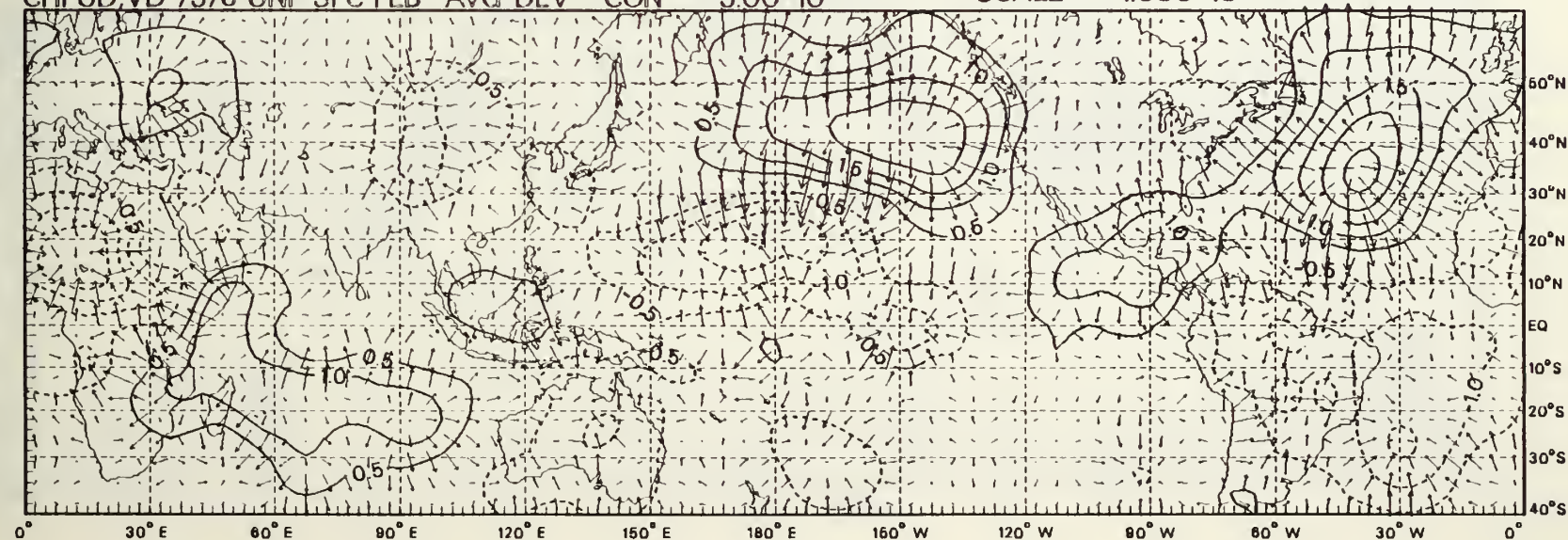
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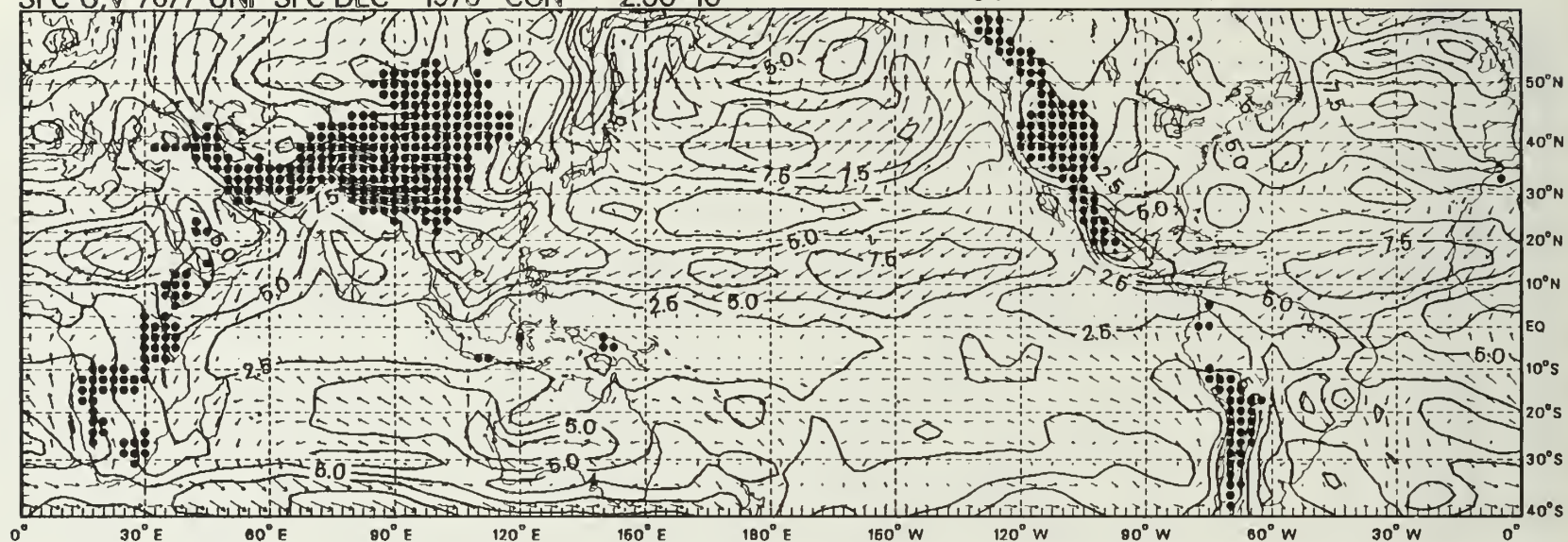
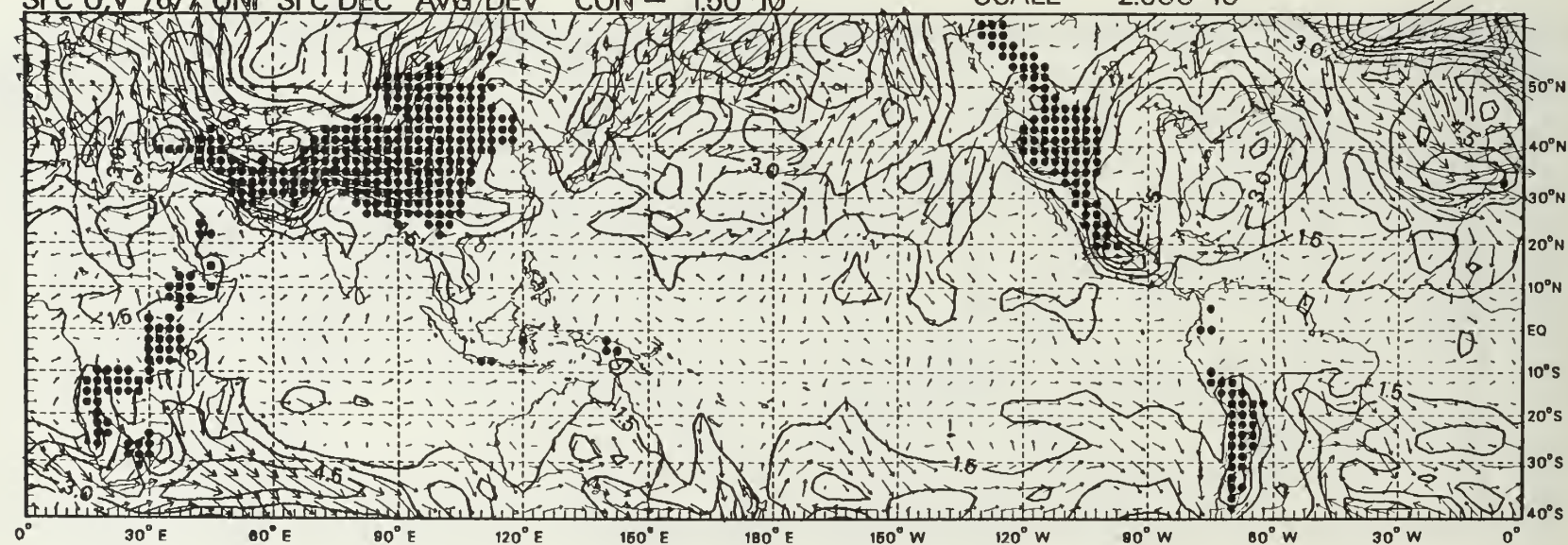
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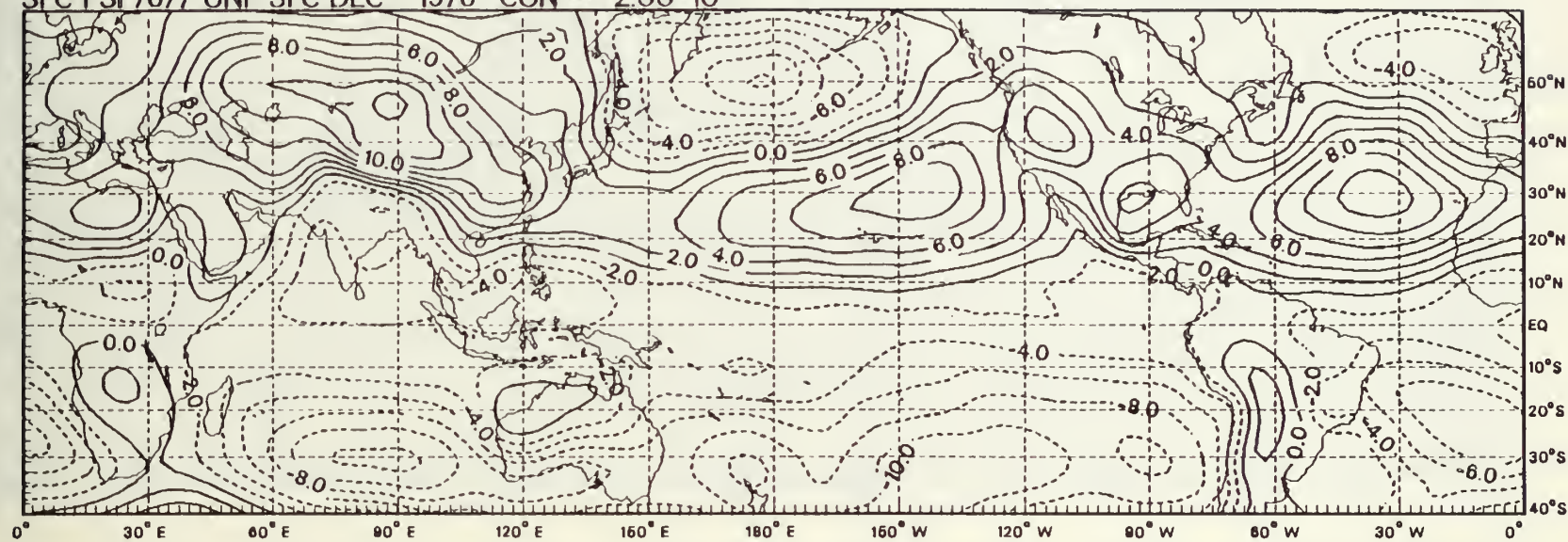
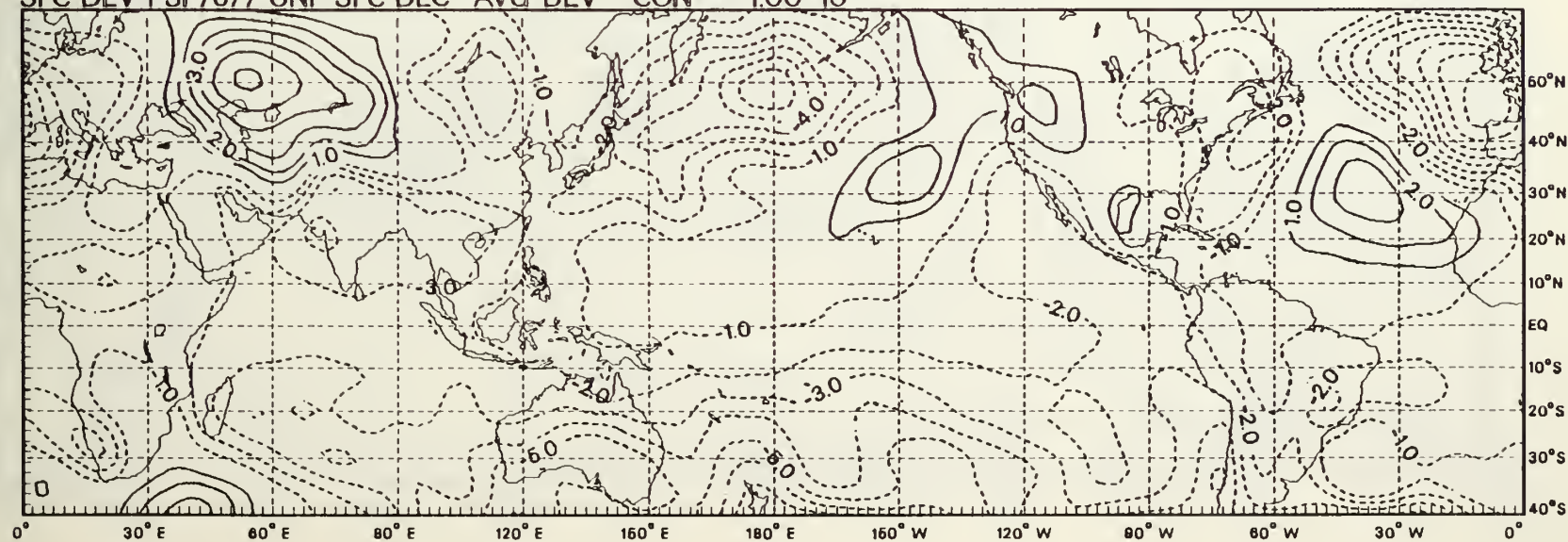




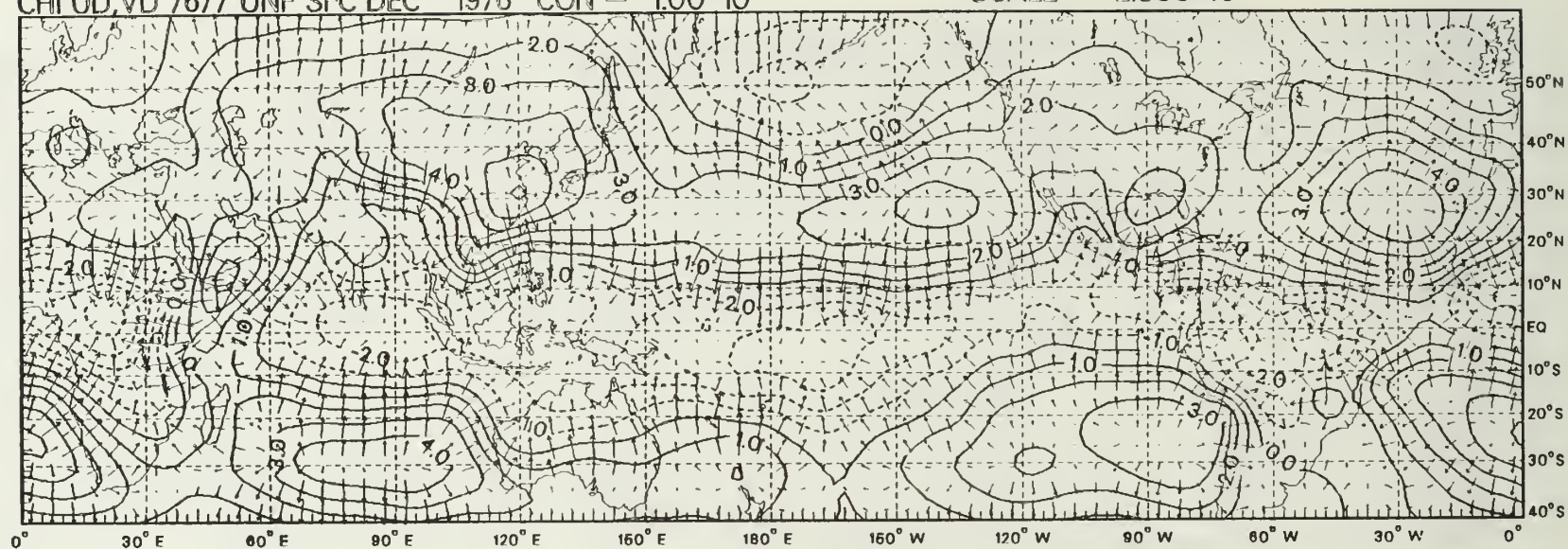
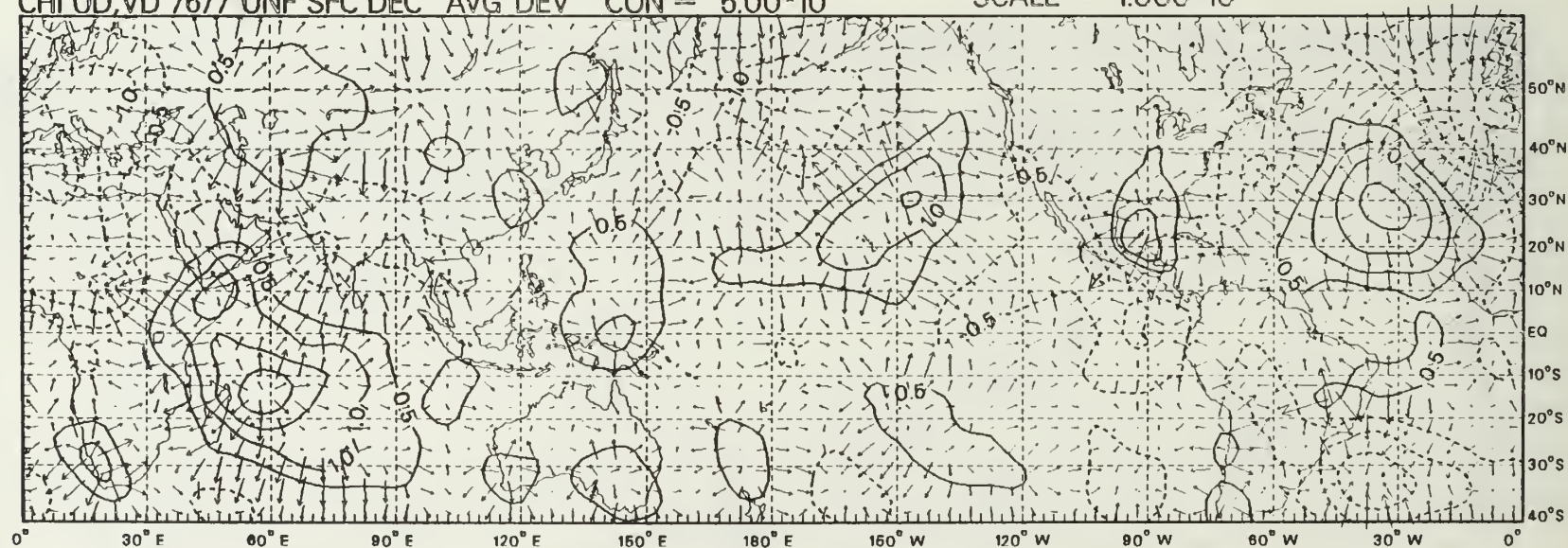
CHI UD, VD 7576 UNF SFC FEB 1976 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$  —CHI UD, VD 7576 UNF SFC FEB AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$  —



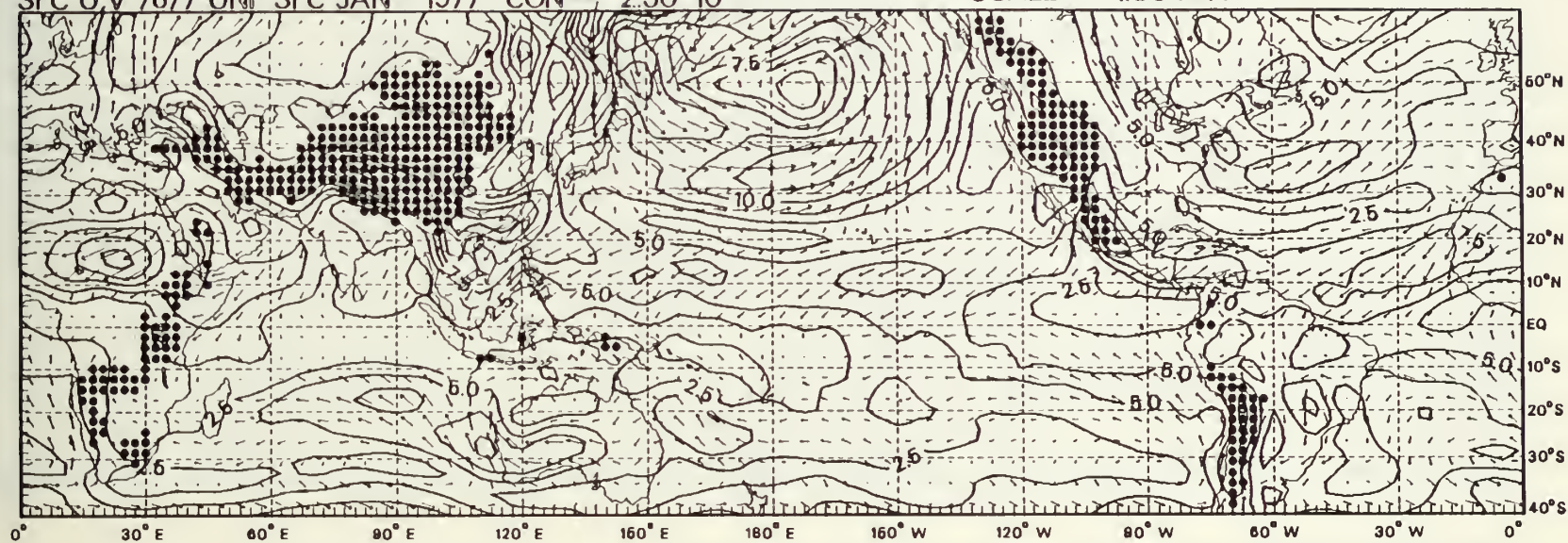
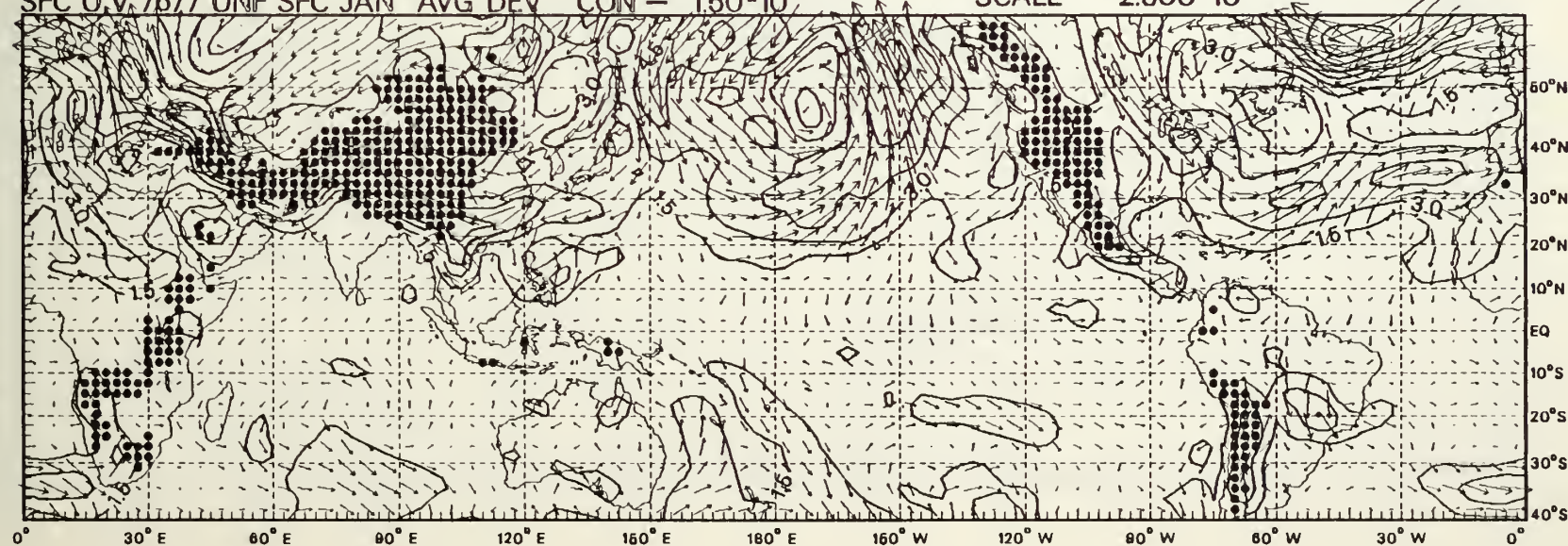
SFC U,V 7677 UNF SFC DEC 1976 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U,V 7677 UNF SFC DEC AVG/DEV CON =  $1.50 \times 10^0$ SCALE =  $2.500 \times 10^0$  —

SFC PSI 7677 UNF SFC DEC 1976 CON =  $2.00 \times 10^0$ SFC DEV PSI 7677 UNF SFC DEC AVG DEV CON =  $1.00 \times 10^0$ 

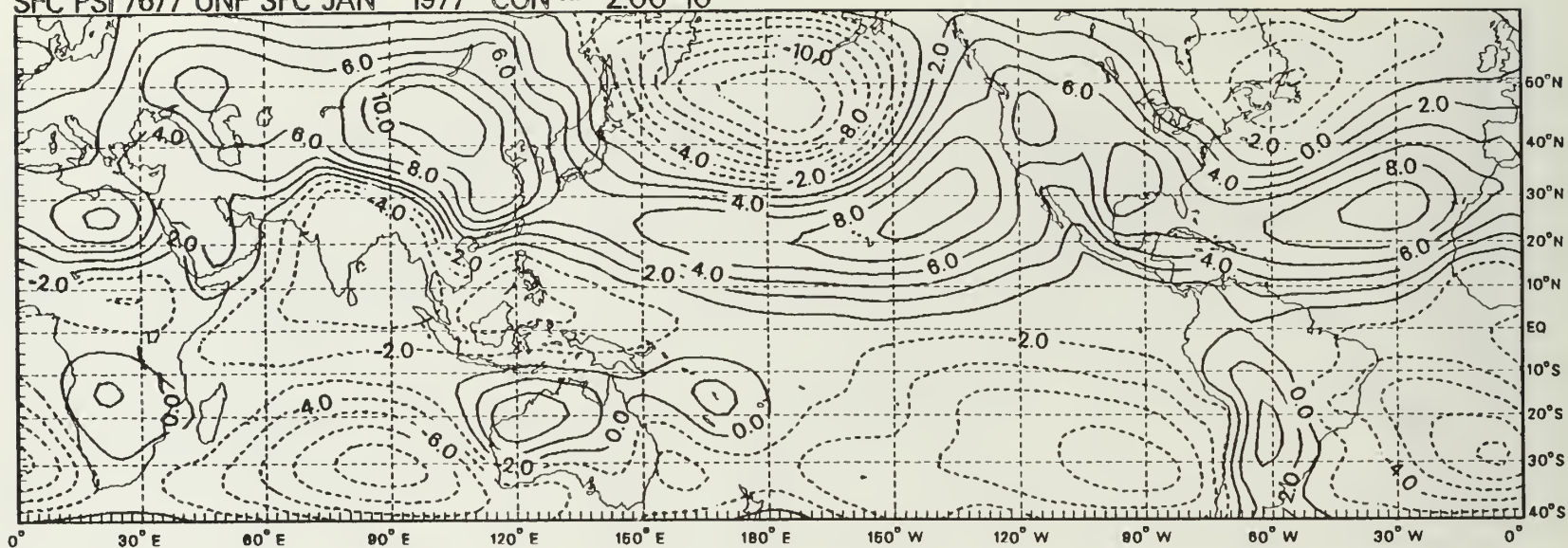


CHI UD,VD 7677 UNF SFC DEC 1976 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$  —CHI UD,VD 7677 UNF SFC DEC AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$  —

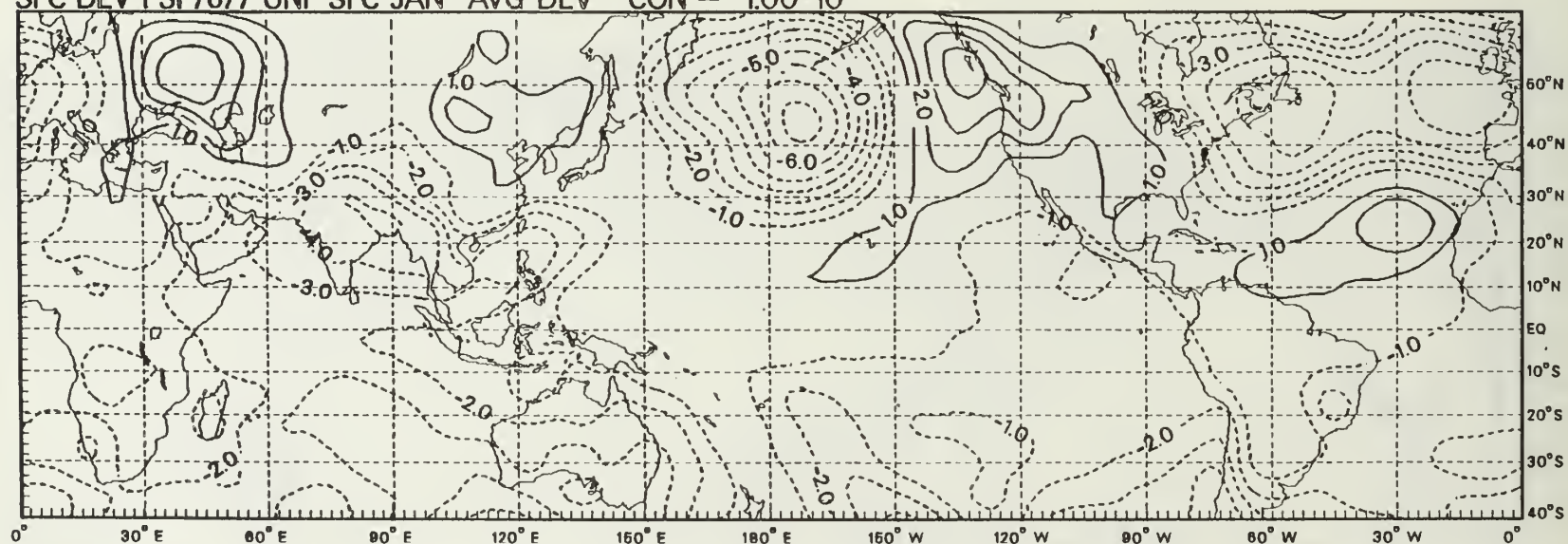


SFC U.V. 7677 UNF SFC JAN 1977 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U.V. 7677 UNF SFC JAN AVG DEV CON =  $1.50 \times 10^0$ SCALE =  $2.500 \times 10^0$  —

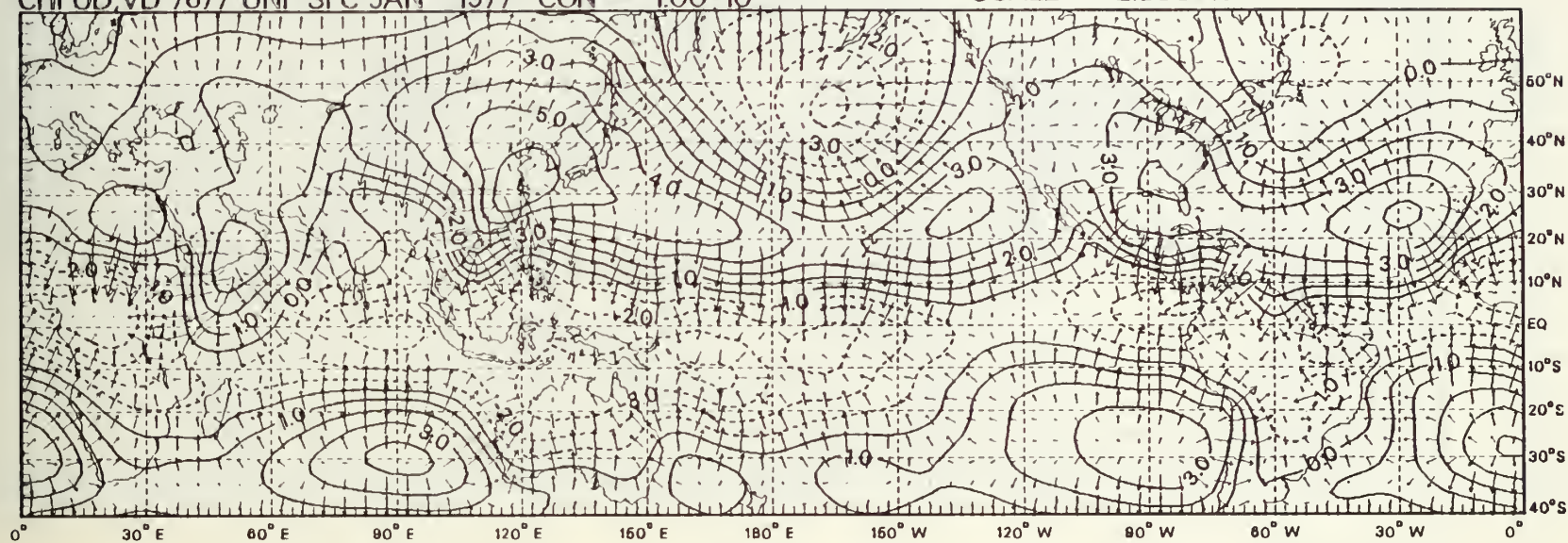
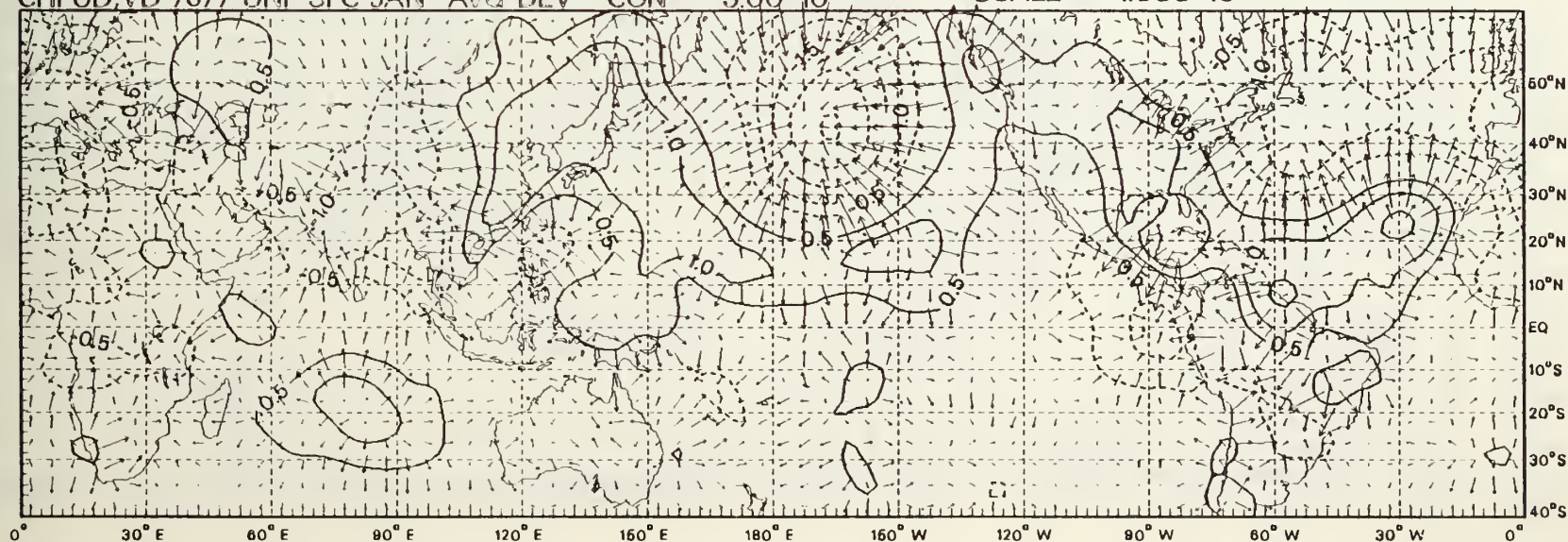
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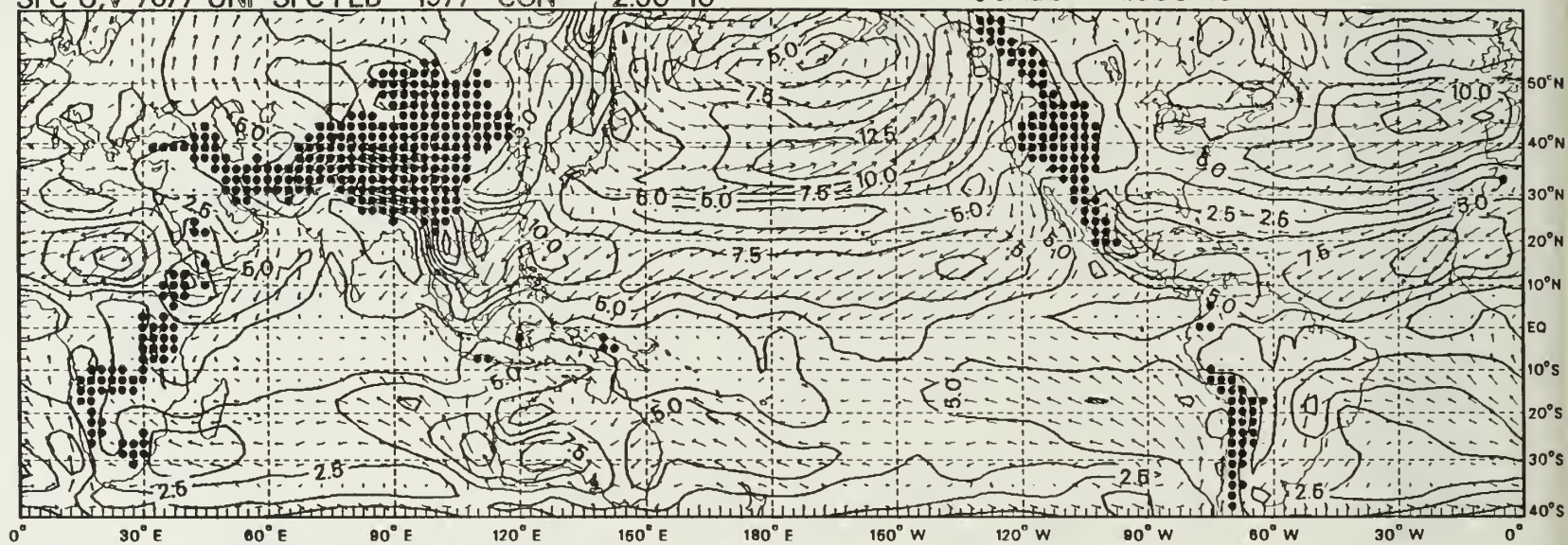
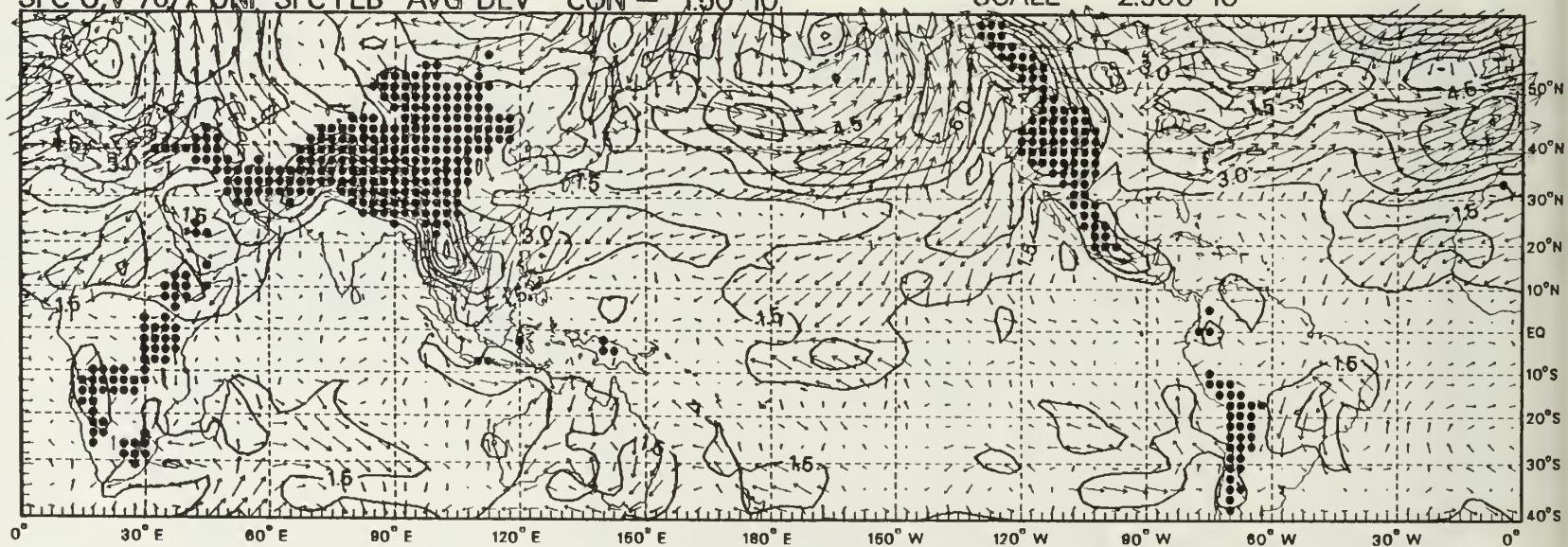
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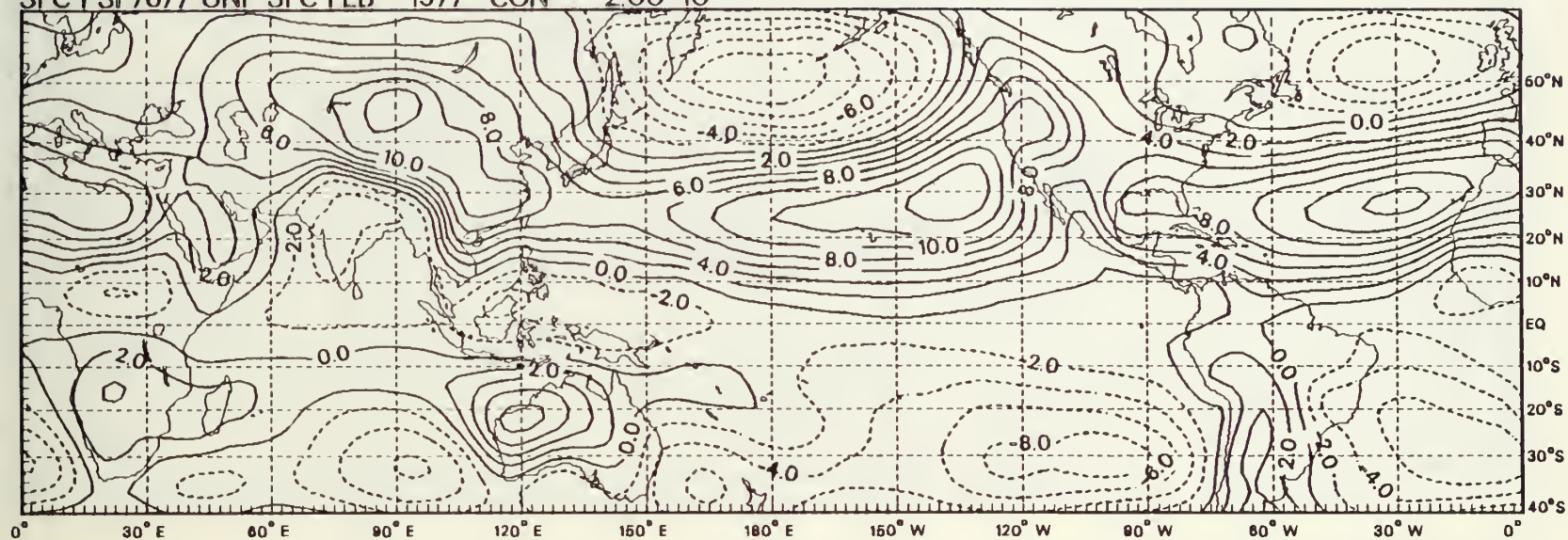
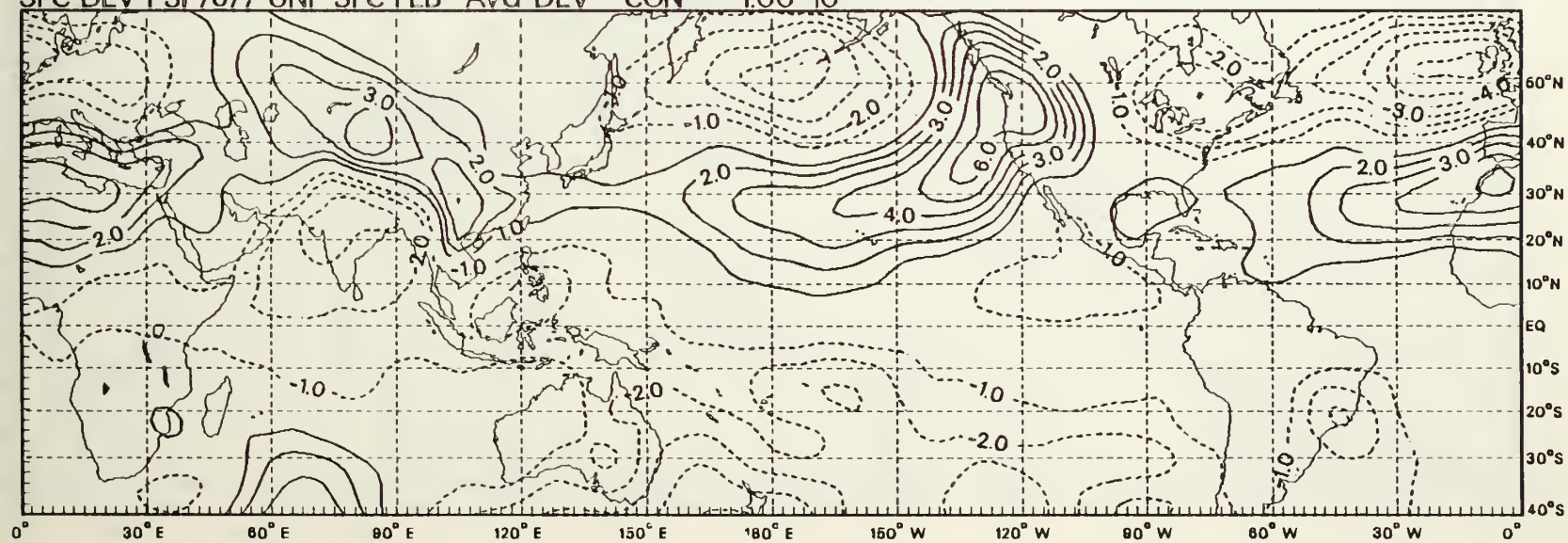


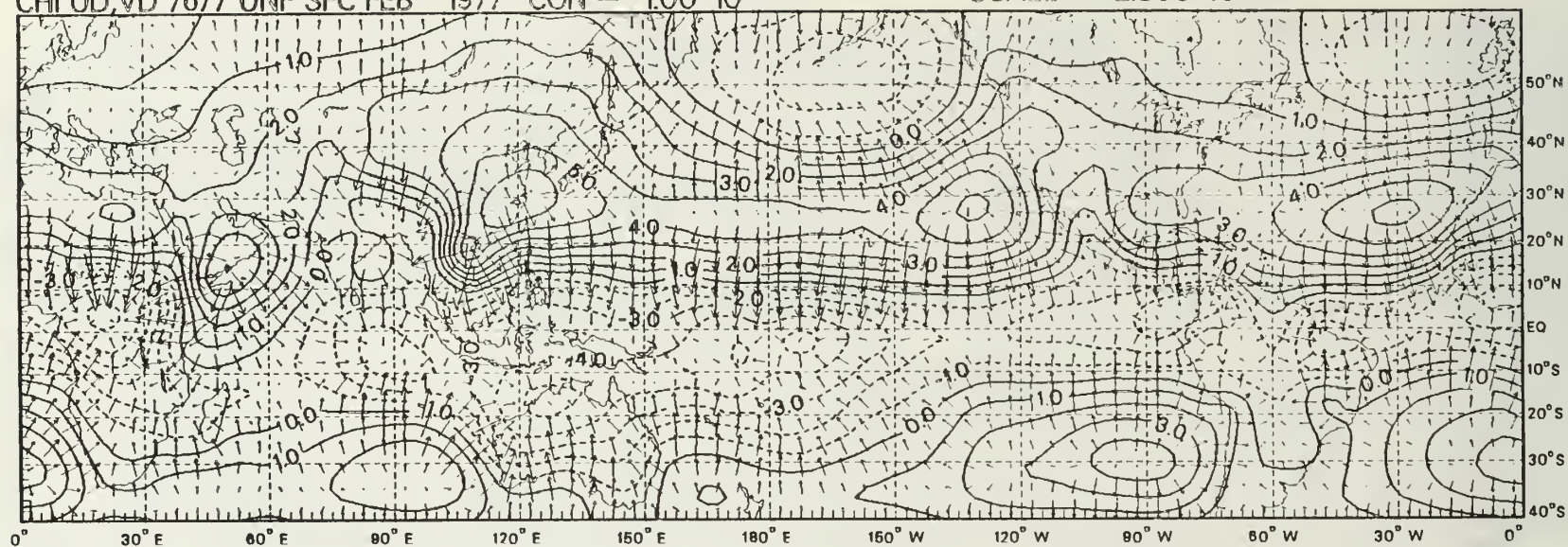
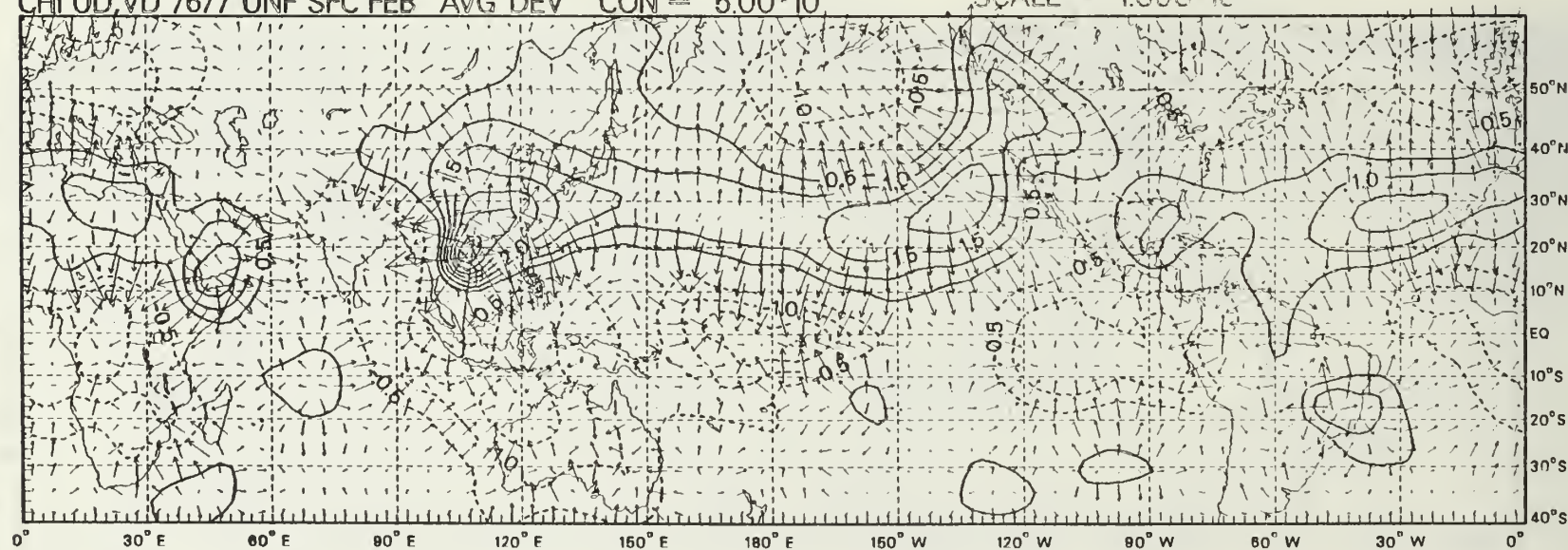
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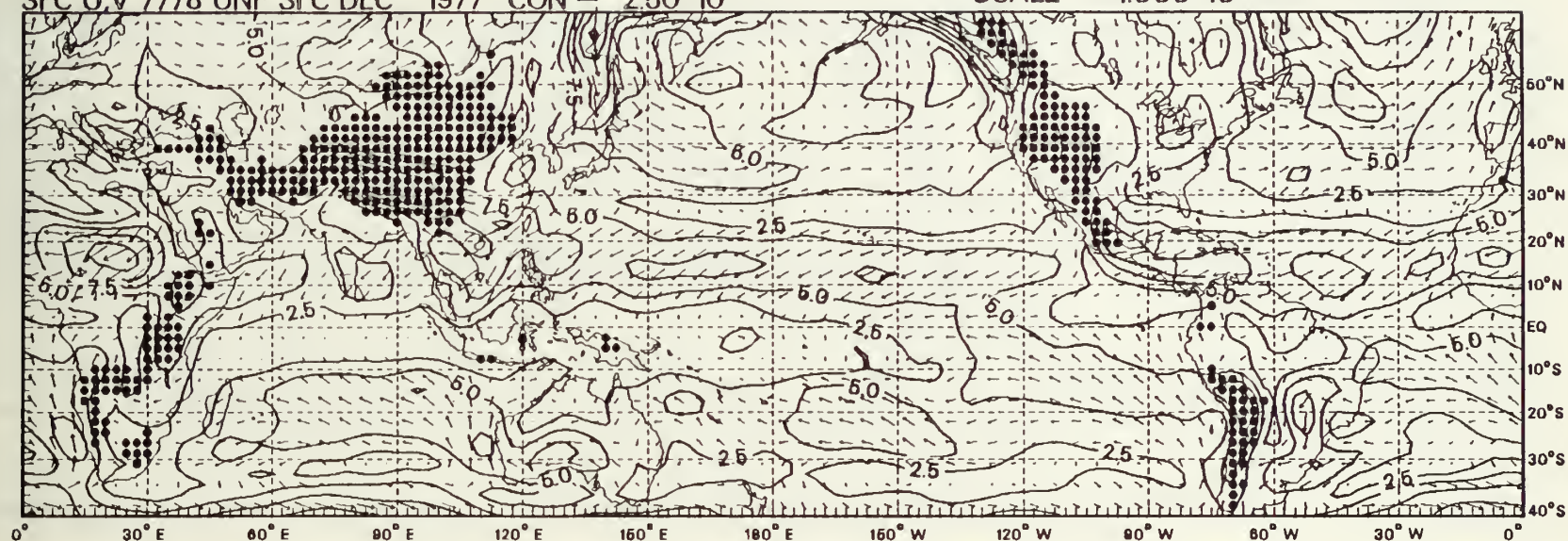
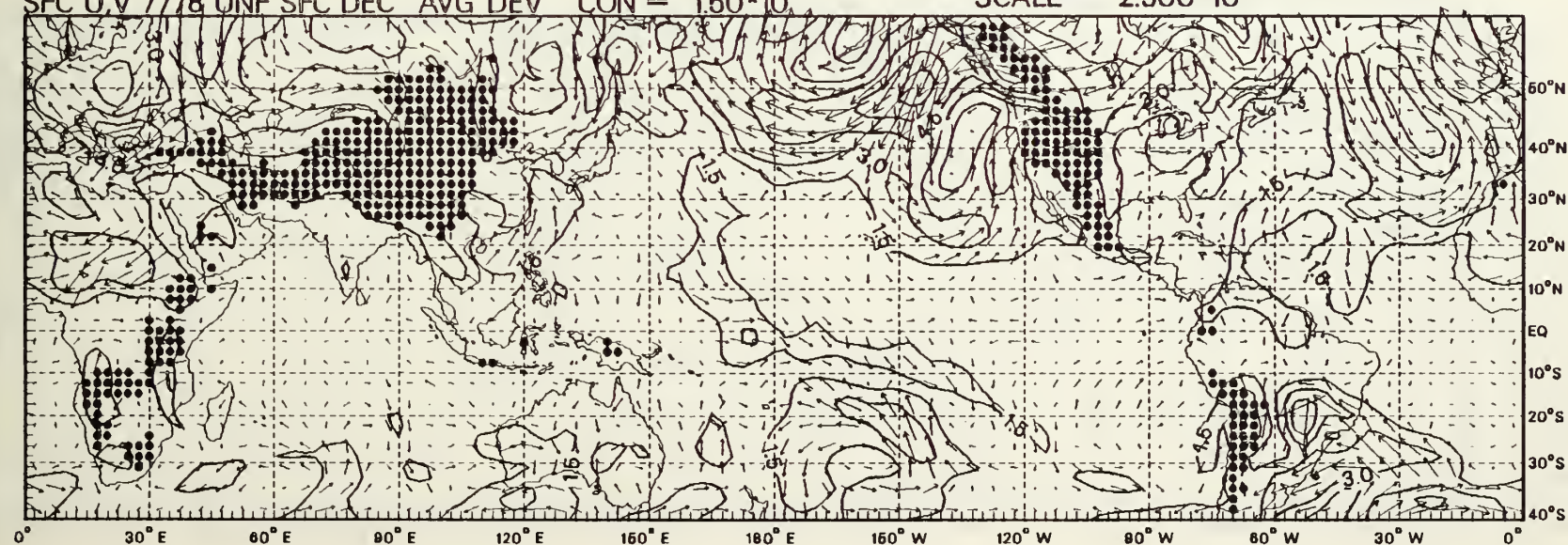
SFC U,V 7677 UNF SFC FEB 1977 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U,V 7677 UNF SFC FEB AVG DEV CON =  $1.50 \times 10^0$ SCALE =  $2.500 \times 10^0$  —

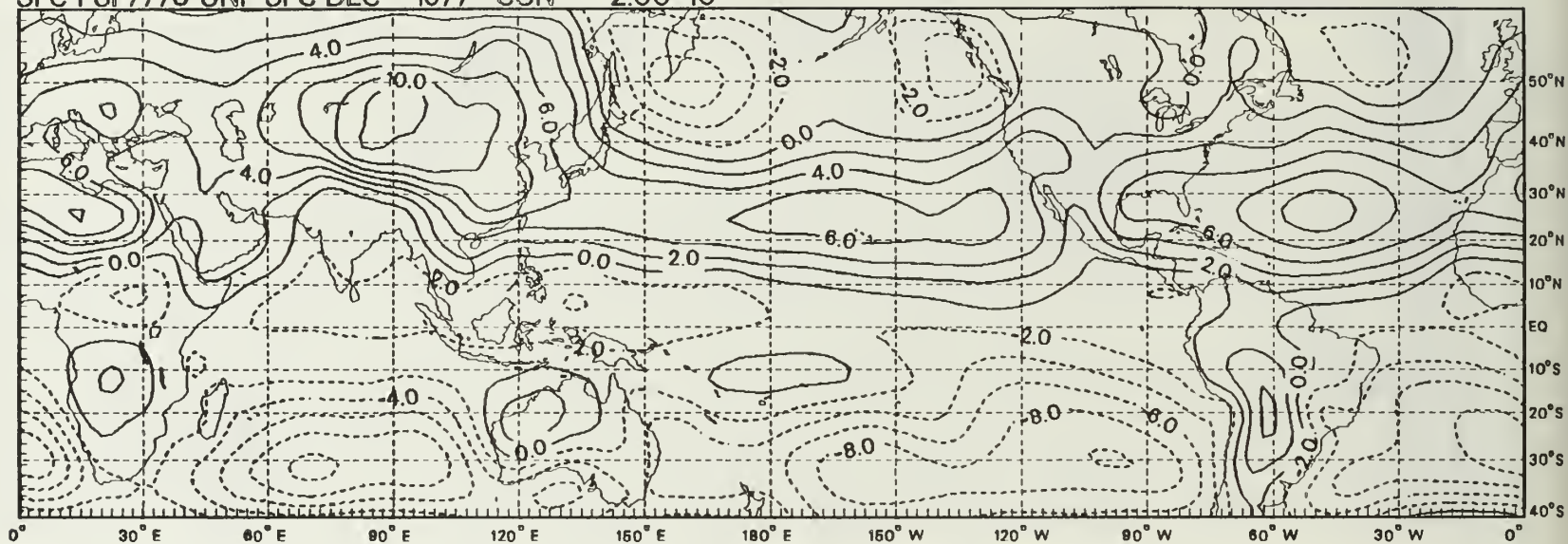
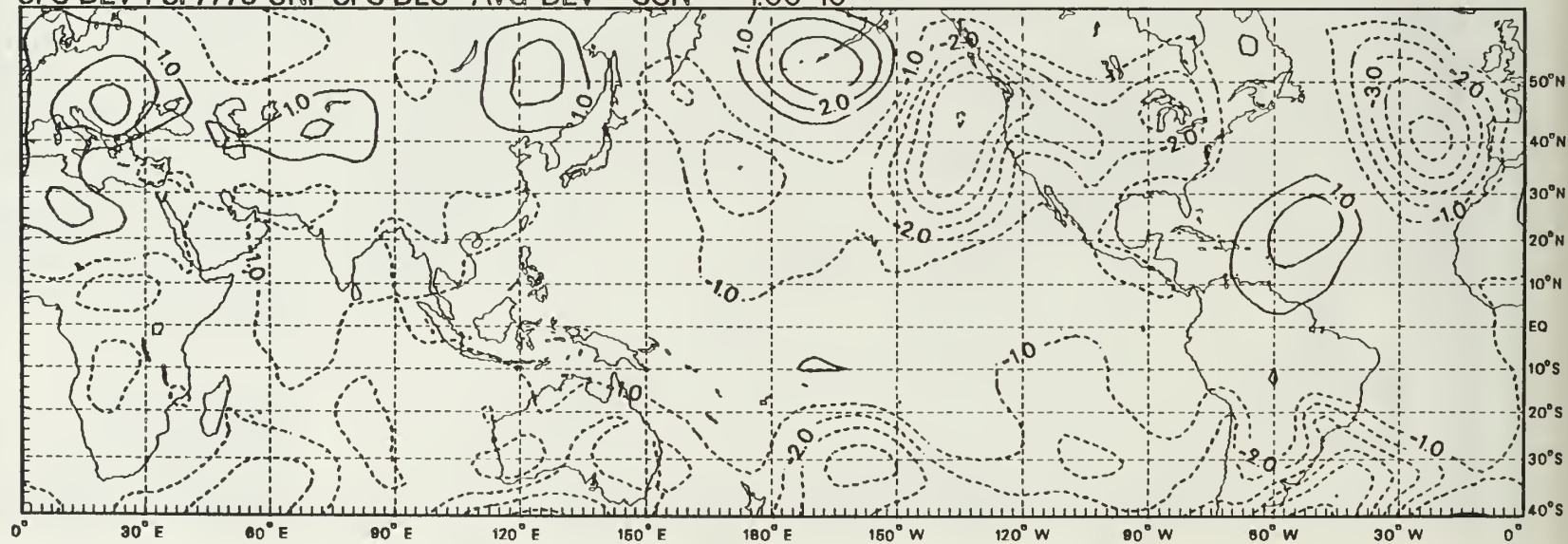


SFC PSI 7677 UNF SFC FEB 1977 CON =  $2.00 \times 10^0$ SFC DEV PSI 7677 UNF SFC FEB AVG DEV CON =  $1.00 \times 10^0$ 

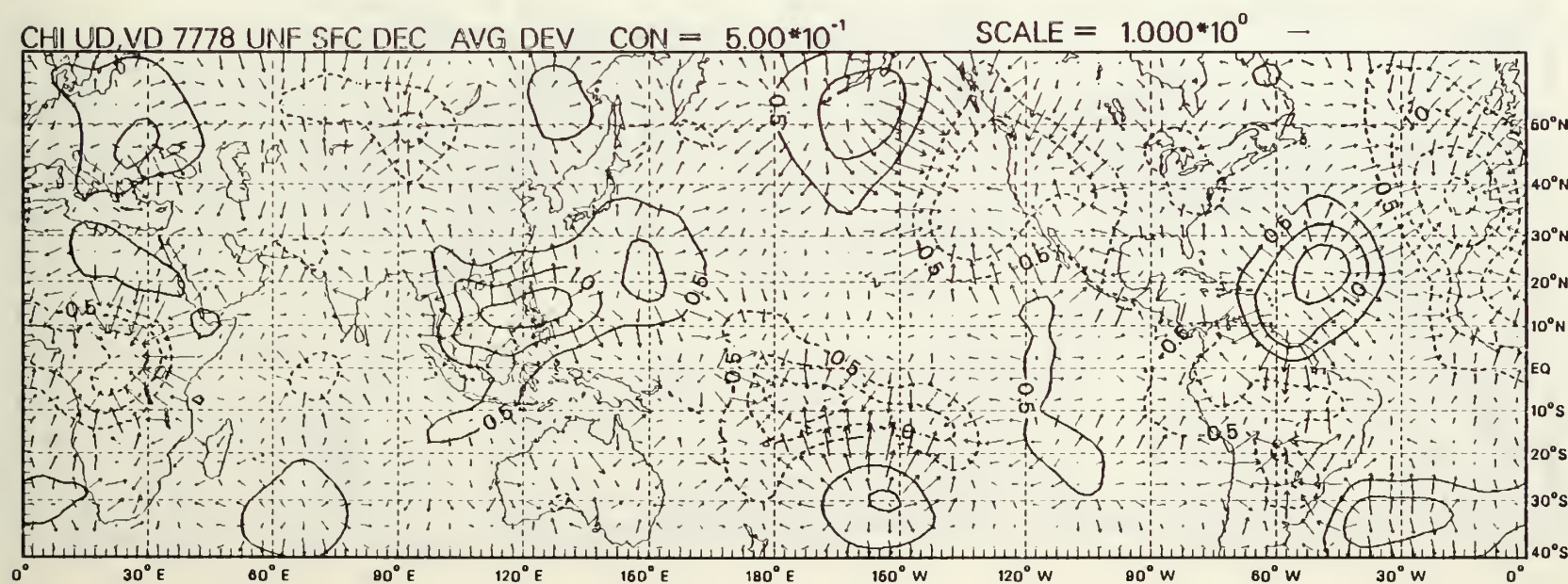
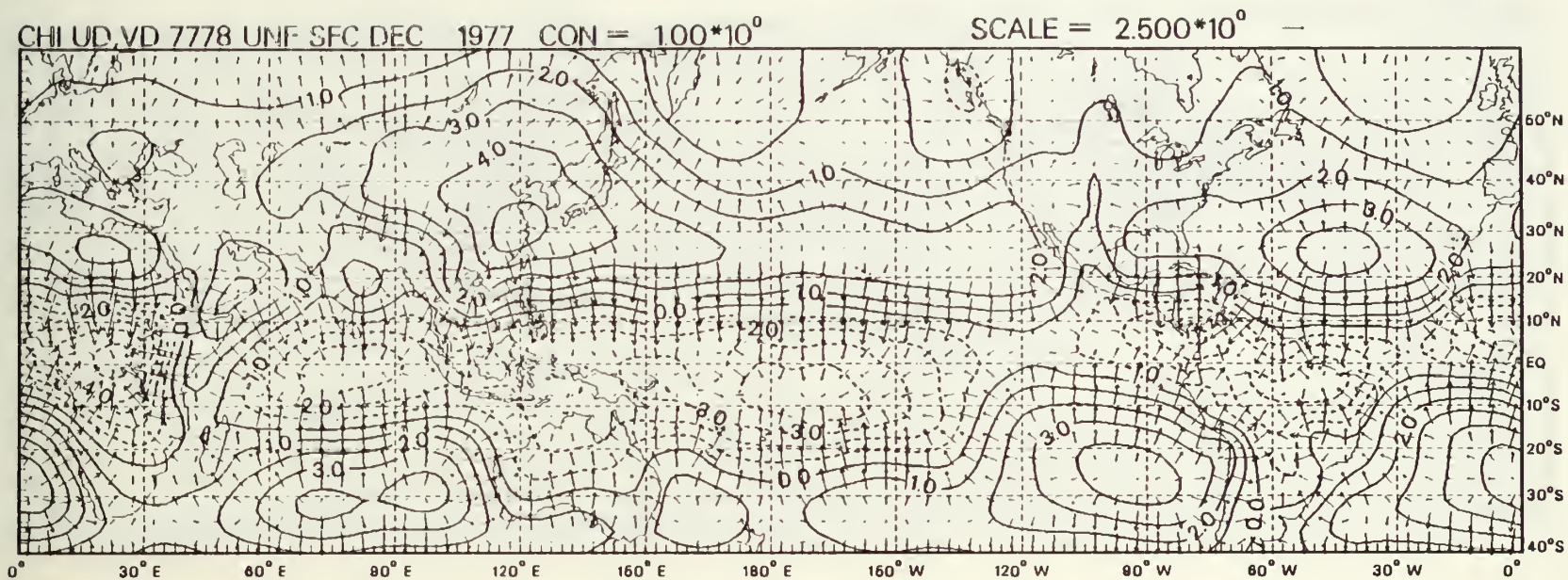
CHI UD, VD 7677 UNF SFC FEB 1977 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$  —CHI UD, VD 7677 UNF SFC FEB AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$  —



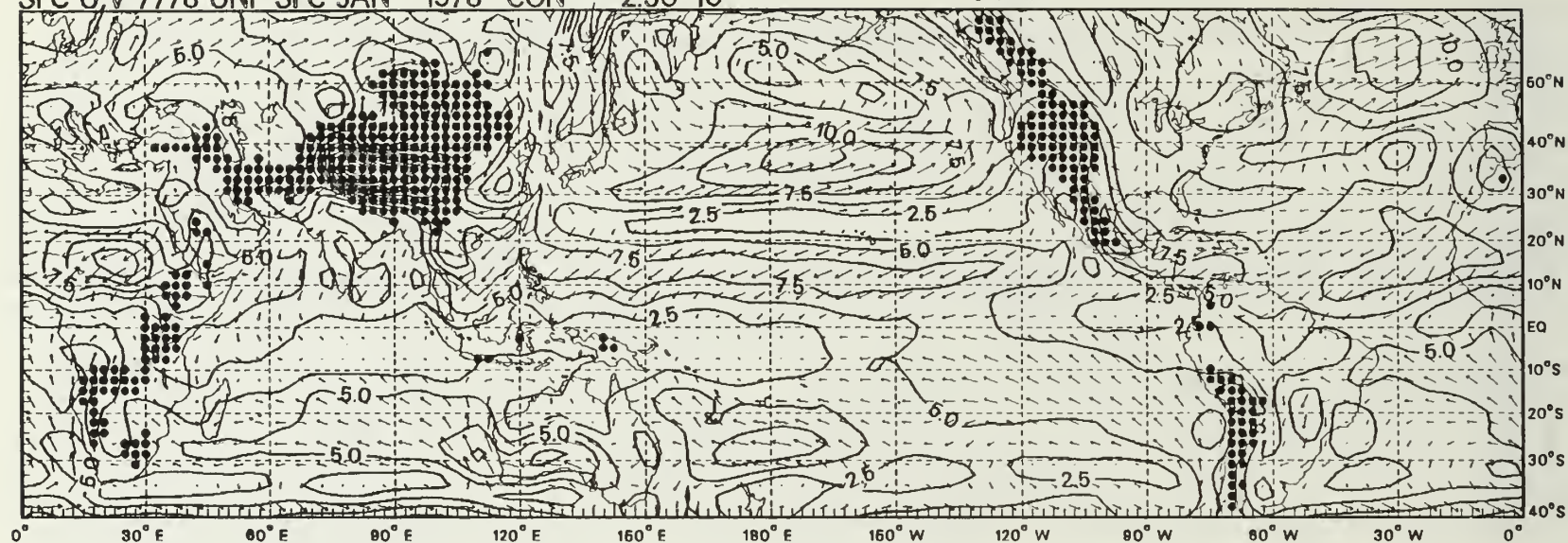
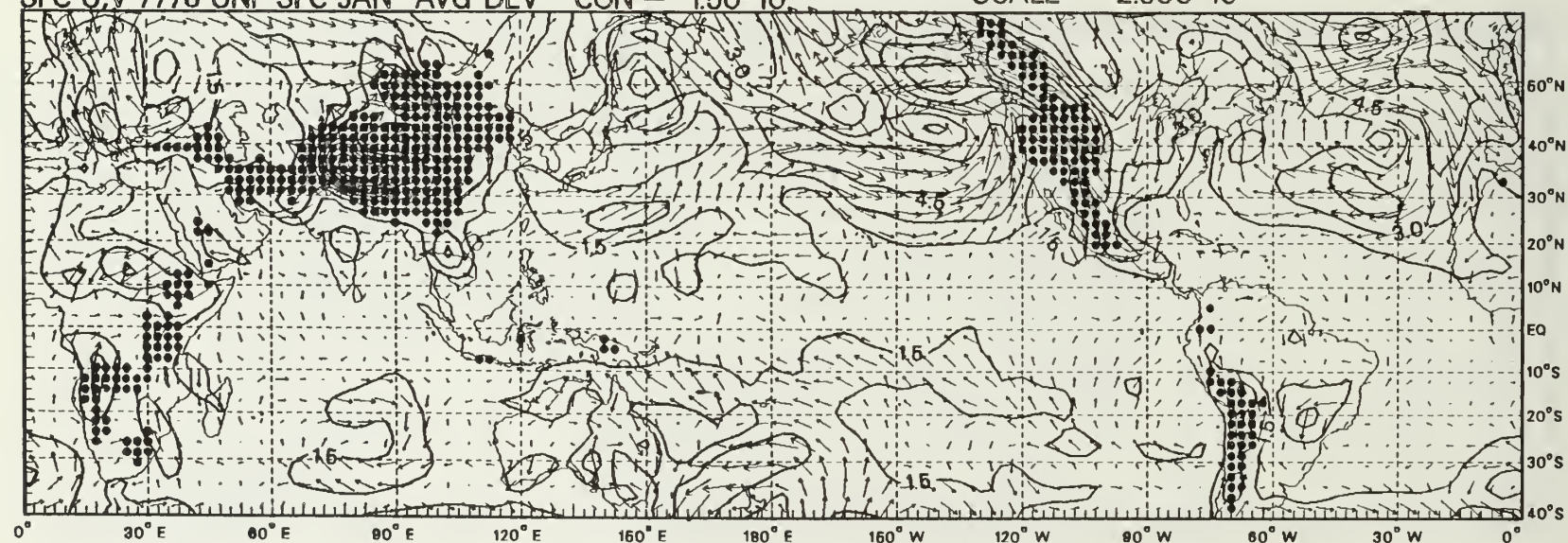
SFC U.V 7778 UNF SFC DEC 1977 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U.V 7778 UNF SFC DEC AVG DEV CON =  $1.50 \times 10^0$ SCALE =  $2.500 \times 10^0$  —

SFC PSI 7778 UNF SFC DEC 1977 CON =  $2.00 \times 10^0$ SFC DEV PSI 7778 UNF SFC DEC AVG DEV CON =  $1.00 \times 10^0$ 



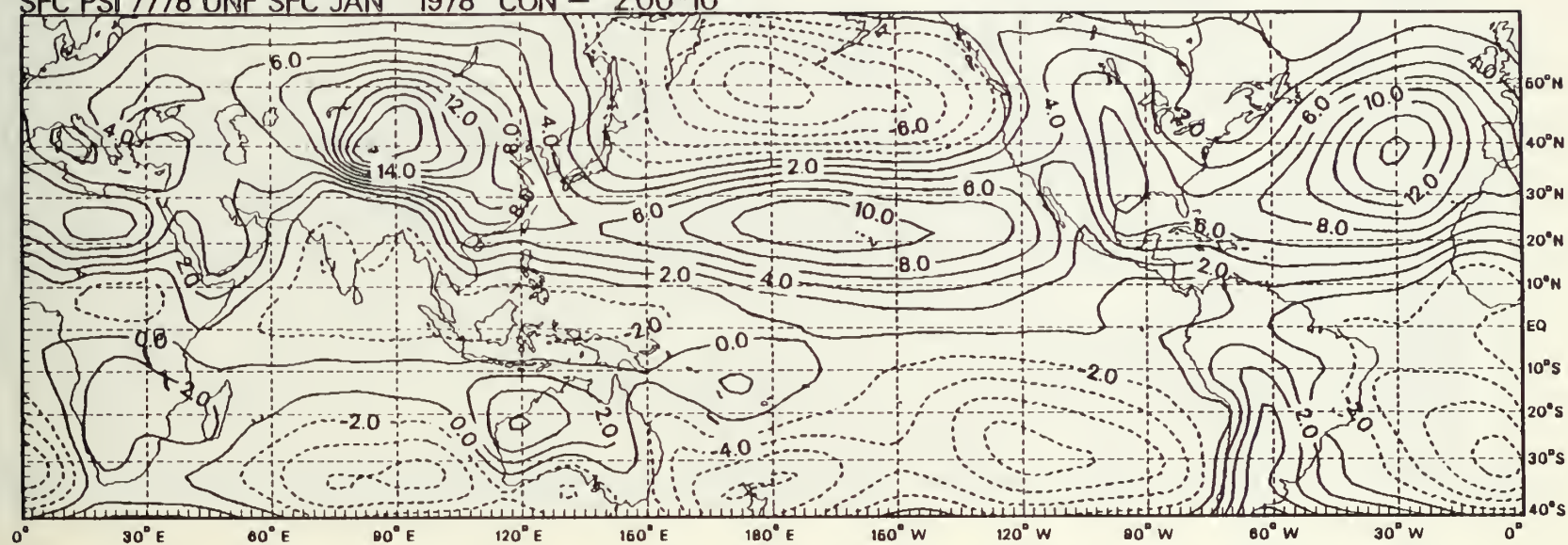




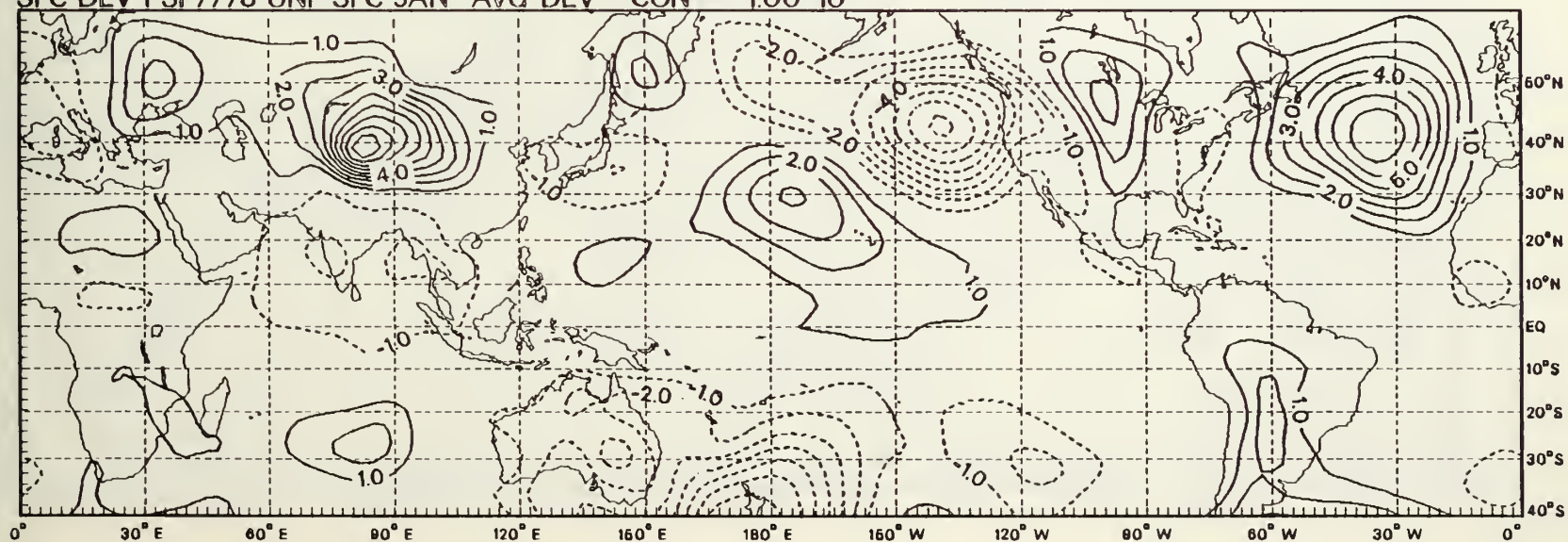
SFC U.V 7778 UNF SFC JAN 1978 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U.V 7778 UNF SFC JAN AVG DEV CON =  $1.50 \times 10^0$ SCALE =  $2.500 \times 10^0$  —

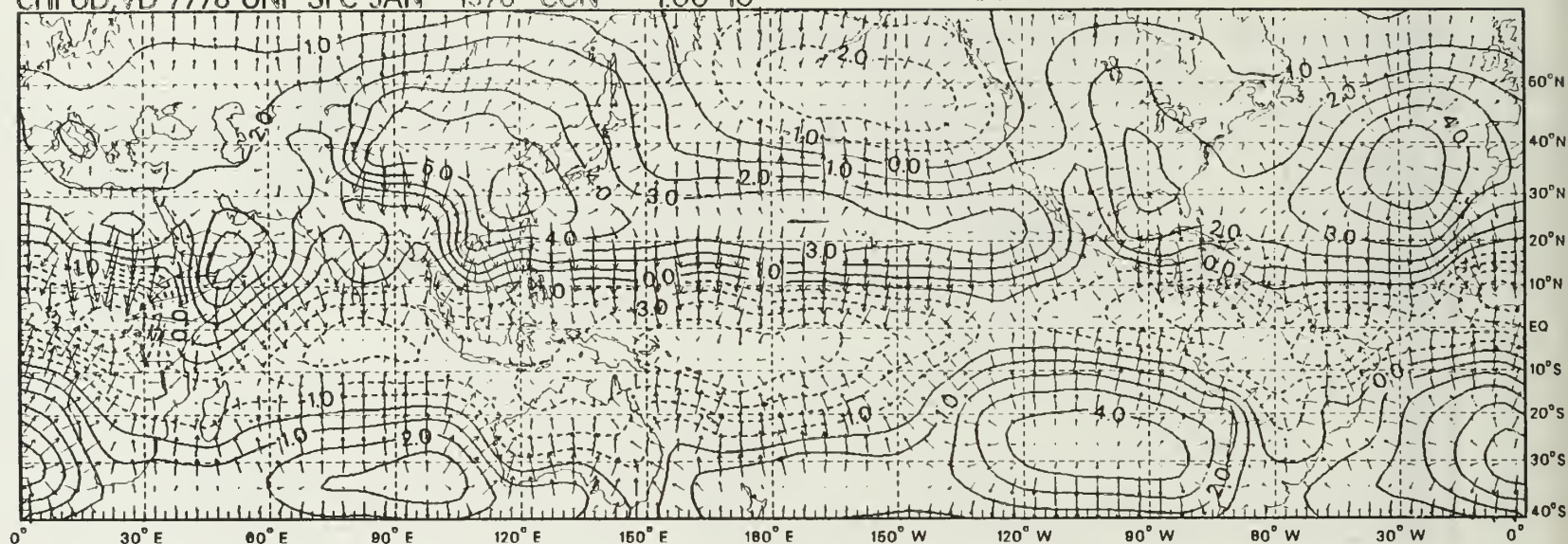
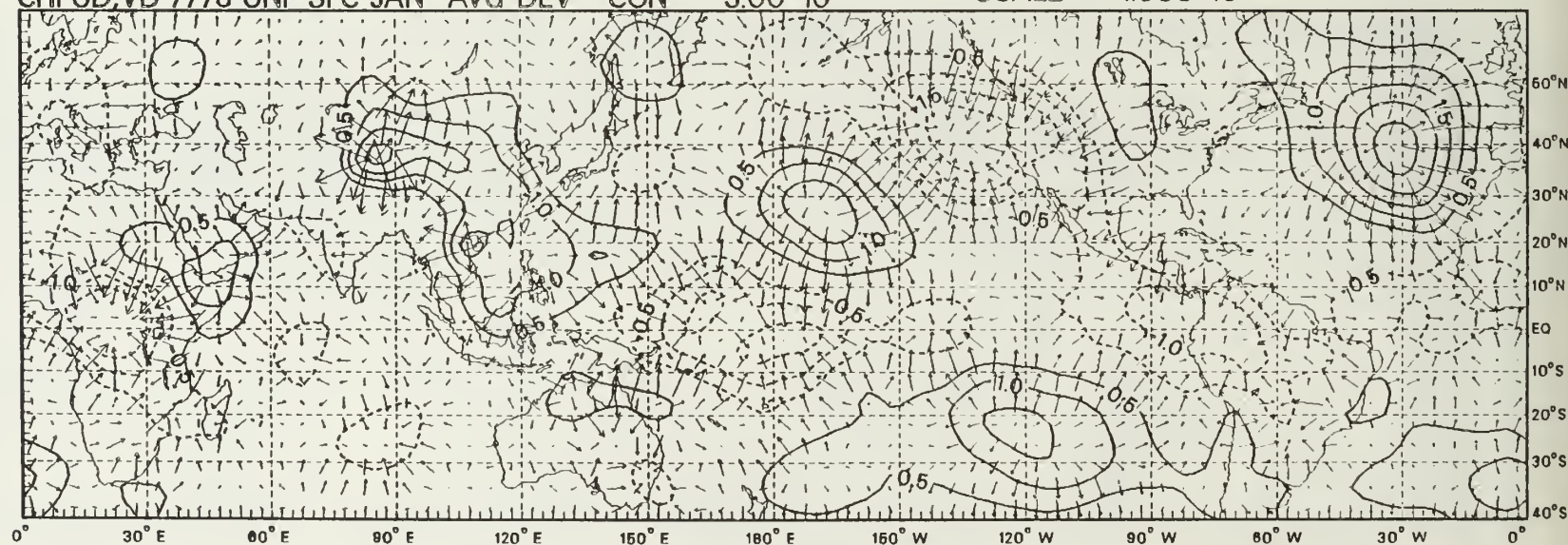


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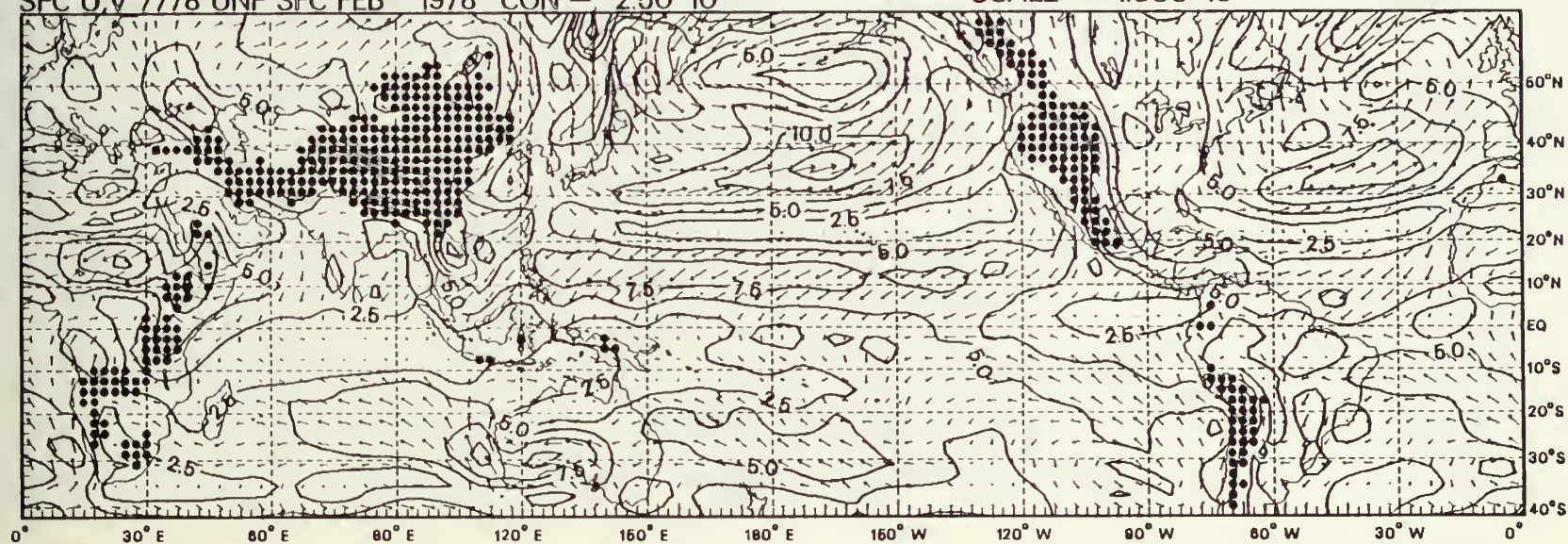
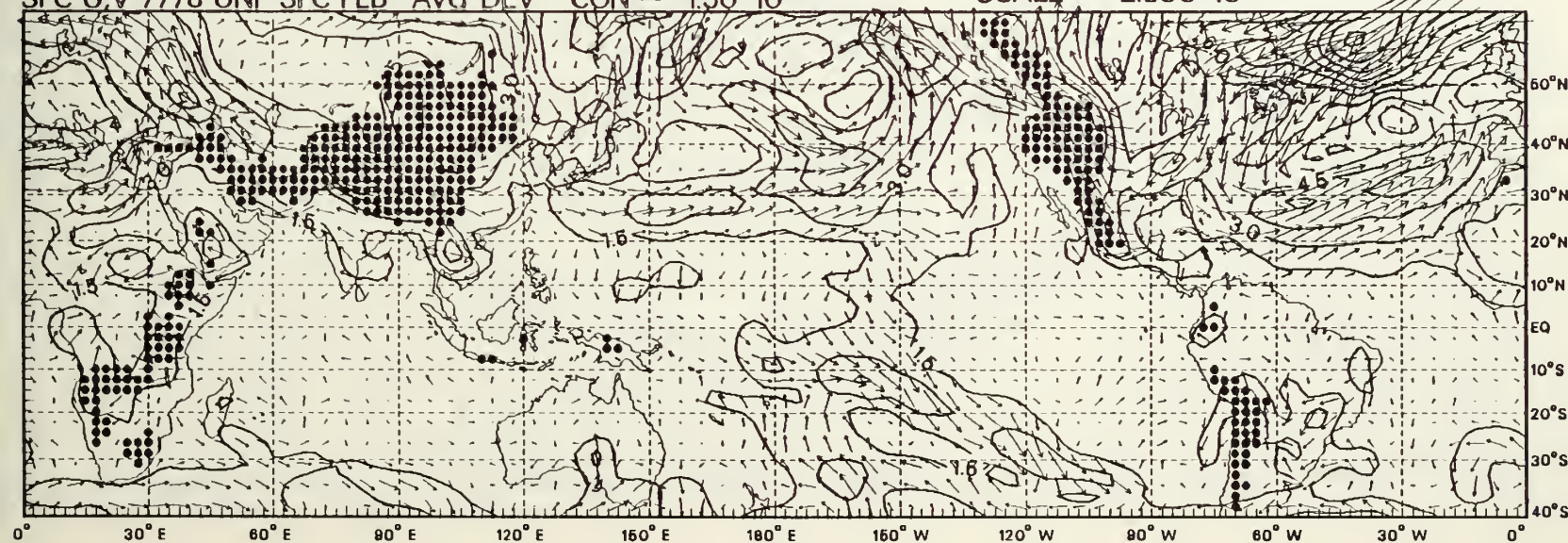


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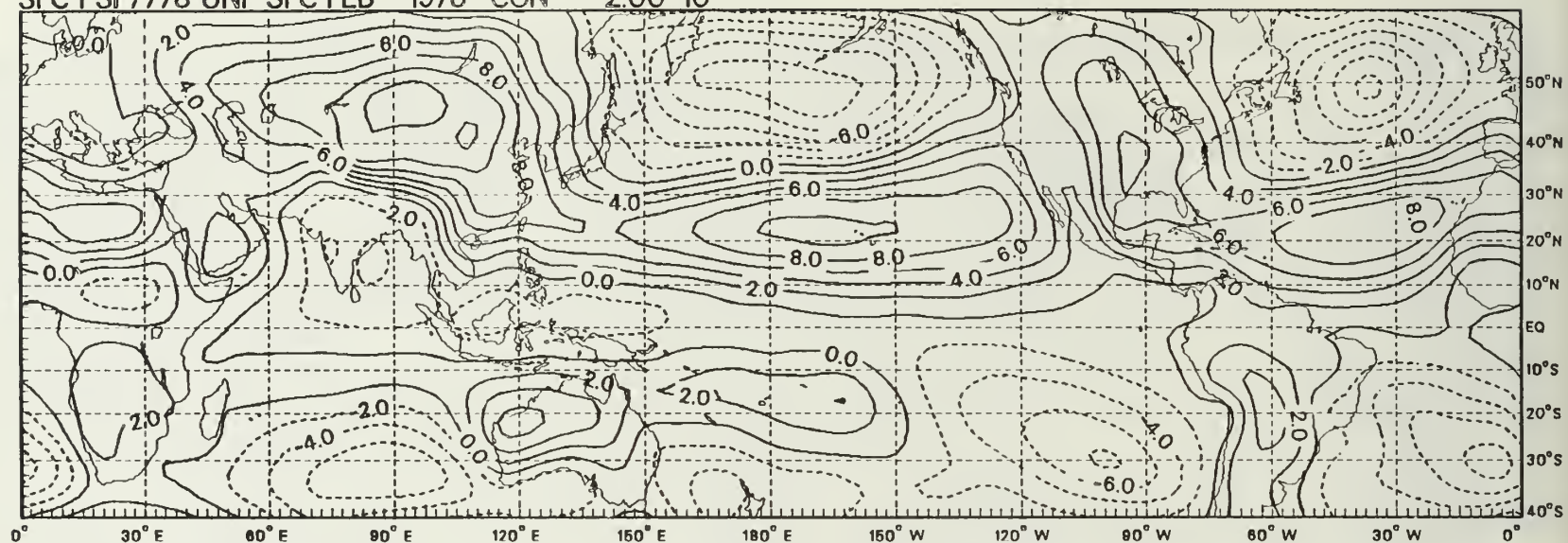


CHI UD.VD 7778 UNF SFC JAN 1978 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$  —CHI UD.VD 7778 UNF SFC JAN AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$  —

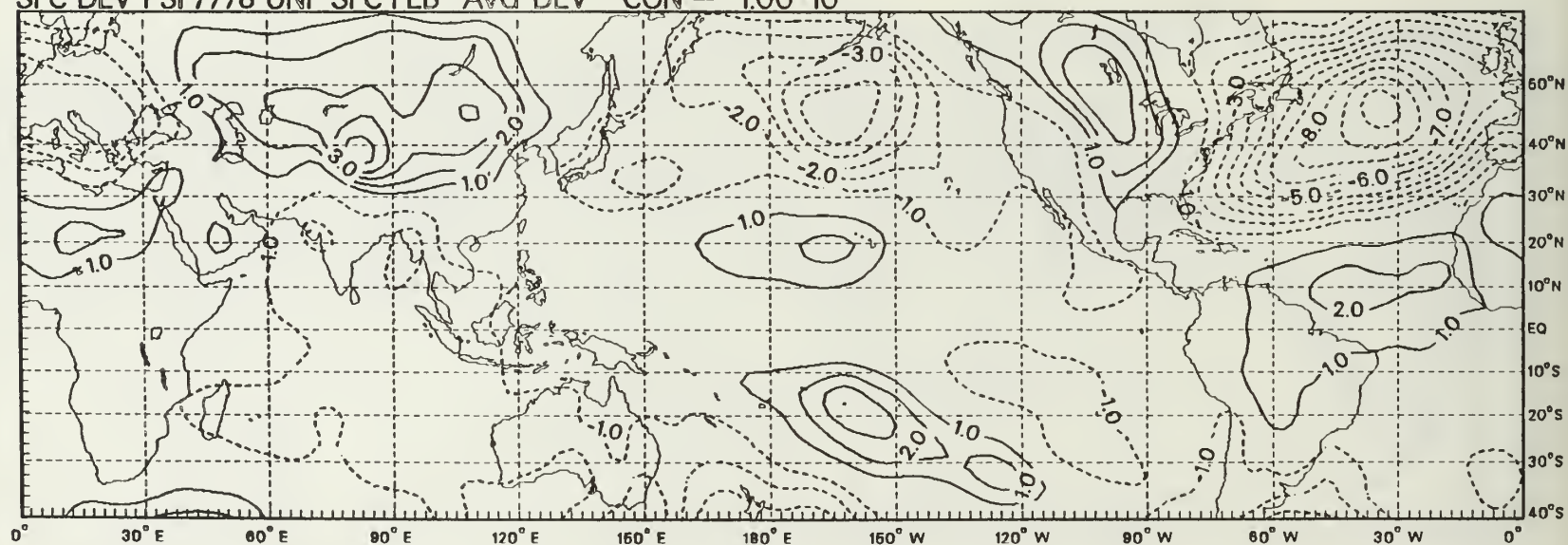


SFC U,V 7778 UNF SFC FEB 1978 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U,V 7778 UNF SFC FEB AVG DEV CON =  $1.50 \times 10^0$ SCALE =  $2.500 \times 10^0$  —

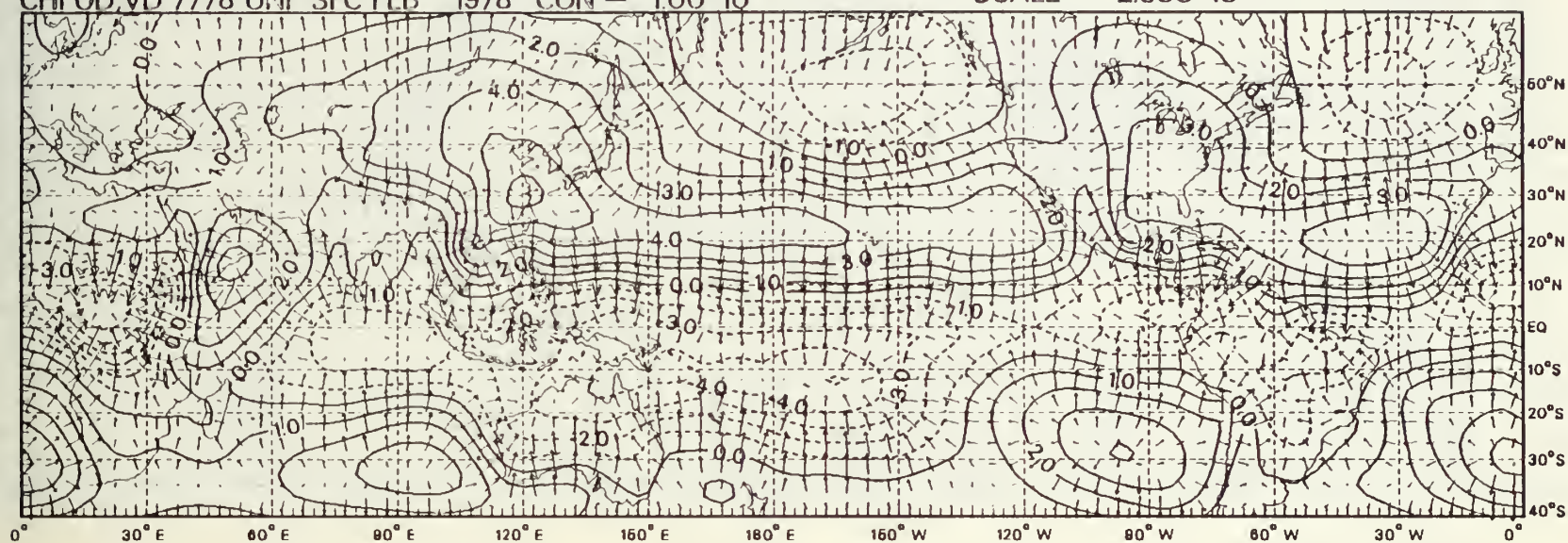
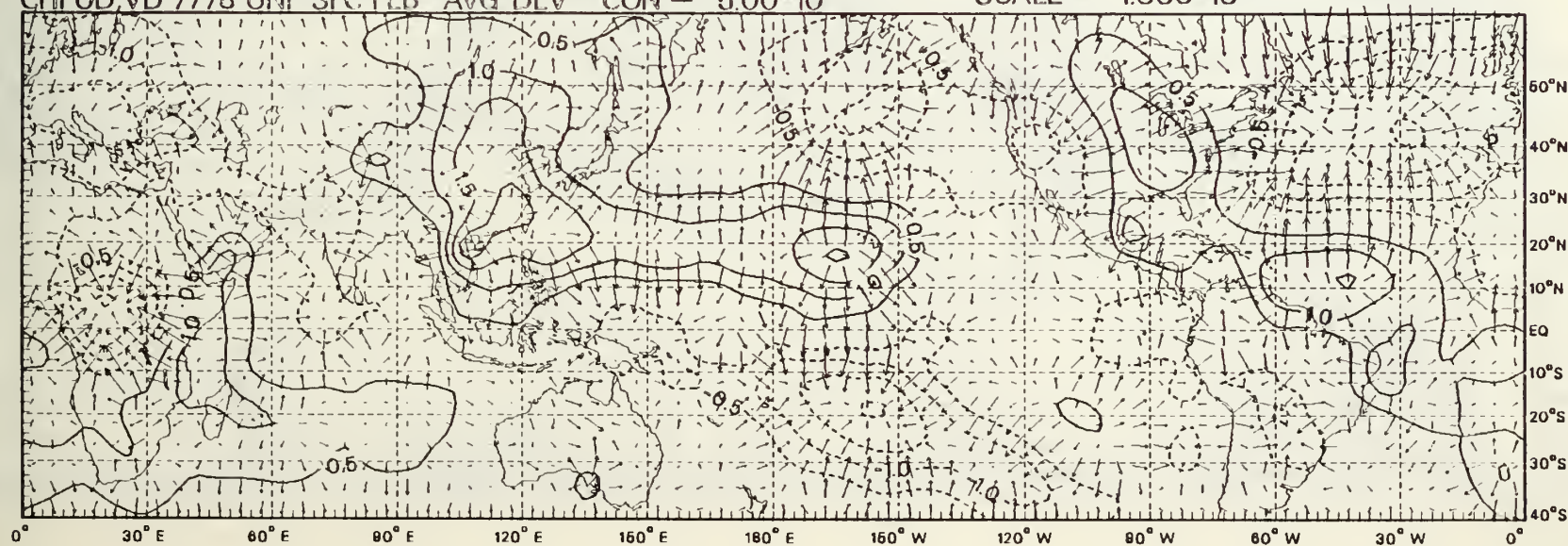
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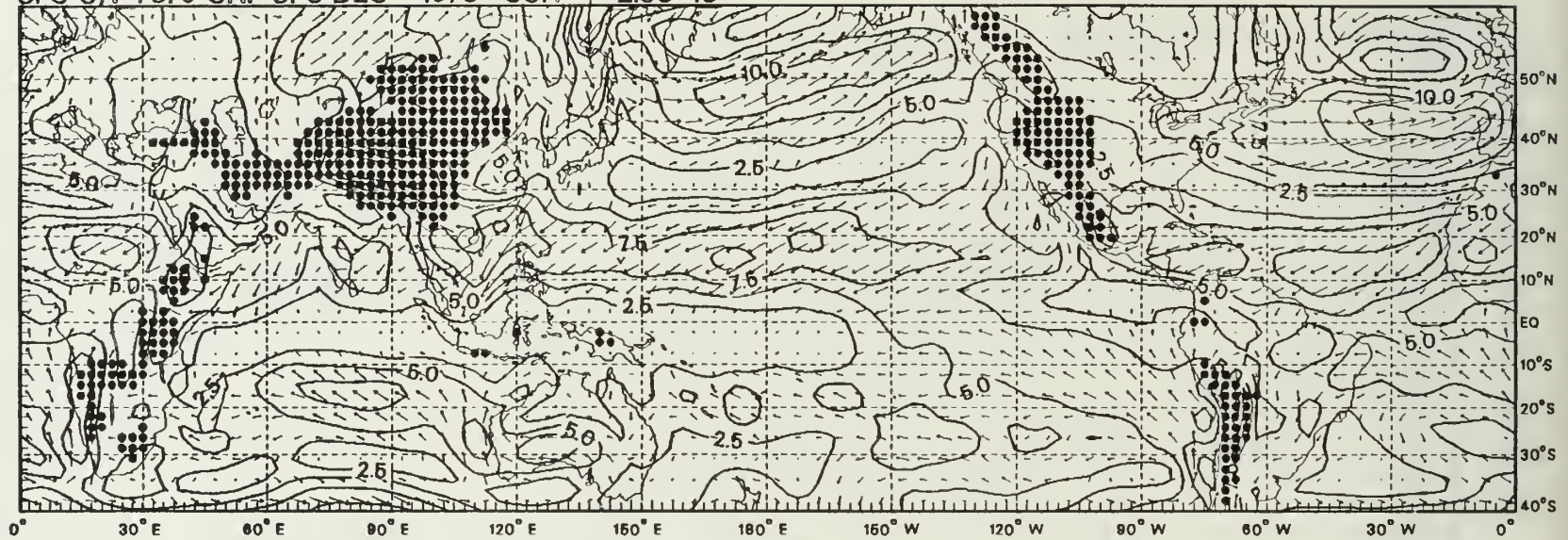
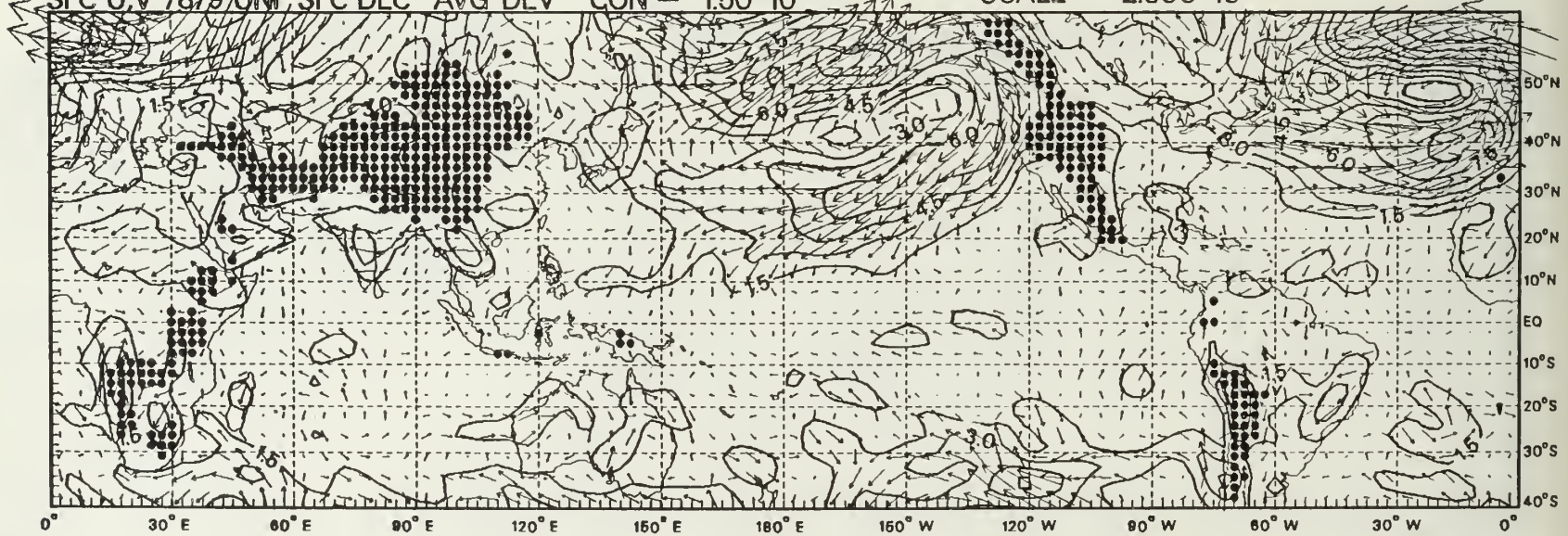
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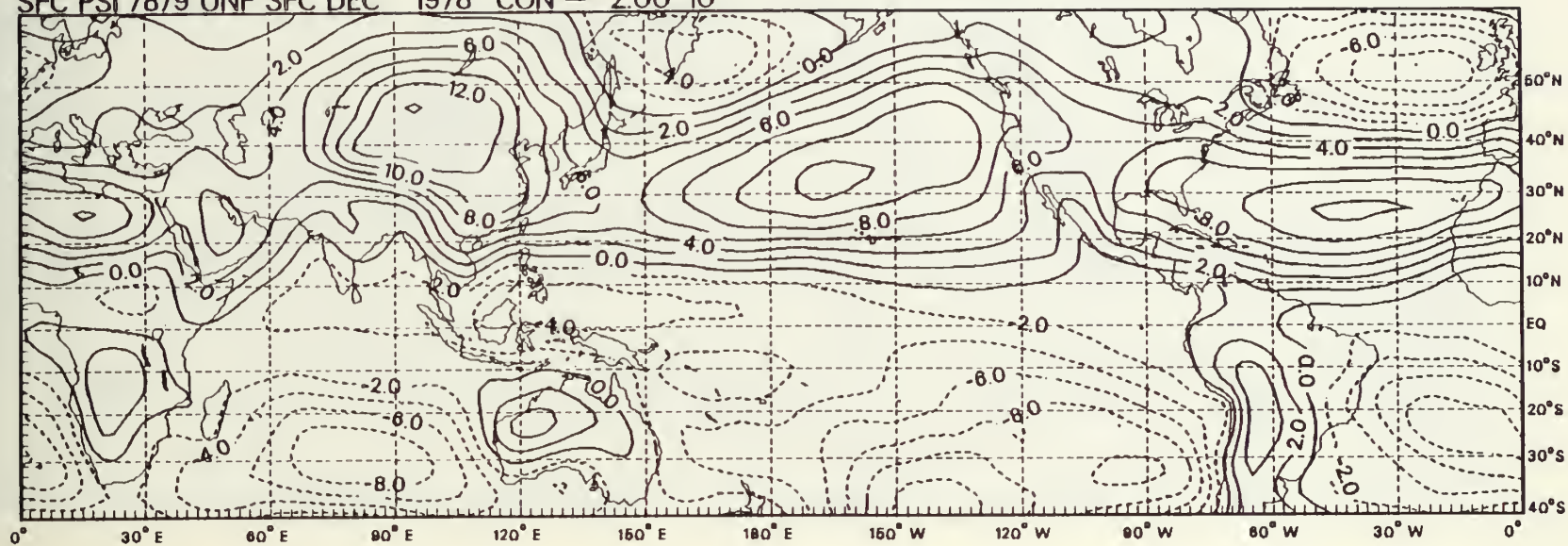
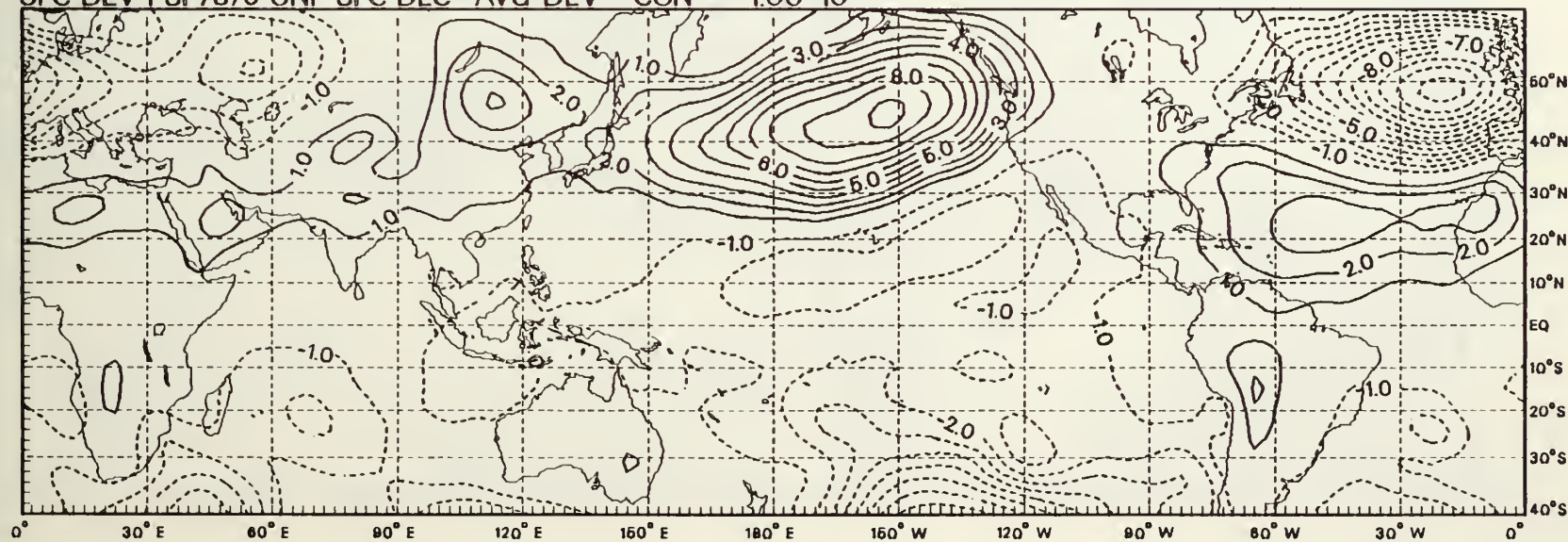


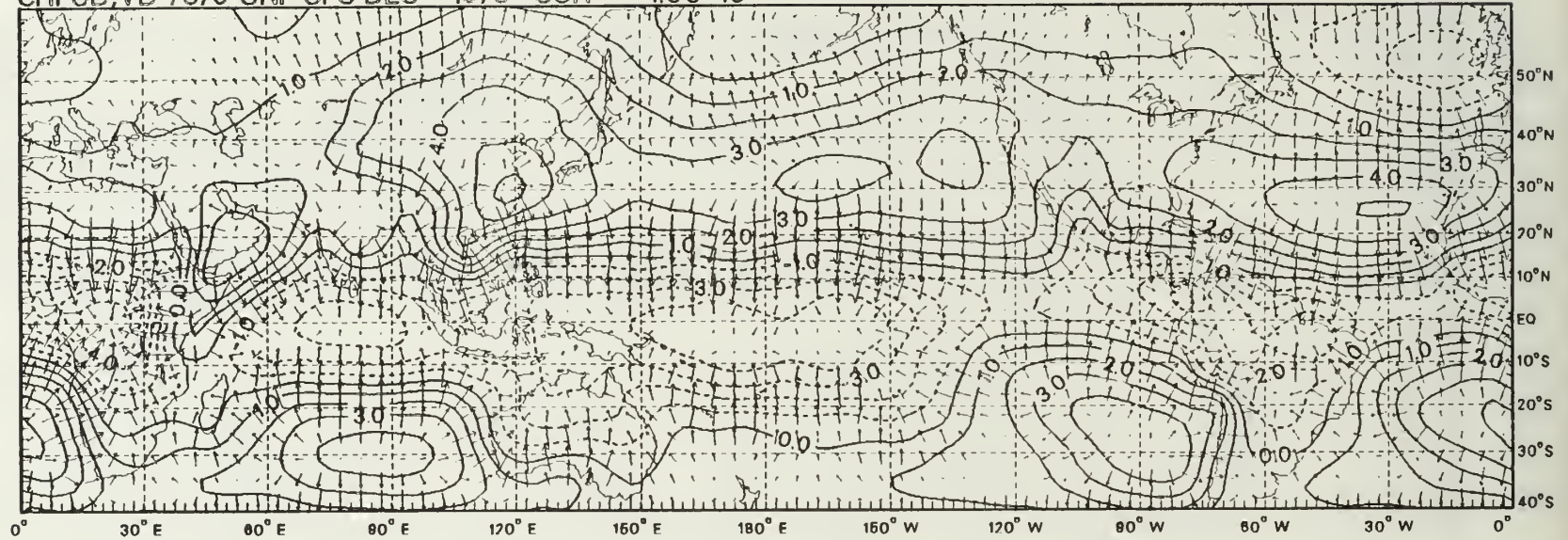
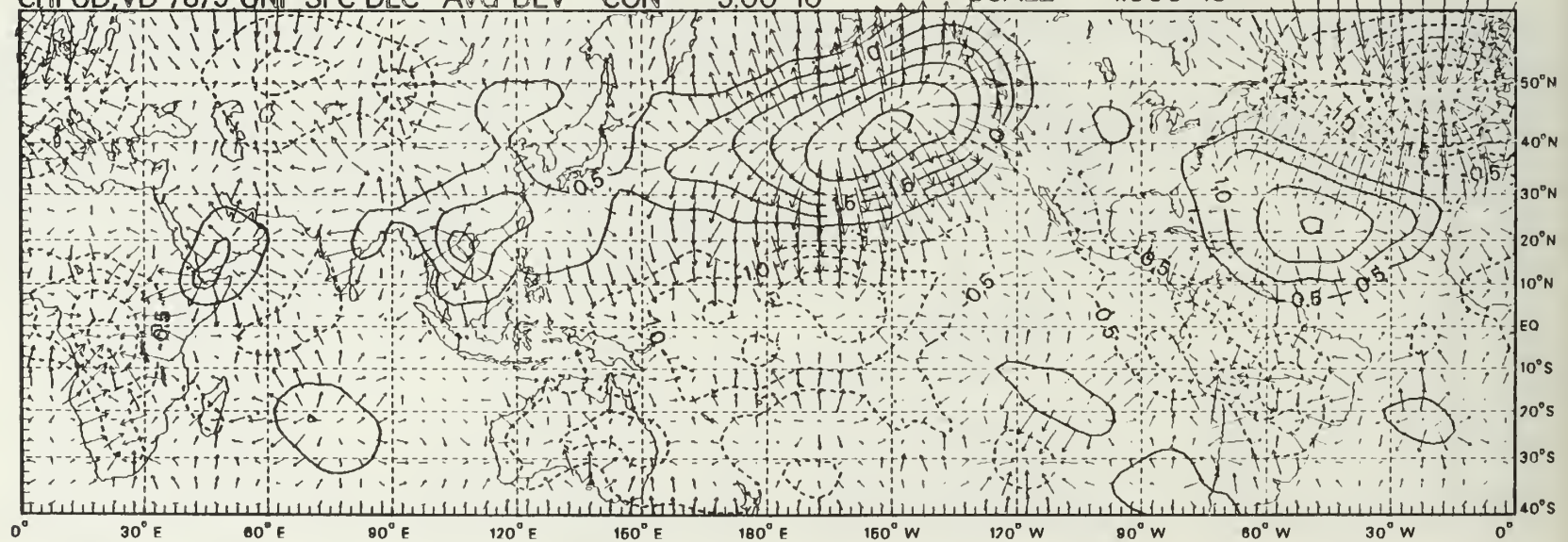
CHI UD.VD 7778 UNF SFC FEB 1978 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$  —CHI UD.VD 7778 UNF SFC FEB AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$  —



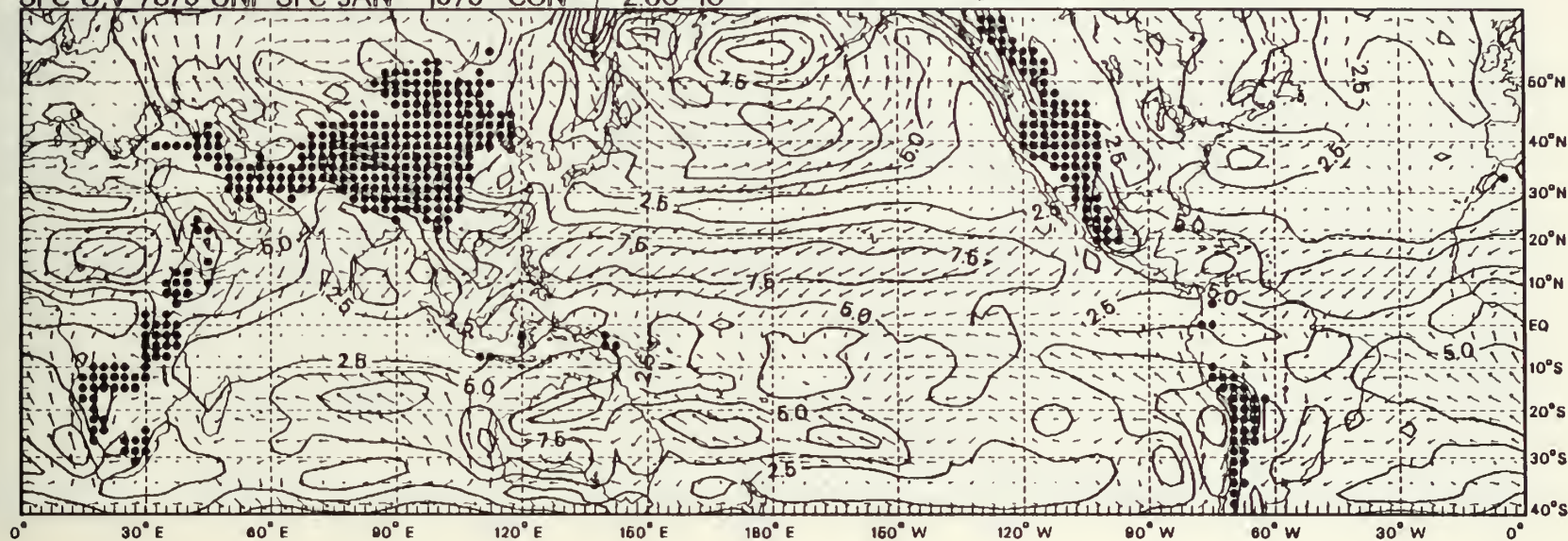
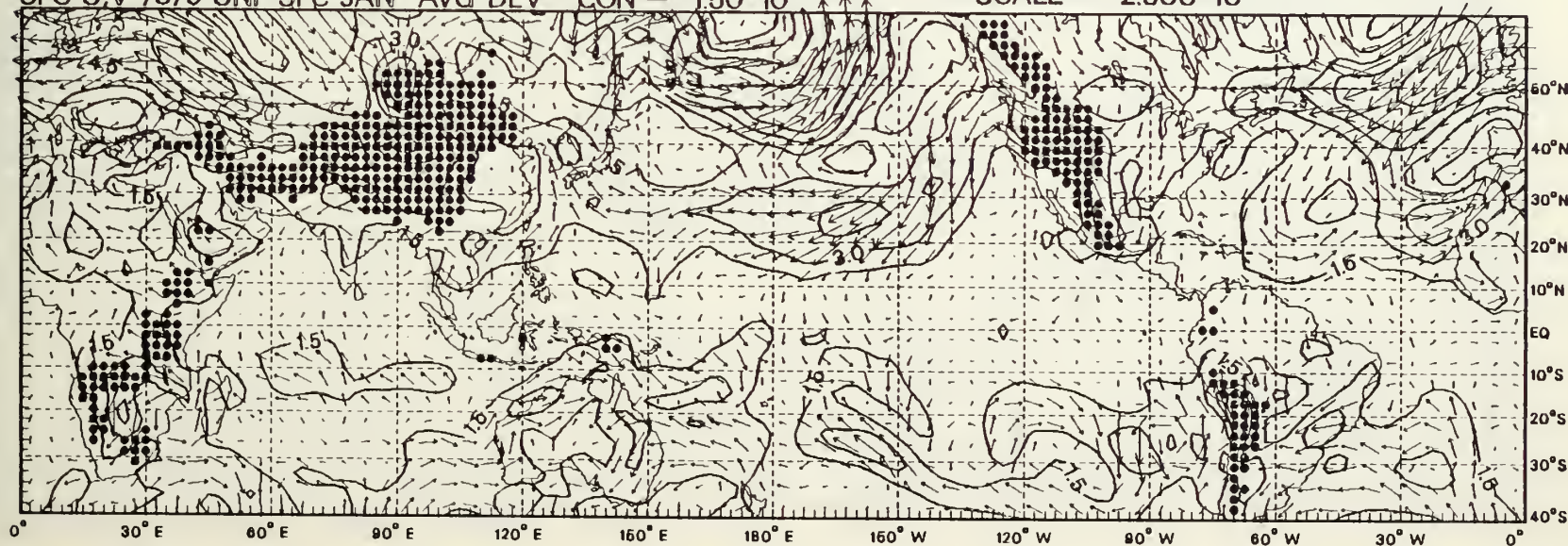
SFC U,V 7879 UNF SFC DEC 1978 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U,V 7879 UNF SFC DEC AVG DEV CON =  $1.50 \times 10^0$ SCALE =  $2.500 \times 10^0$  —

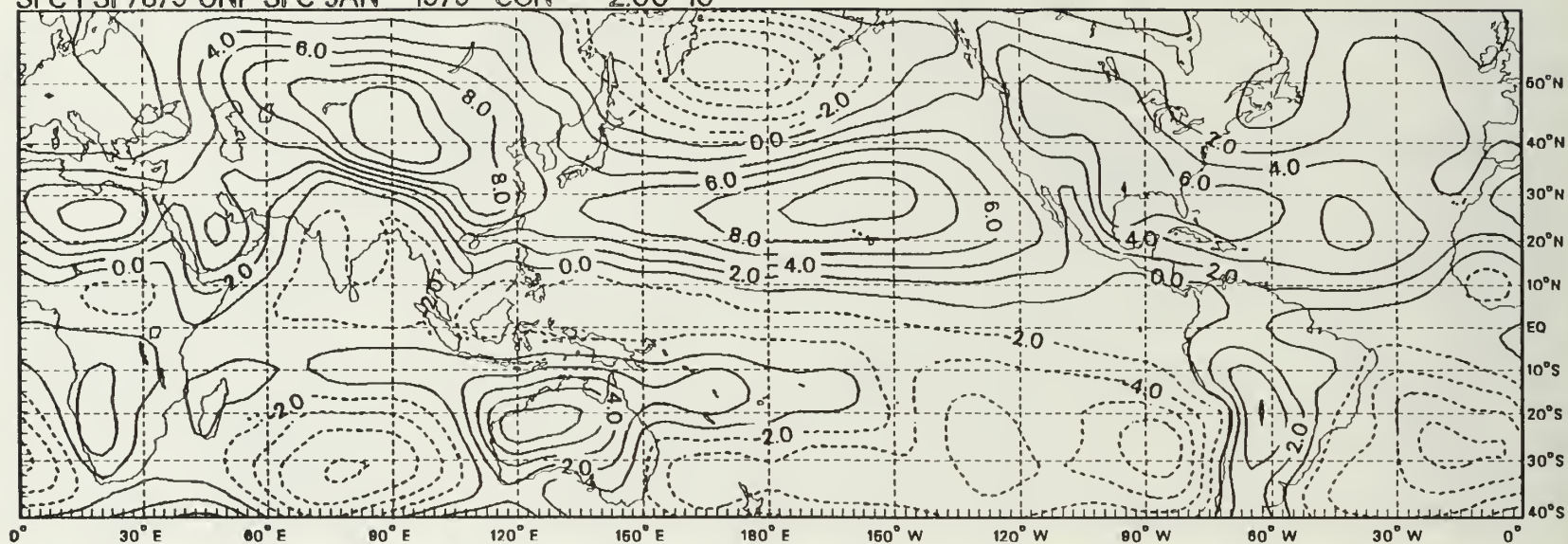
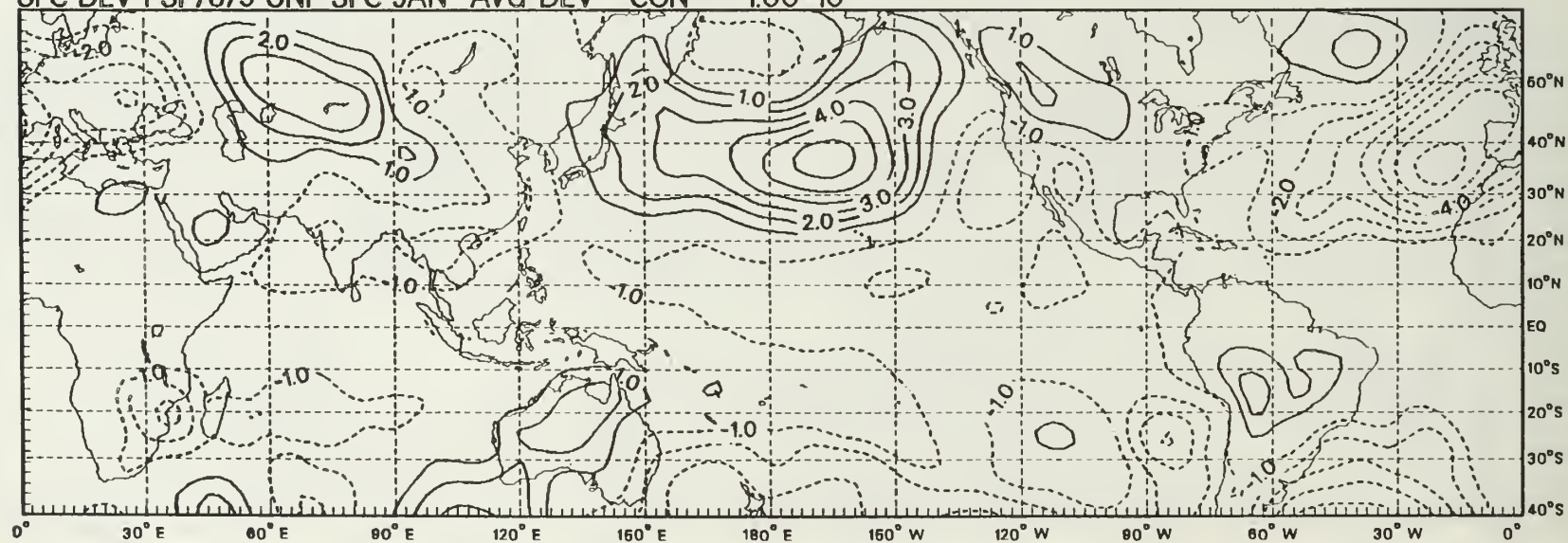


SFC PSI 7879 UNF SFC DEC 1978 CON =  $2.00 \times 10^0$ SFC DEV PSI 7879 UNF SFC DEC AVG DEV CON =  $1.00 \times 10^0$ 

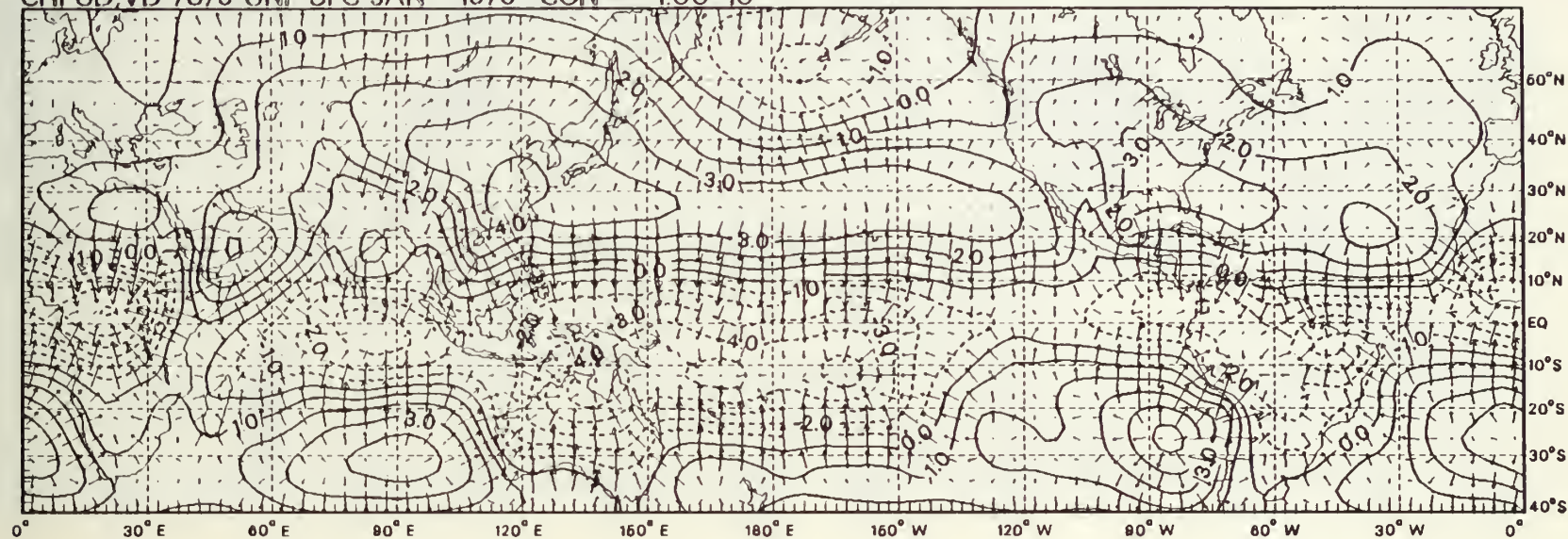
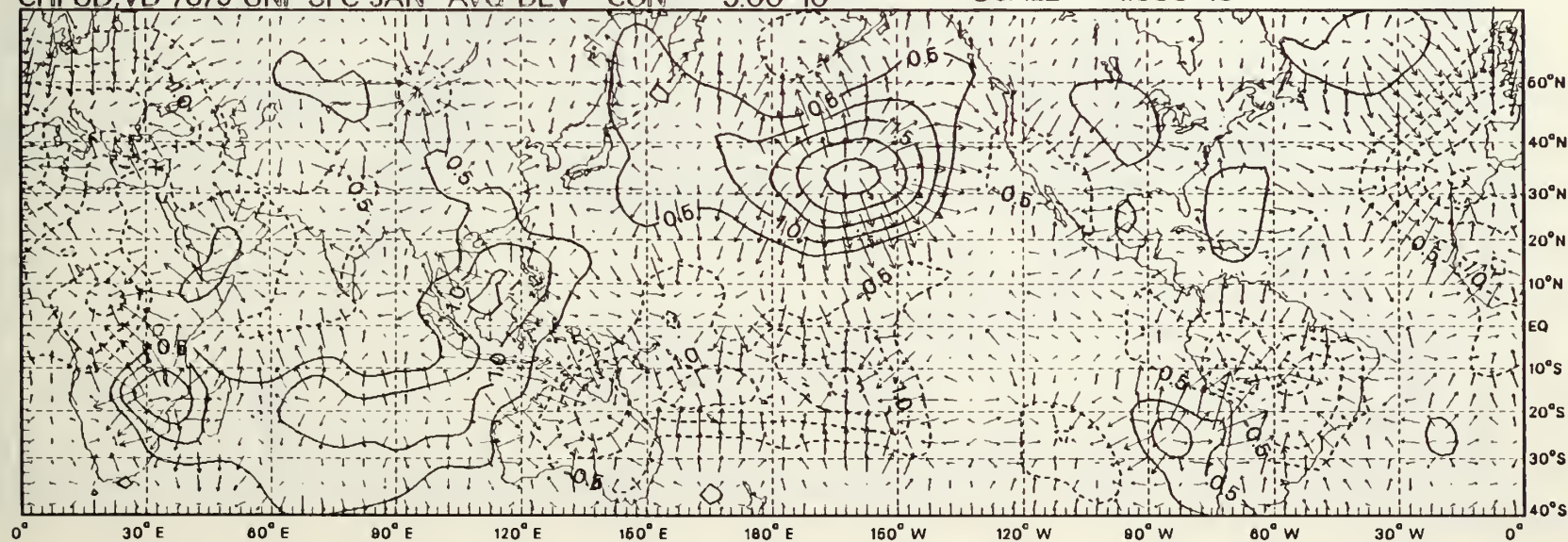
CHI UD,VD 7879 UNF SFC DEC 1978 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$  —CHI UD,VD 7879 UNF SFC DEC AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$  —



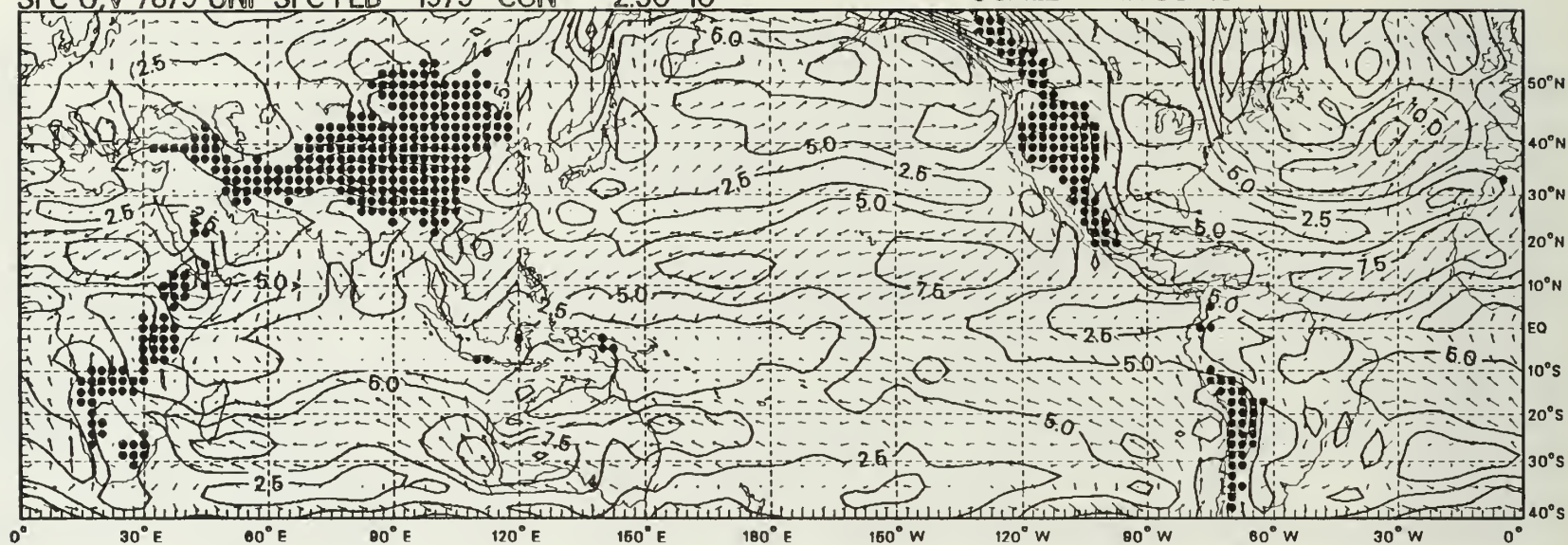
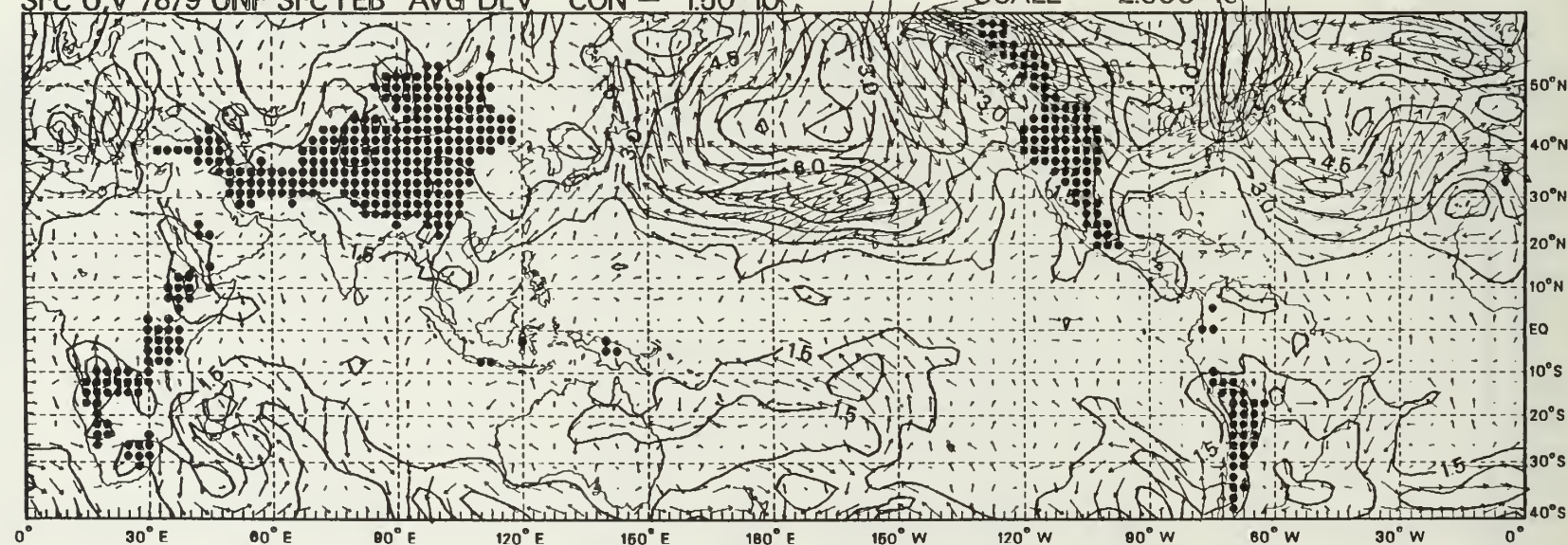
SFC U.V 7879 UNF SFC JAN 1979 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U.V 7879 UNF SFC JAN AVG DEV CON =  $150 \times 10^0$ SCALE =  $2.500 \times 10^0$  —

SFC PSI 7879 UNF SFC JAN 1979 CON =  $2.00 \times 10^0$ SFC DEV PSI 7879 UNF SFC JAN AVG DEV CON =  $1.00 \times 10^0$ 

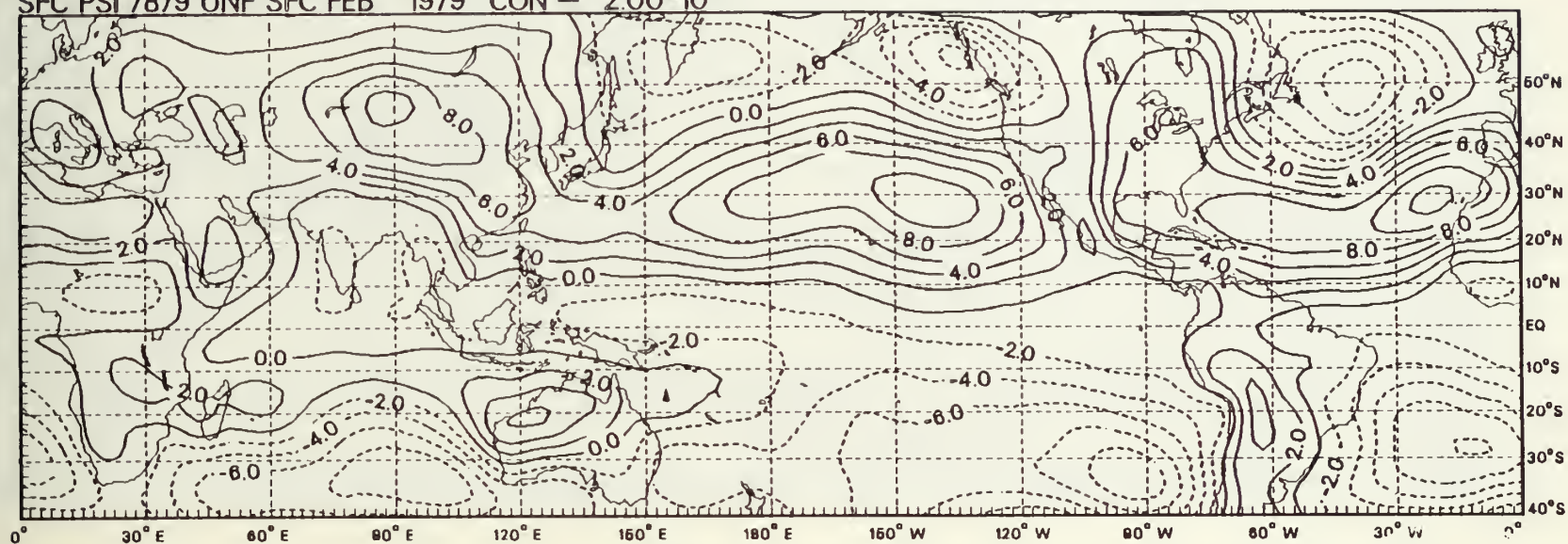
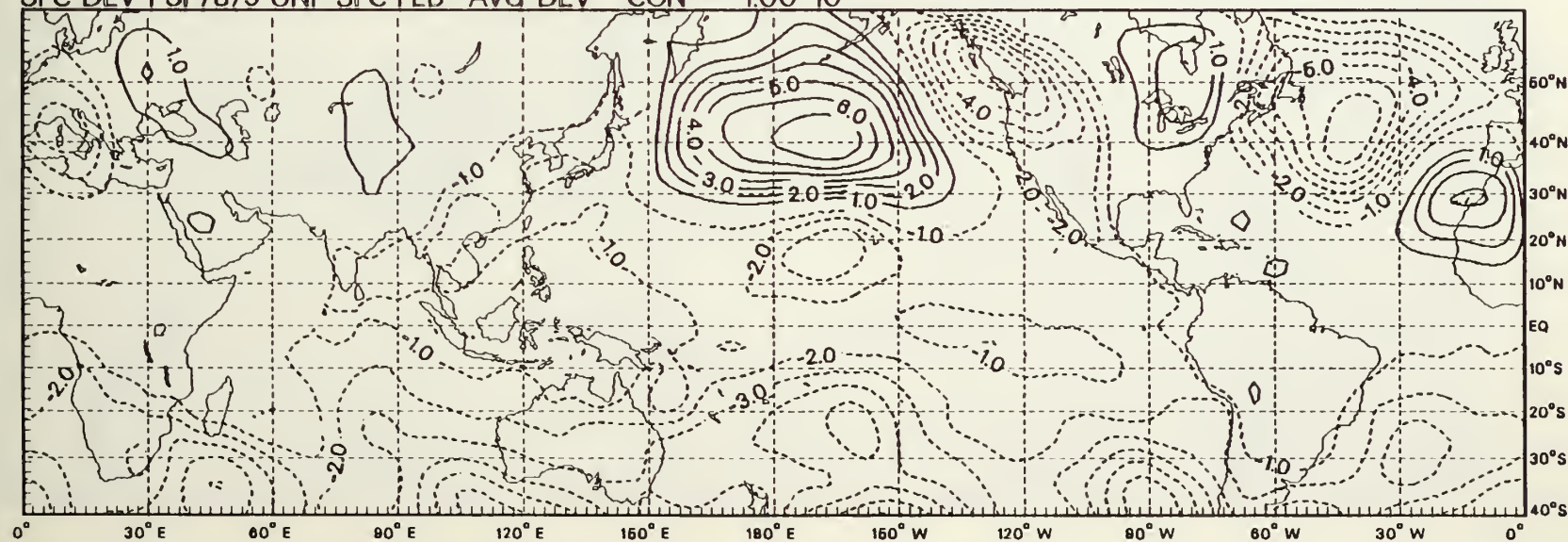


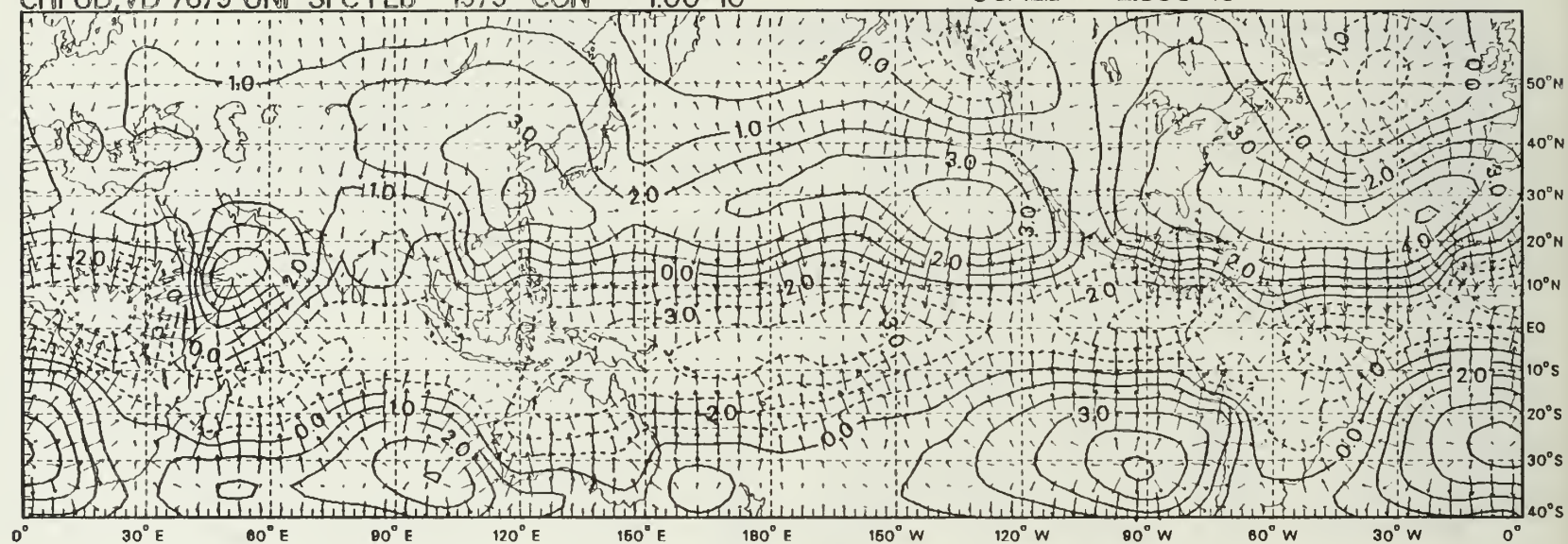
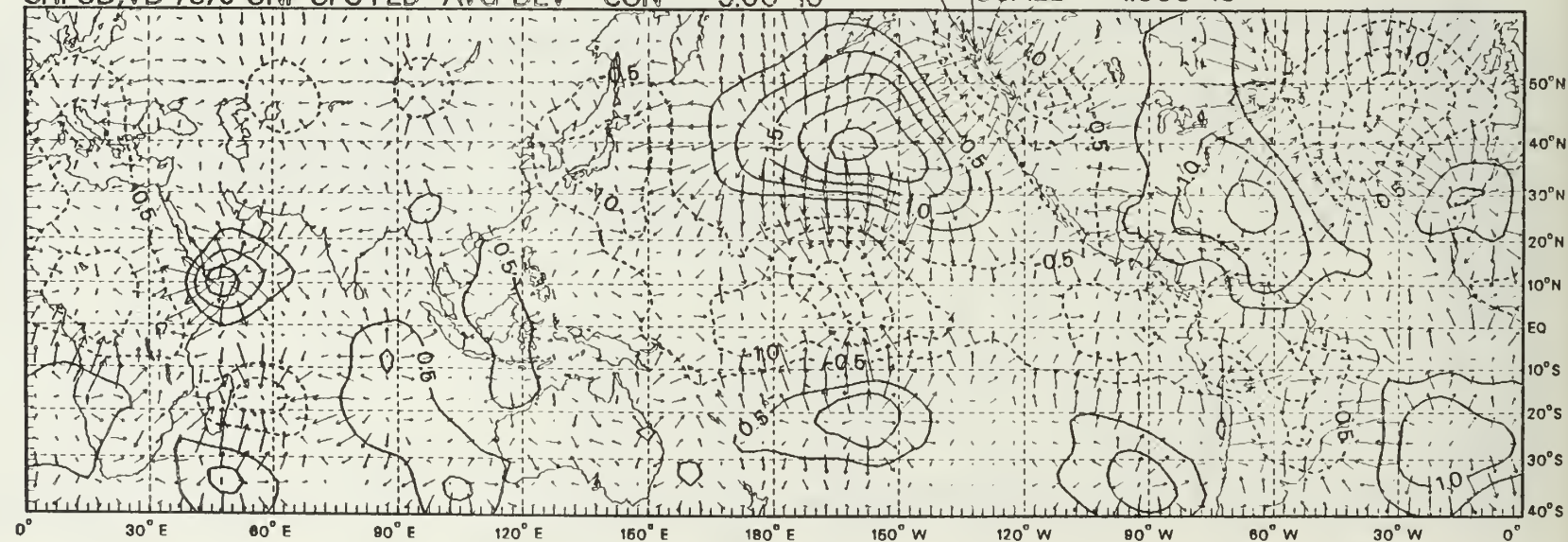
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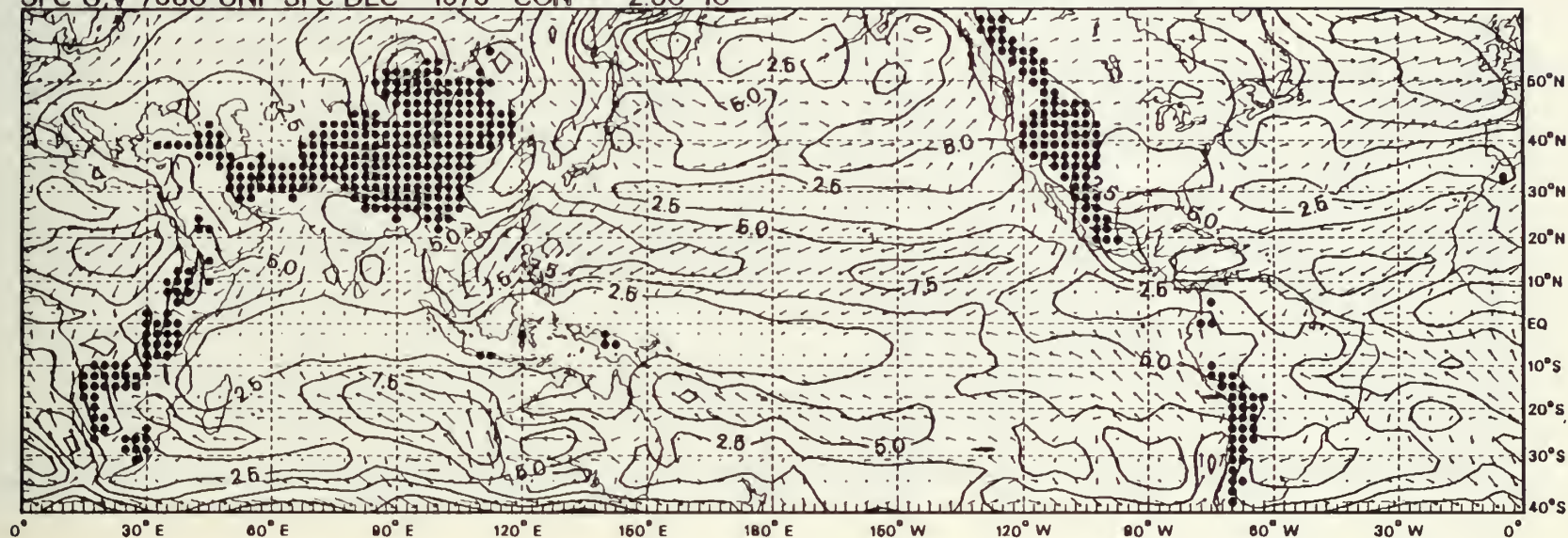
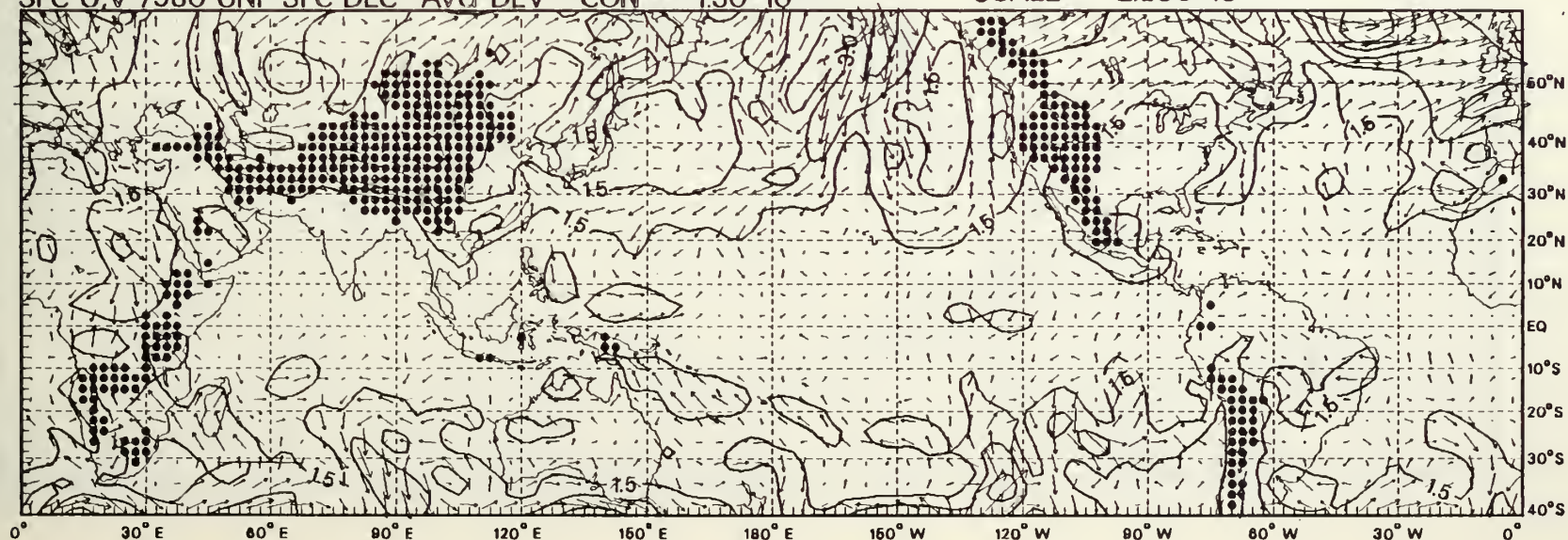
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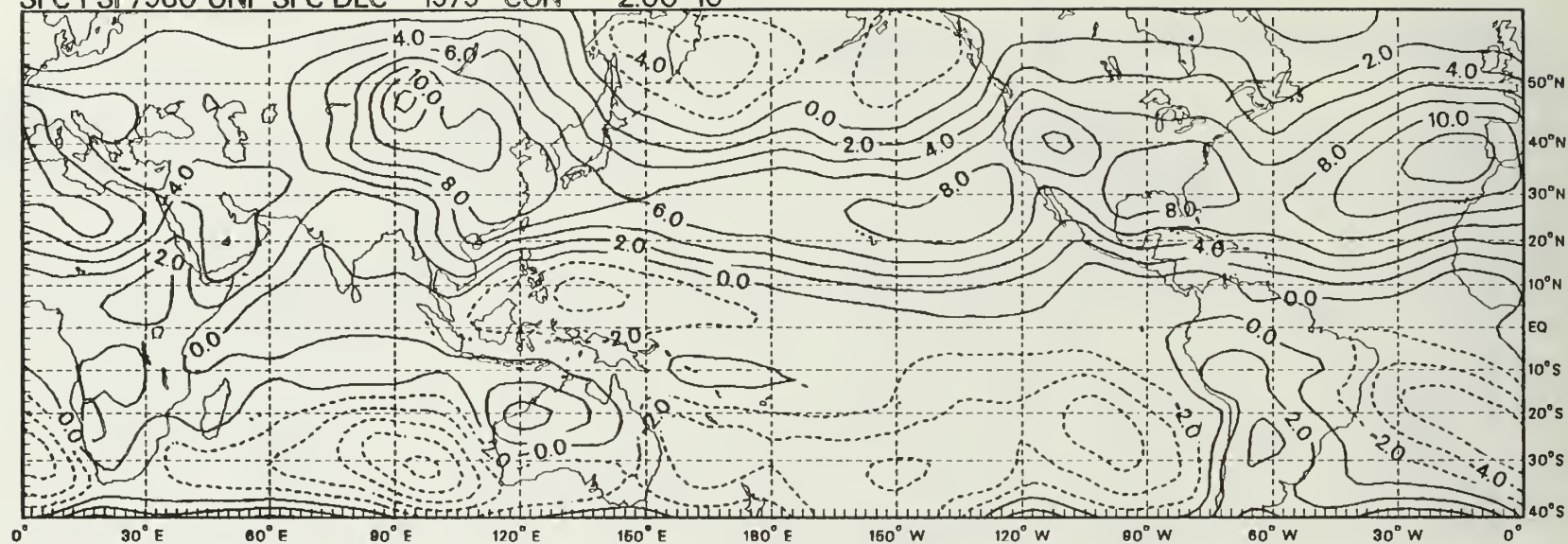
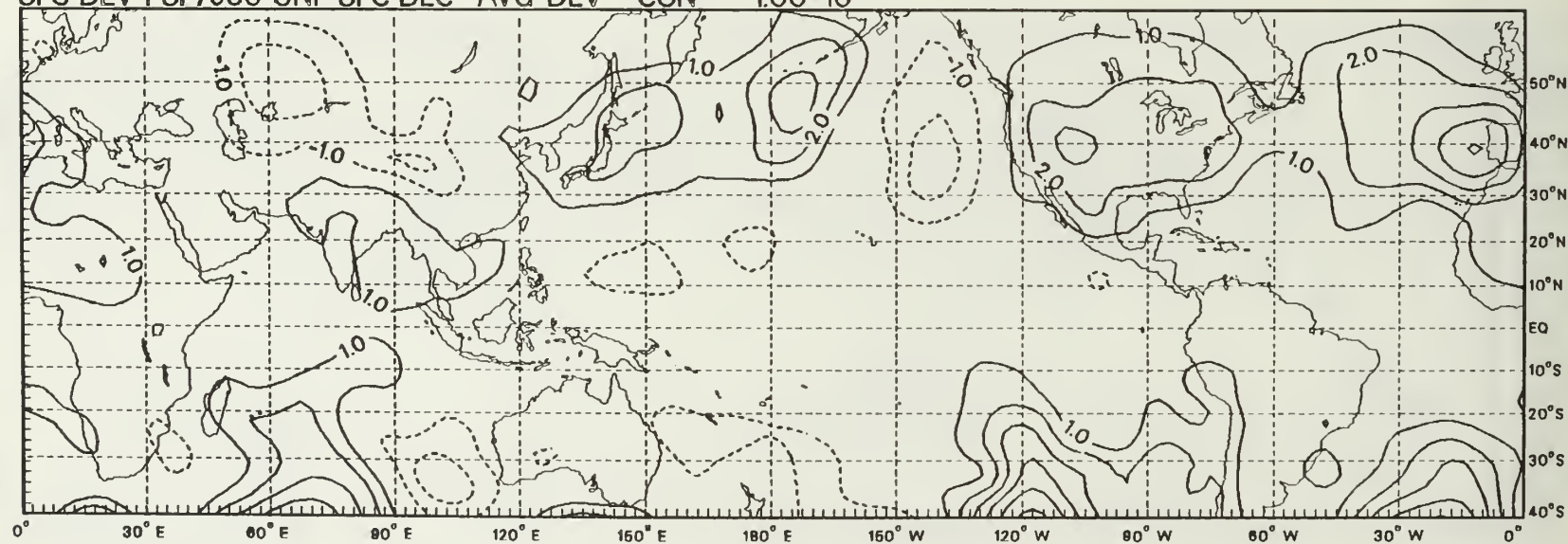


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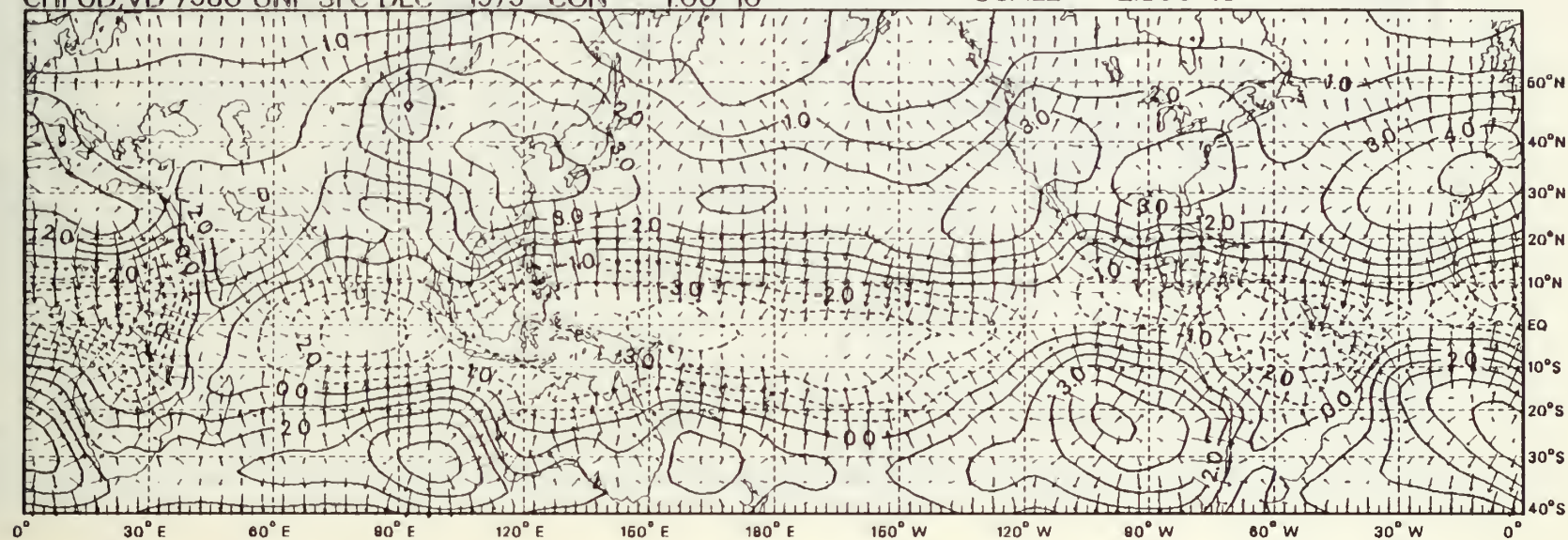
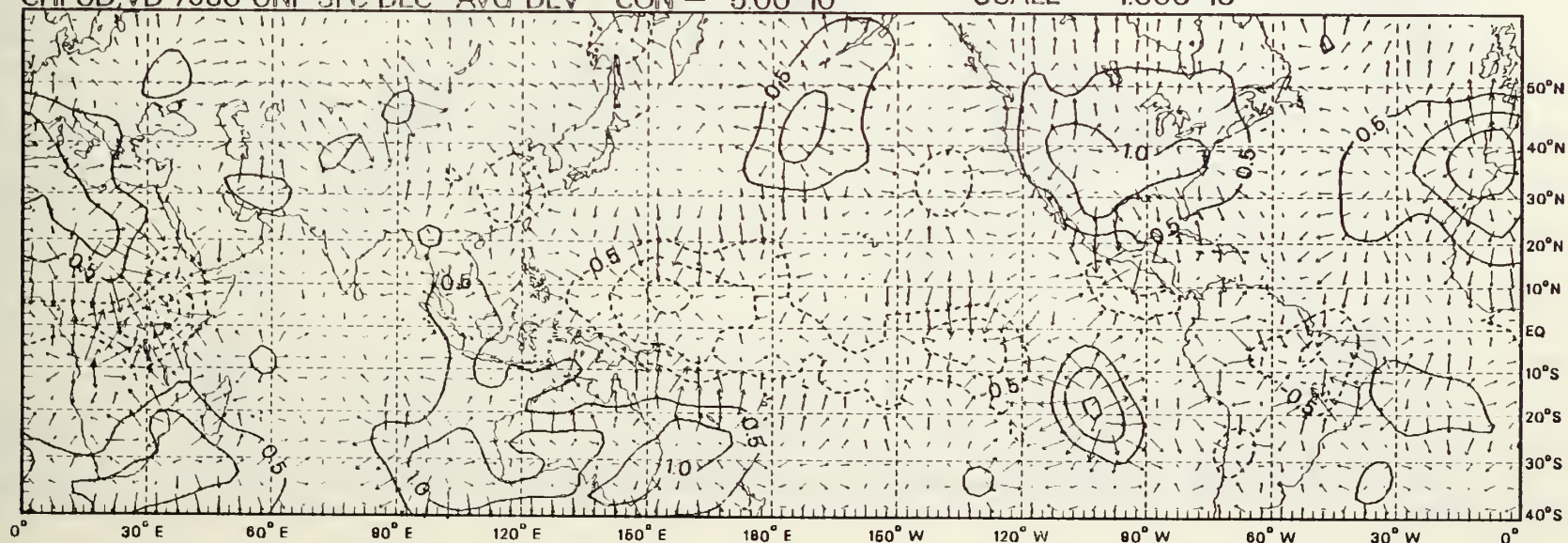
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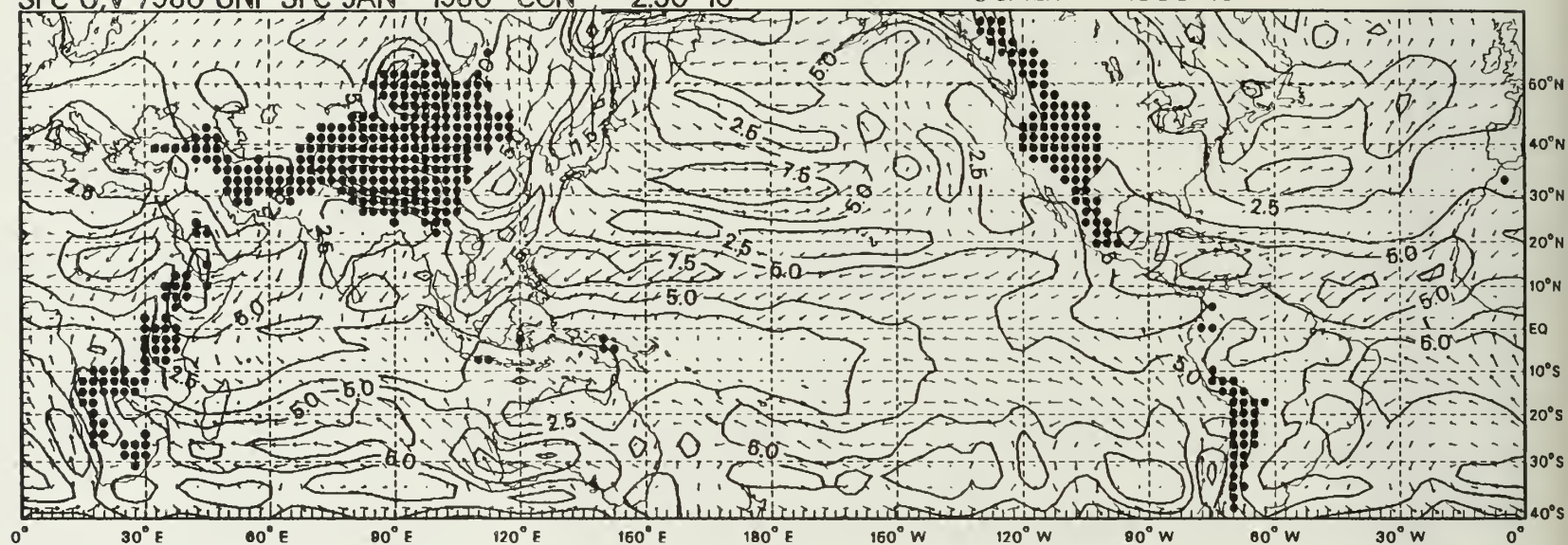
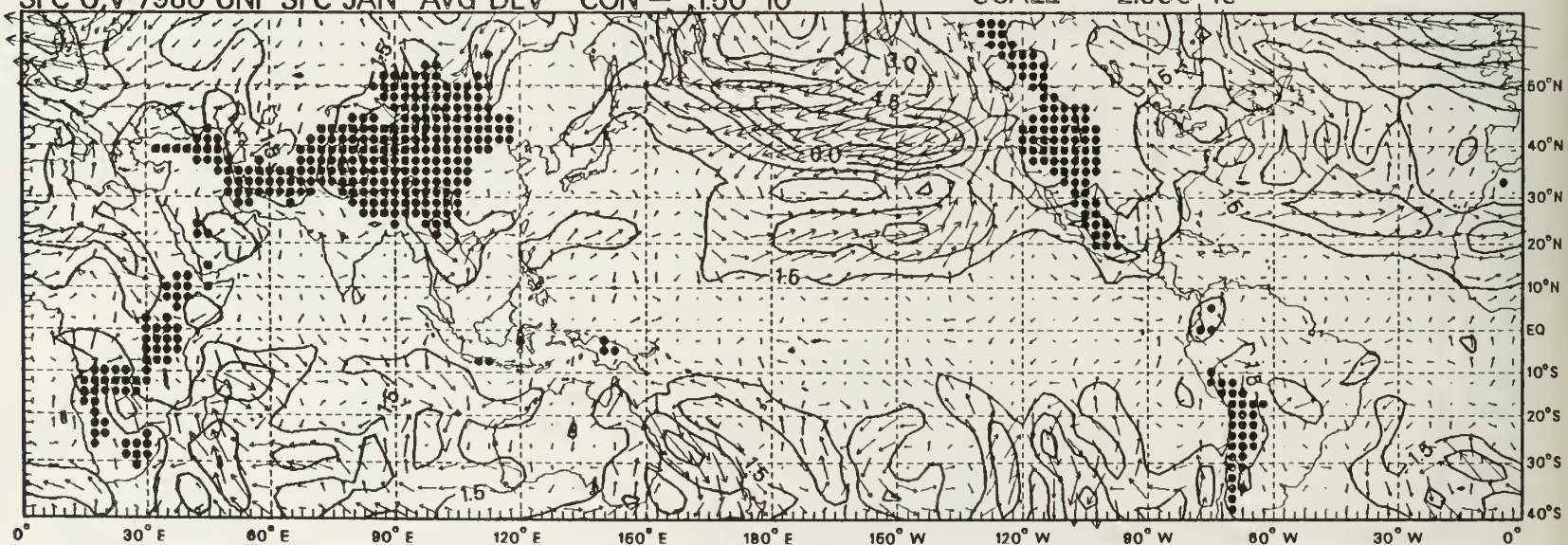
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SFC PSI 7980 UNF SFC DEC 1979 CON =  $2.00 \times 10^0$ SFC DEV PSI 7980 UNF SFC DEC AVG DEV CON =  $1.00 \times 10^0$ 



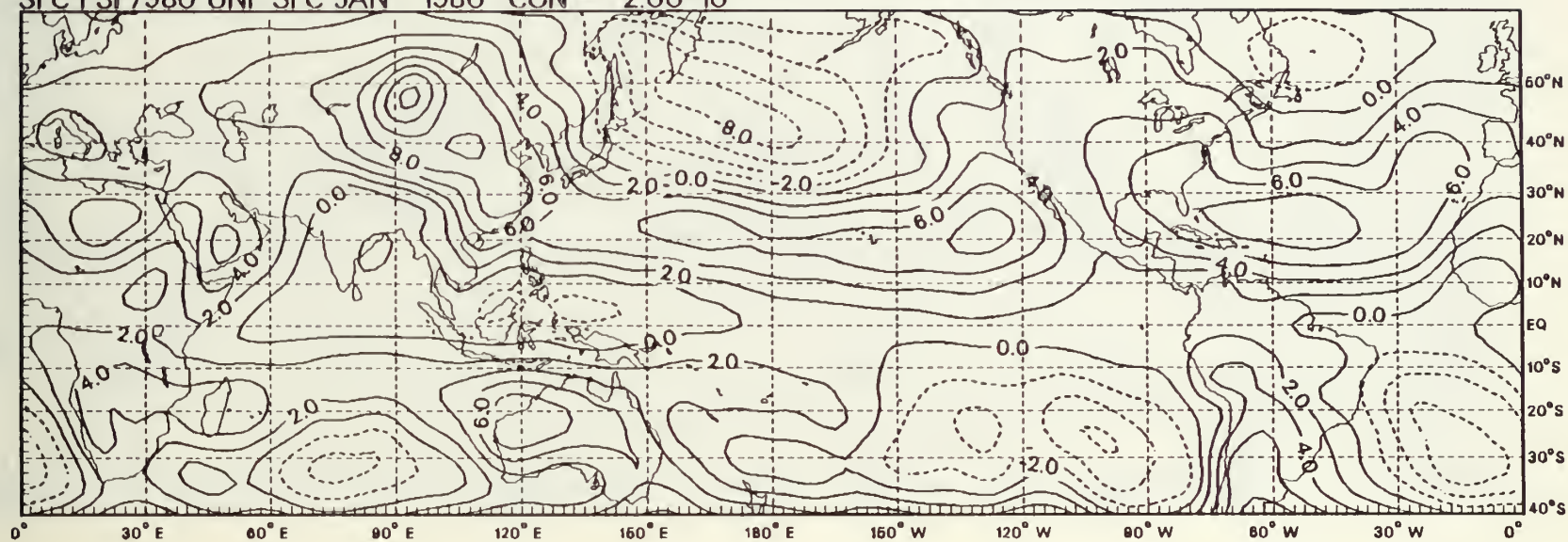
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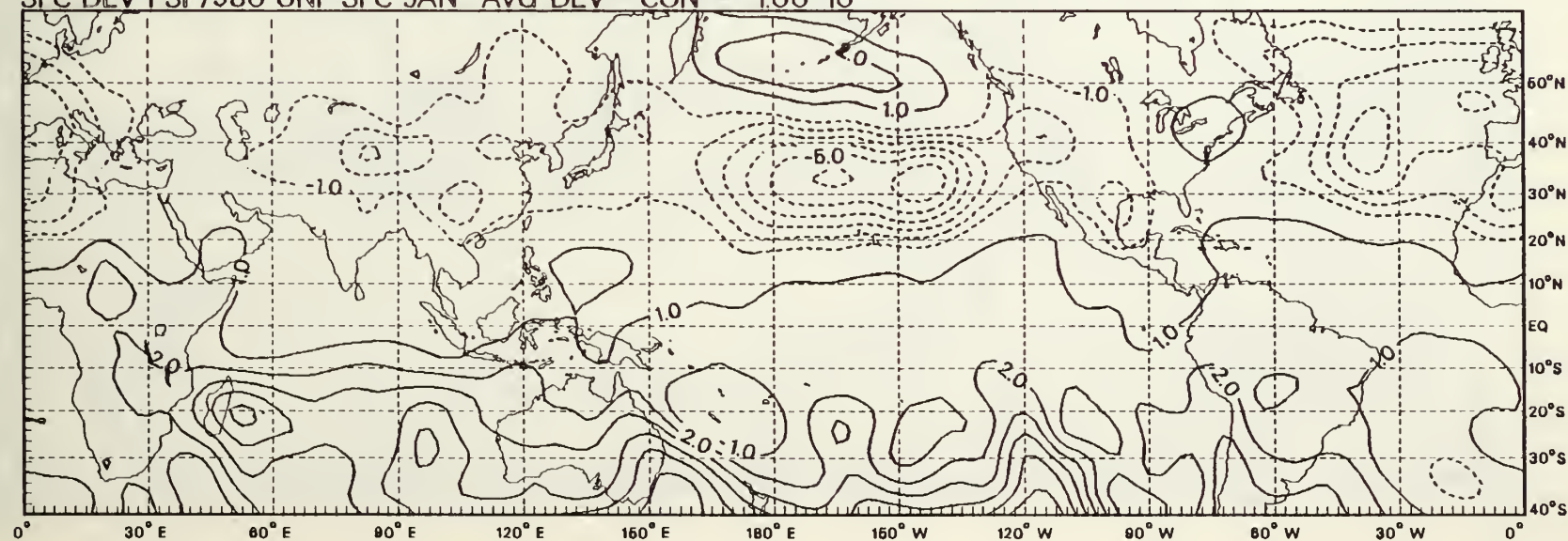
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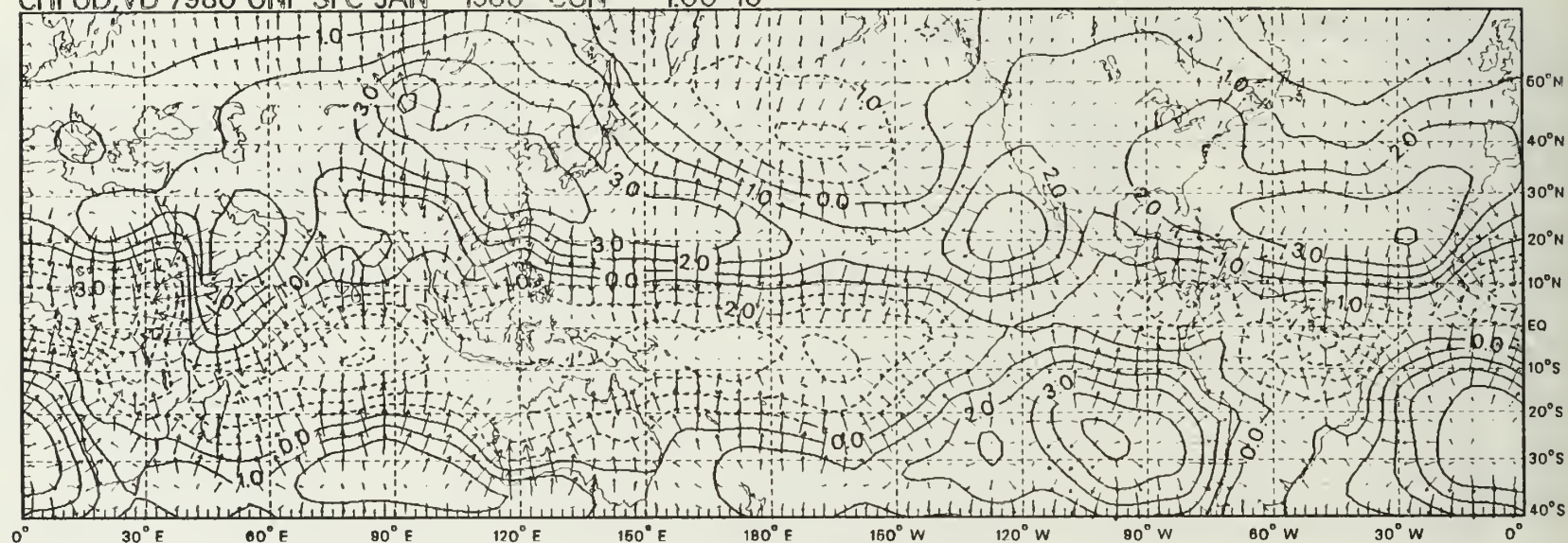
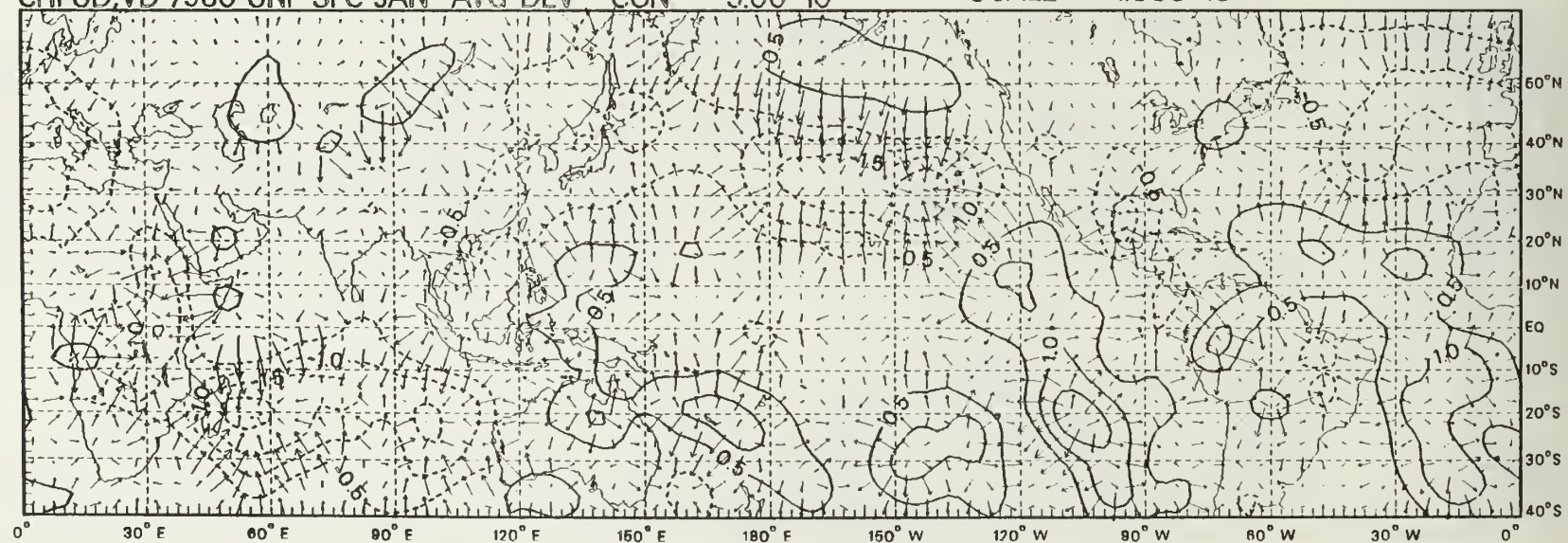


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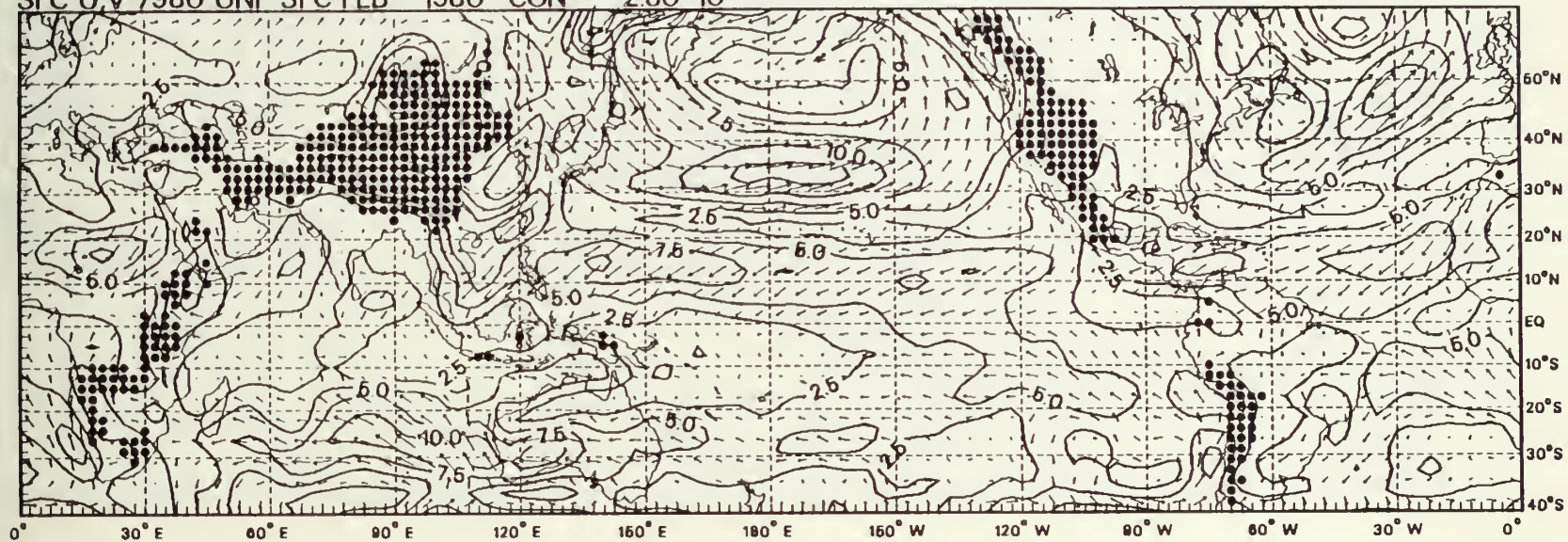
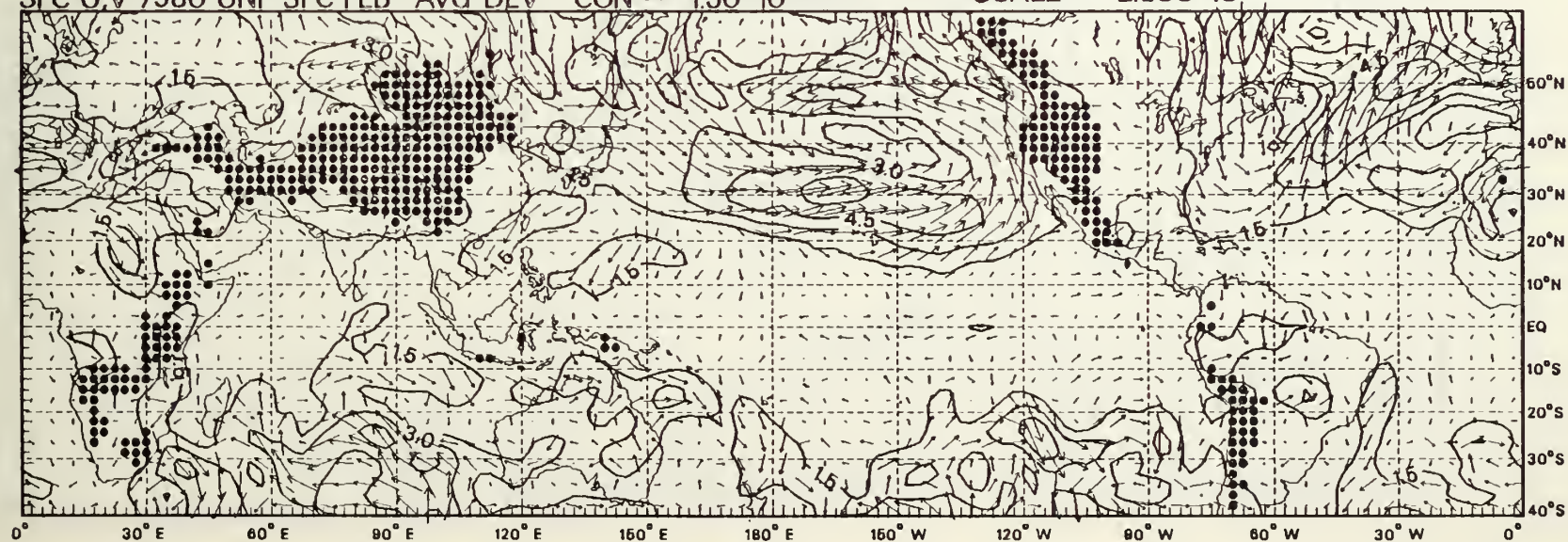


SFC DEV PSI 7980 UNF SFC JAN AVG DEV CON =  $1.00 \times 10^0$

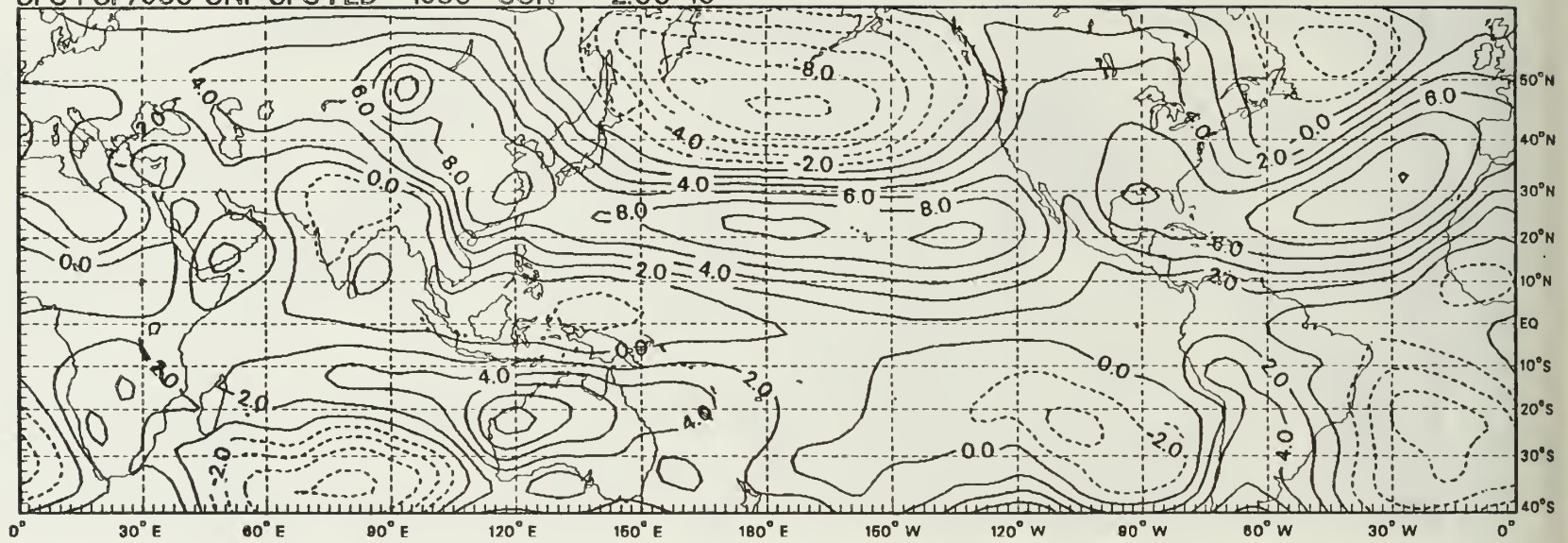


CHI UD,VD 7980 UNF SFC JAN 1980 CON =  $100 \cdot 10^0$ SCALE =  $2500 \cdot 10^0$  —CHI UD,VD 7980 UNF SFC JAN AVG DEV CON =  $5.00 \cdot 10^{-1}$ SCALE =  $1.000 \cdot 10^0$  —

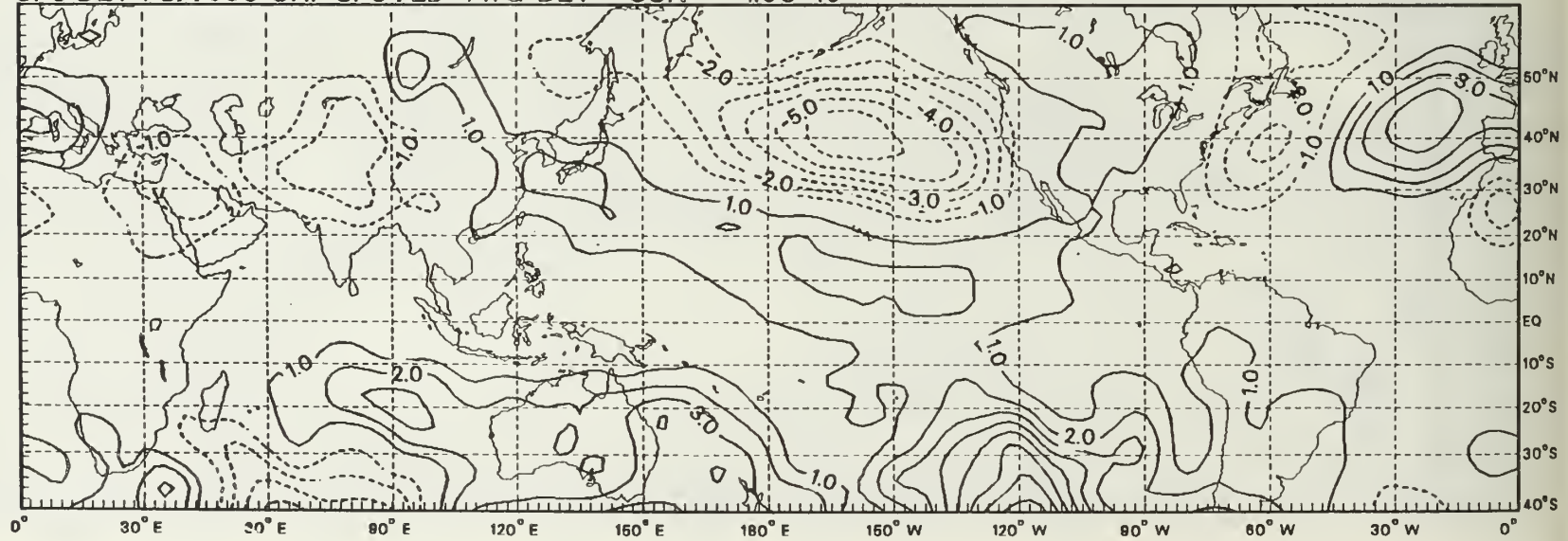


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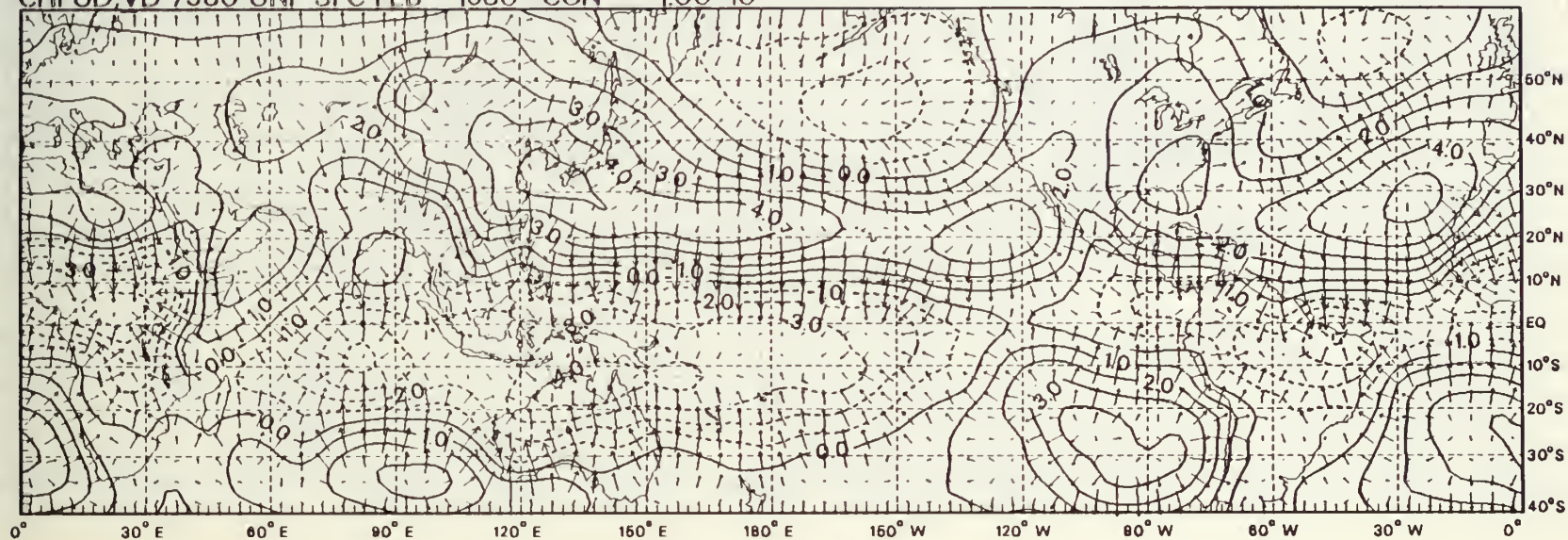
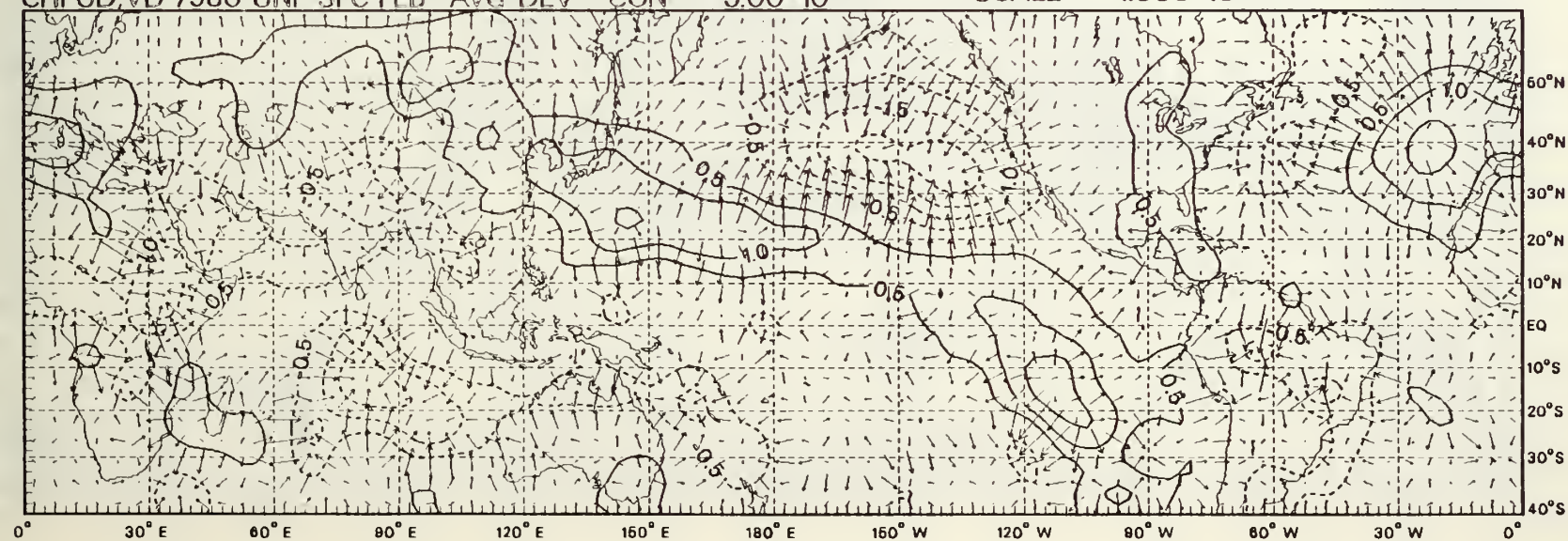
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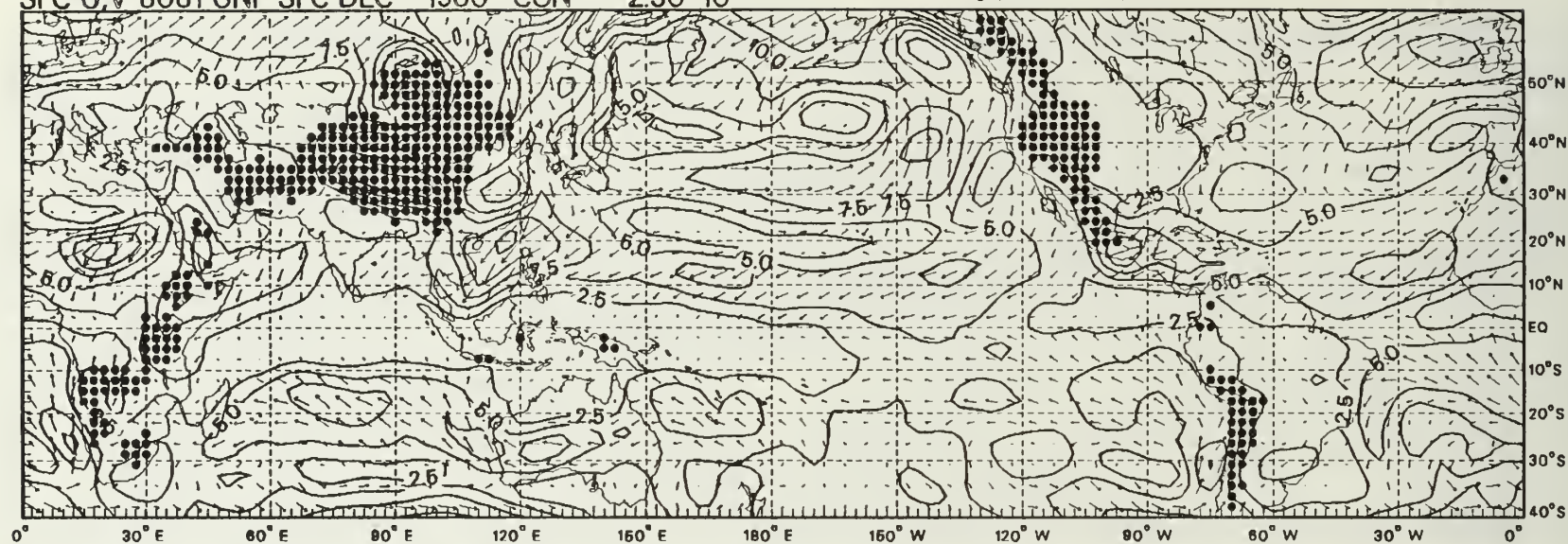
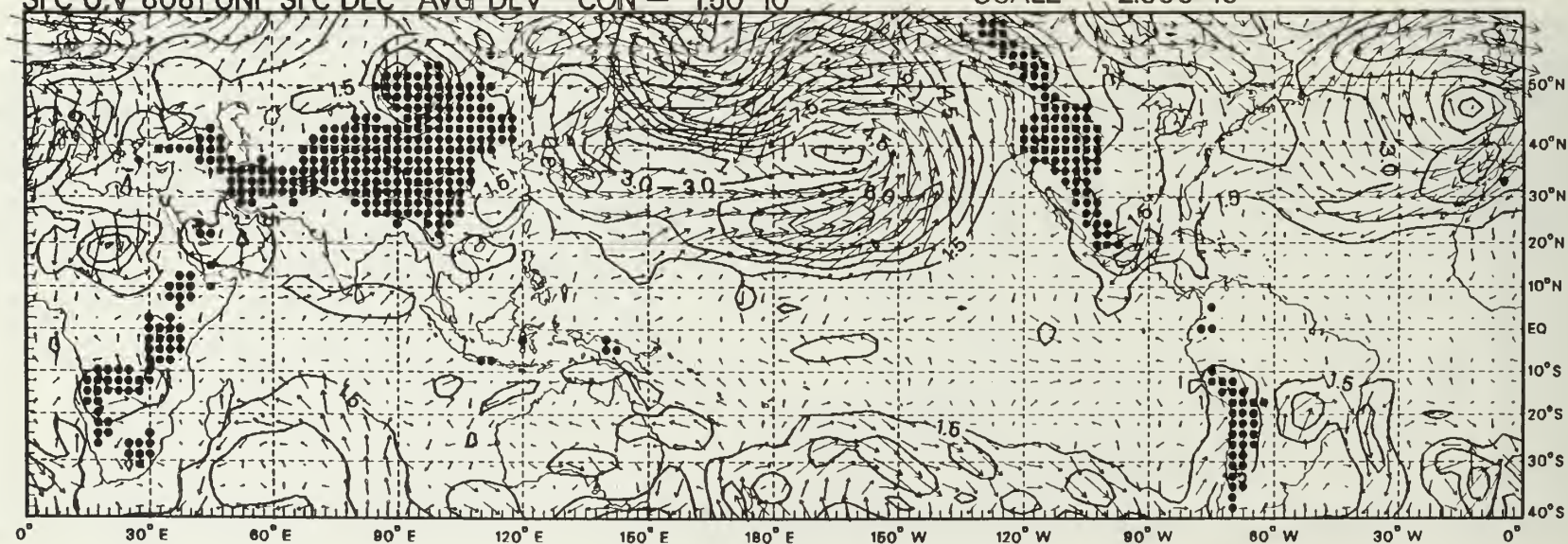
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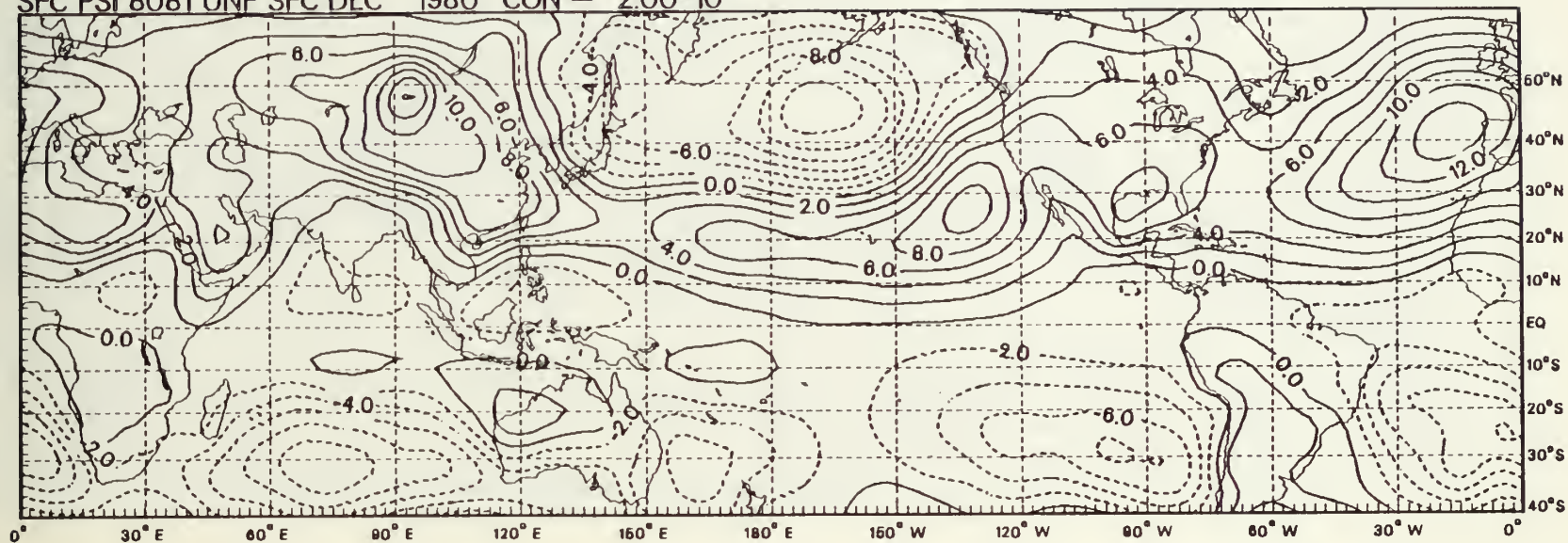
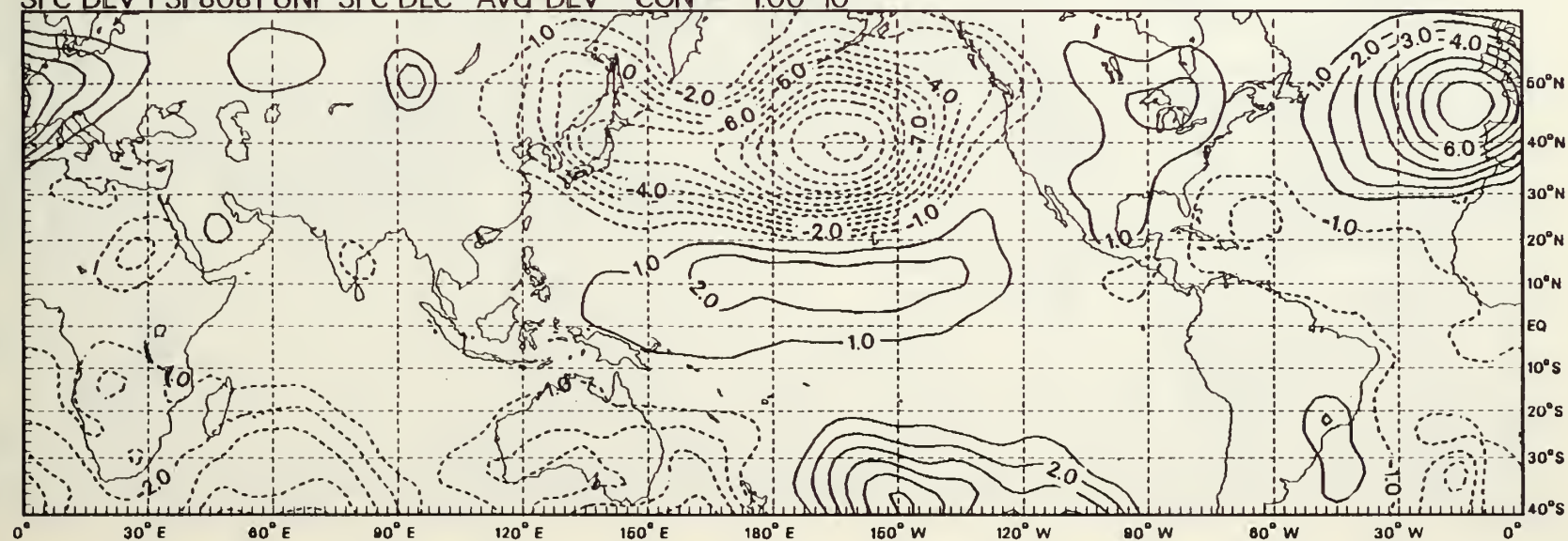


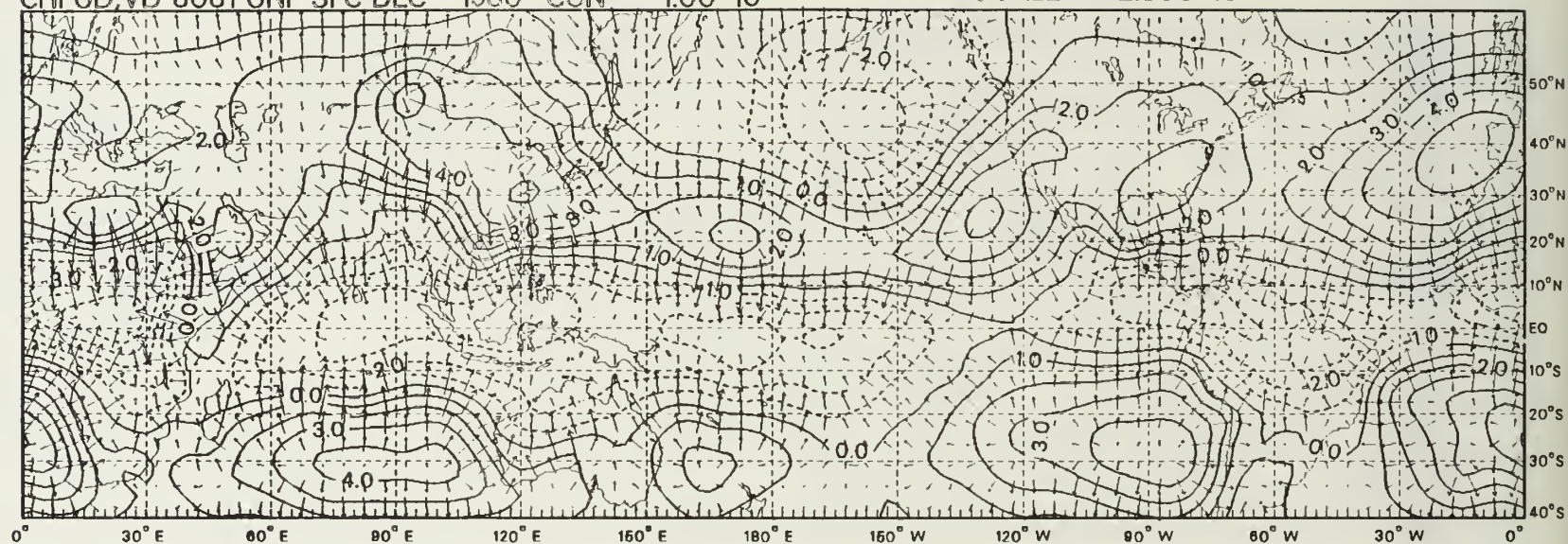
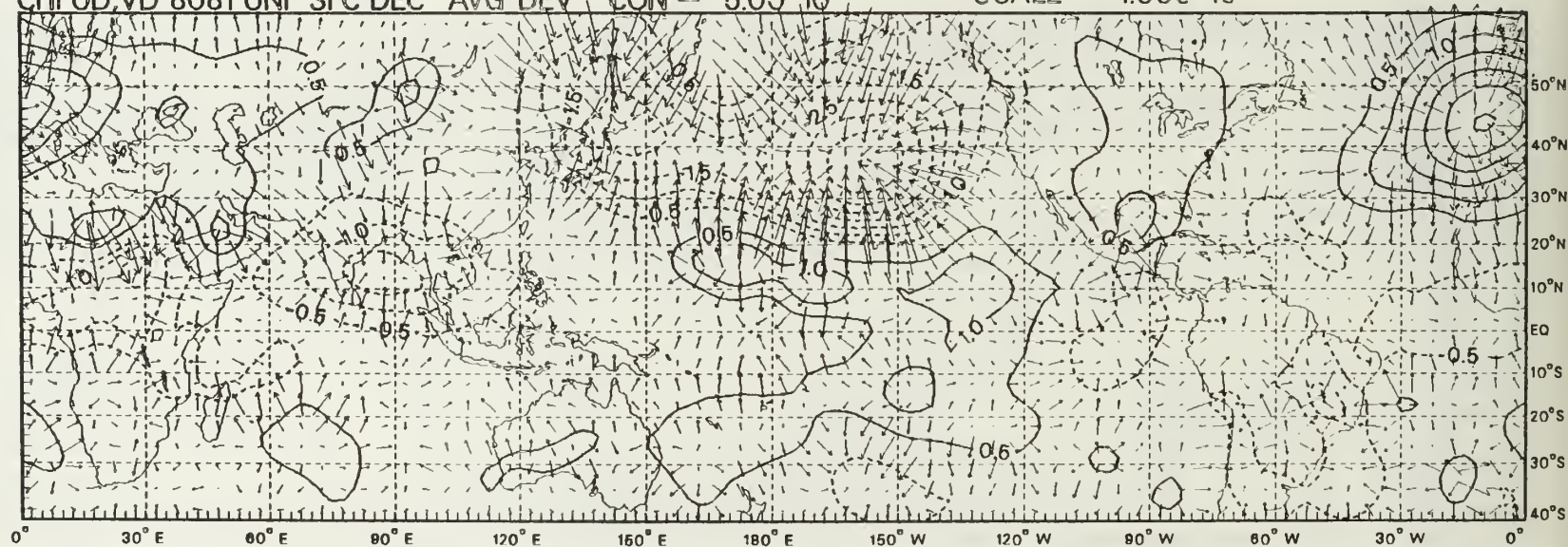
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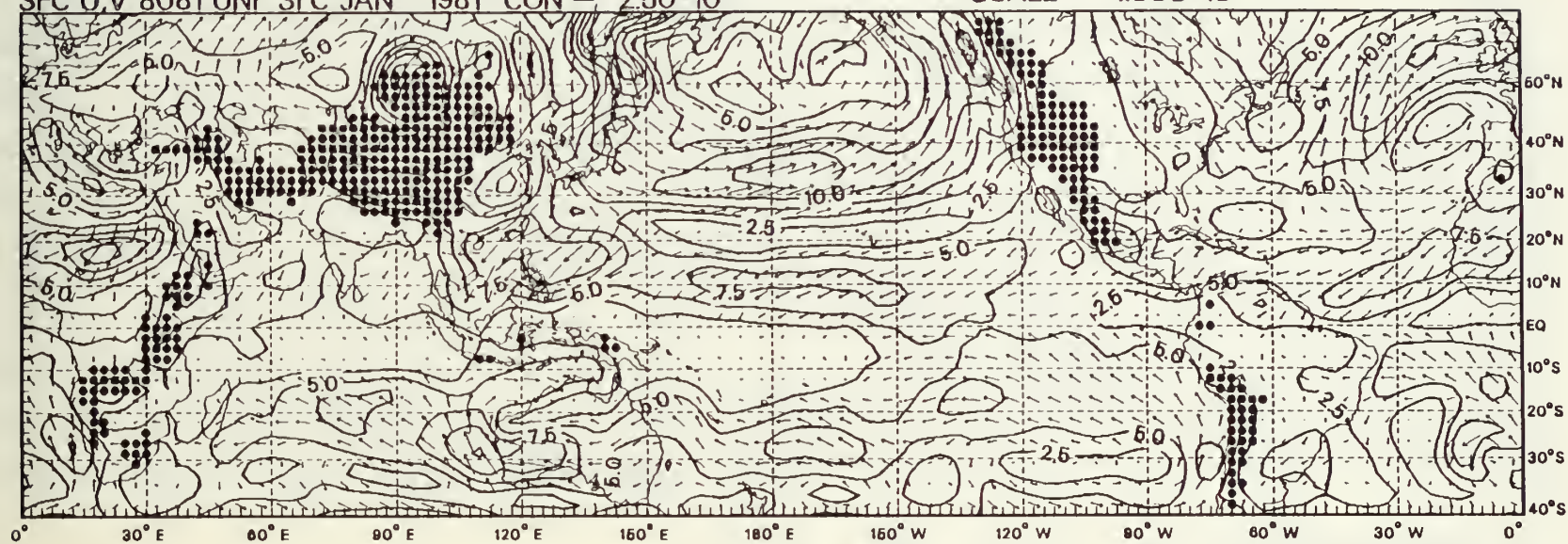
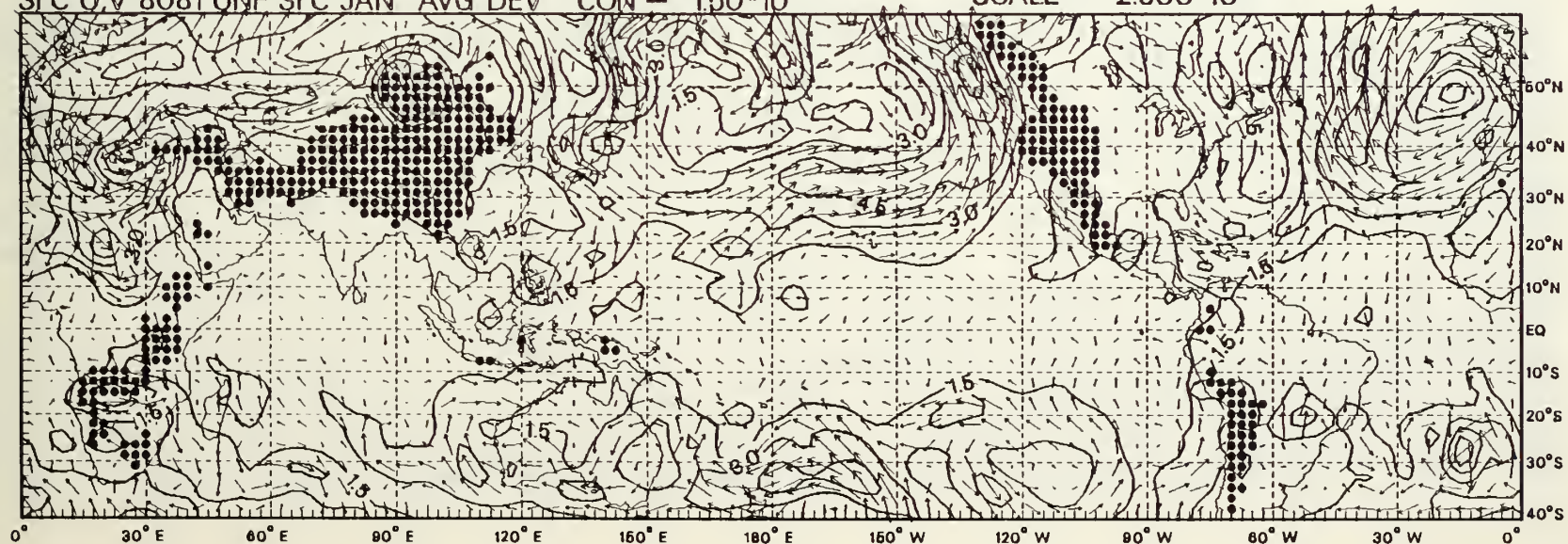
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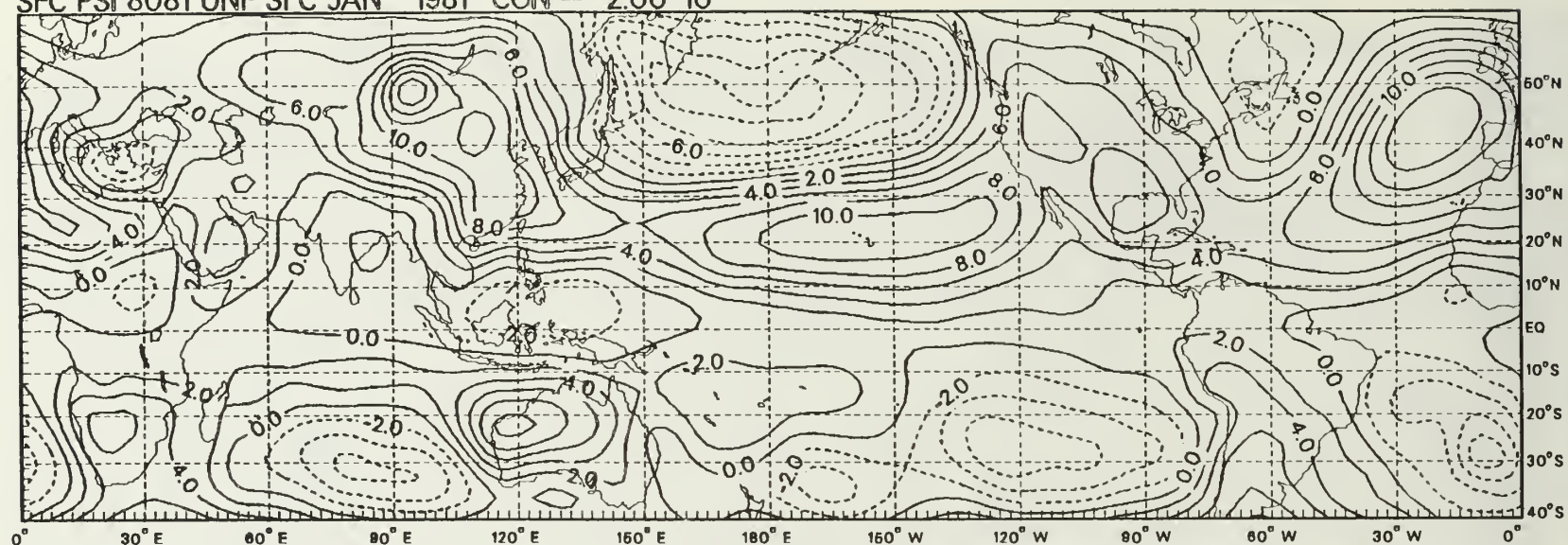
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CHI UD,VD 8081 UNF SFC DEC 1980 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$  —CHI UD,VD 8081 UNF SFC DEC AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$  —

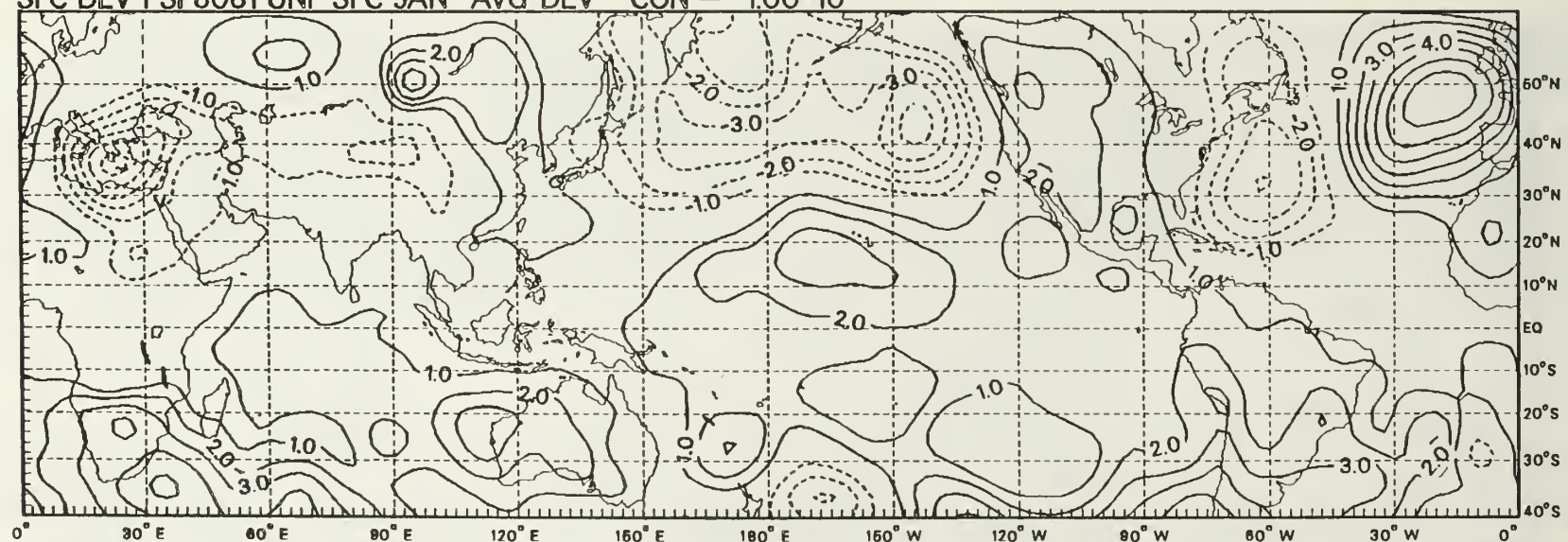


SFC U,V 8081 UNF SFC JAN 1981 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U,V 8081 UNF SFC JAN AVG DEV CON =  $1.50 \times 10^0$ SCALE =  $2.500 \times 10^0$  —

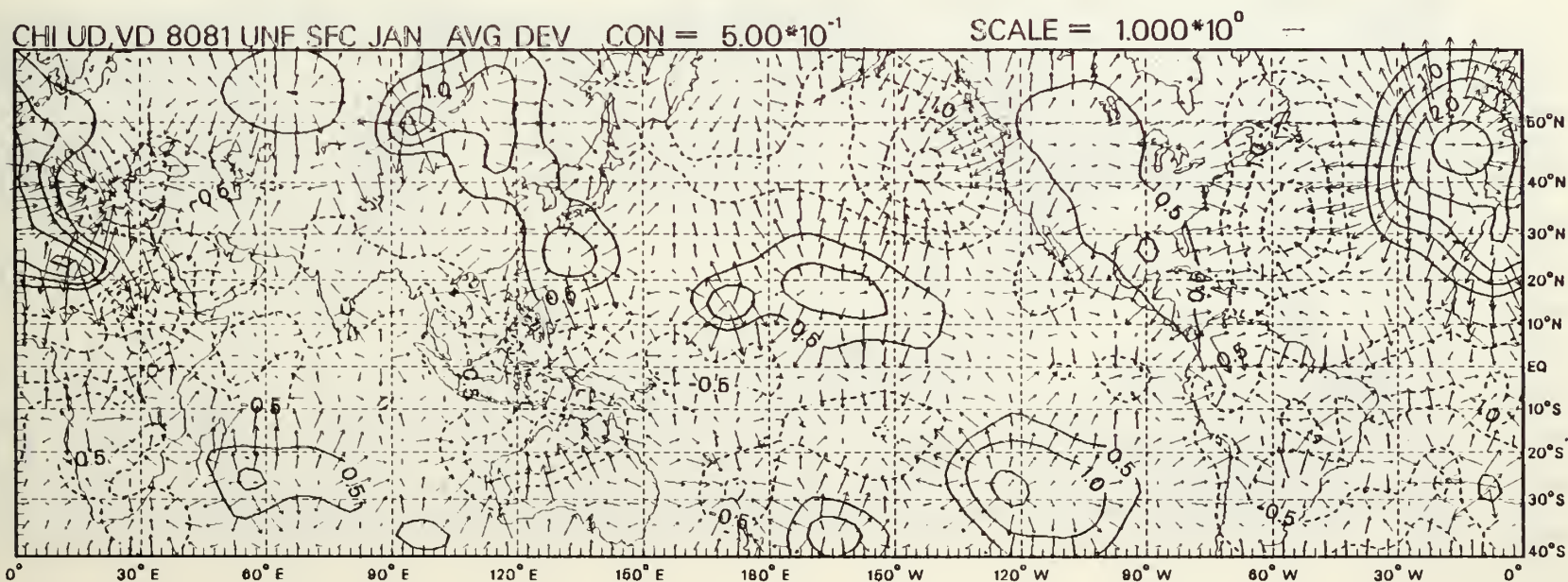
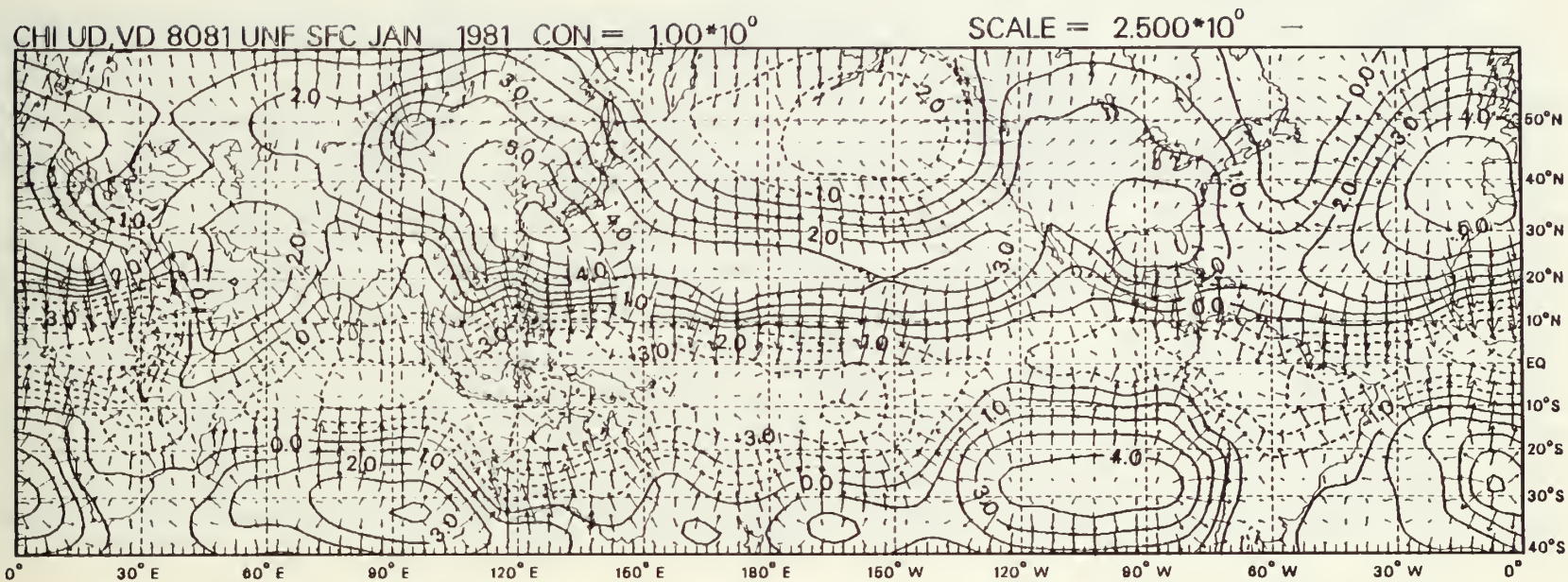
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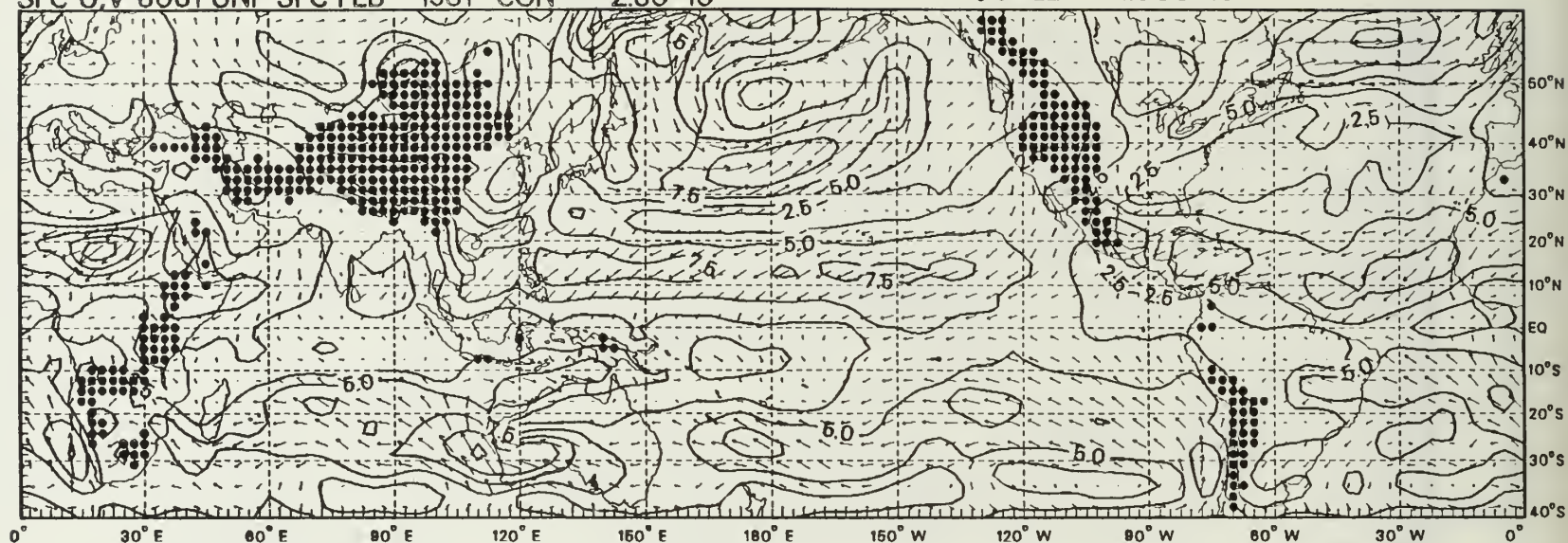
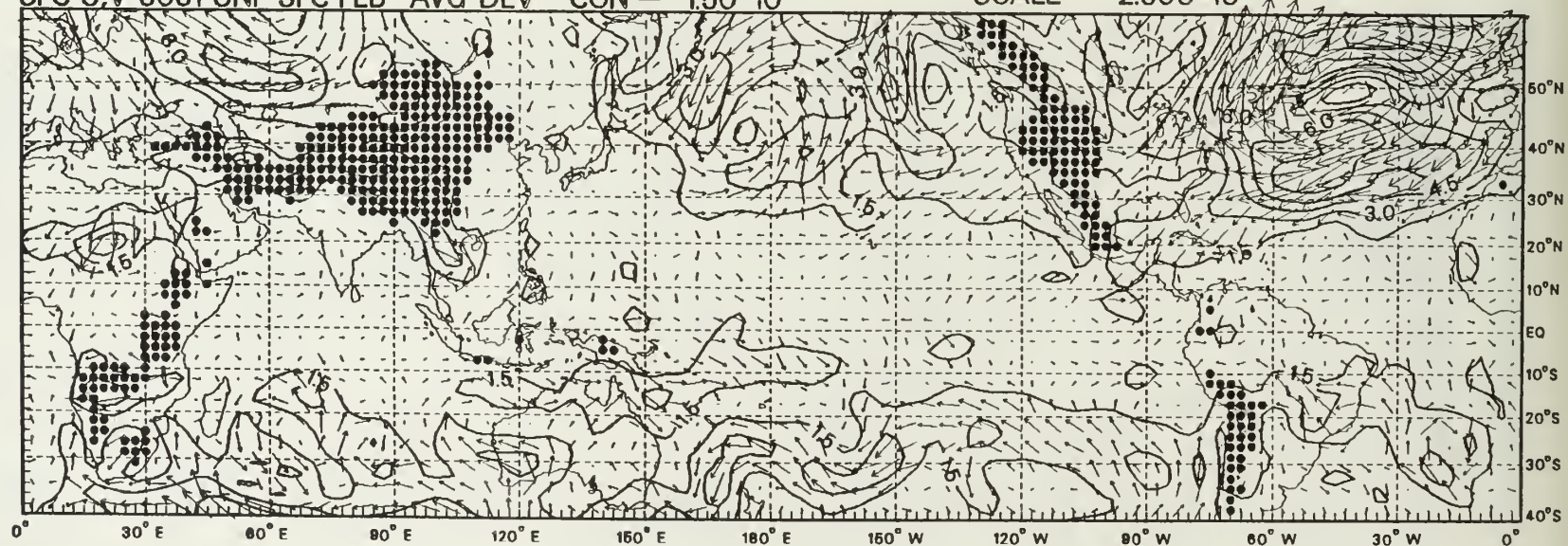
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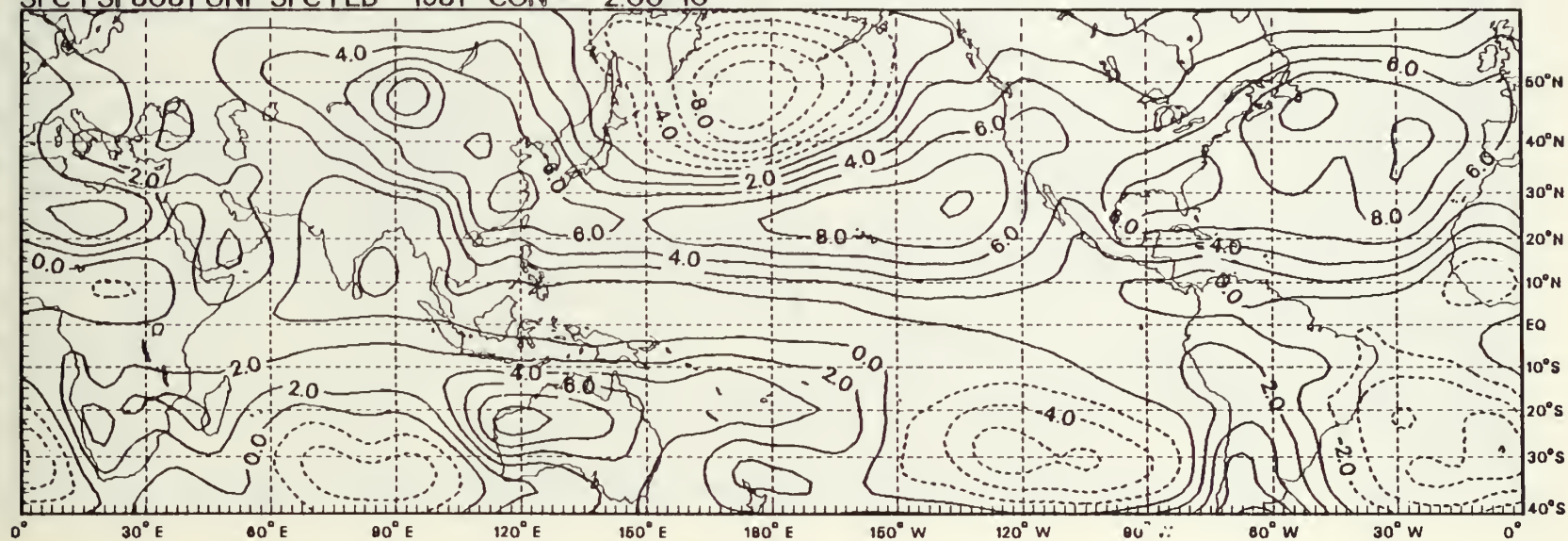
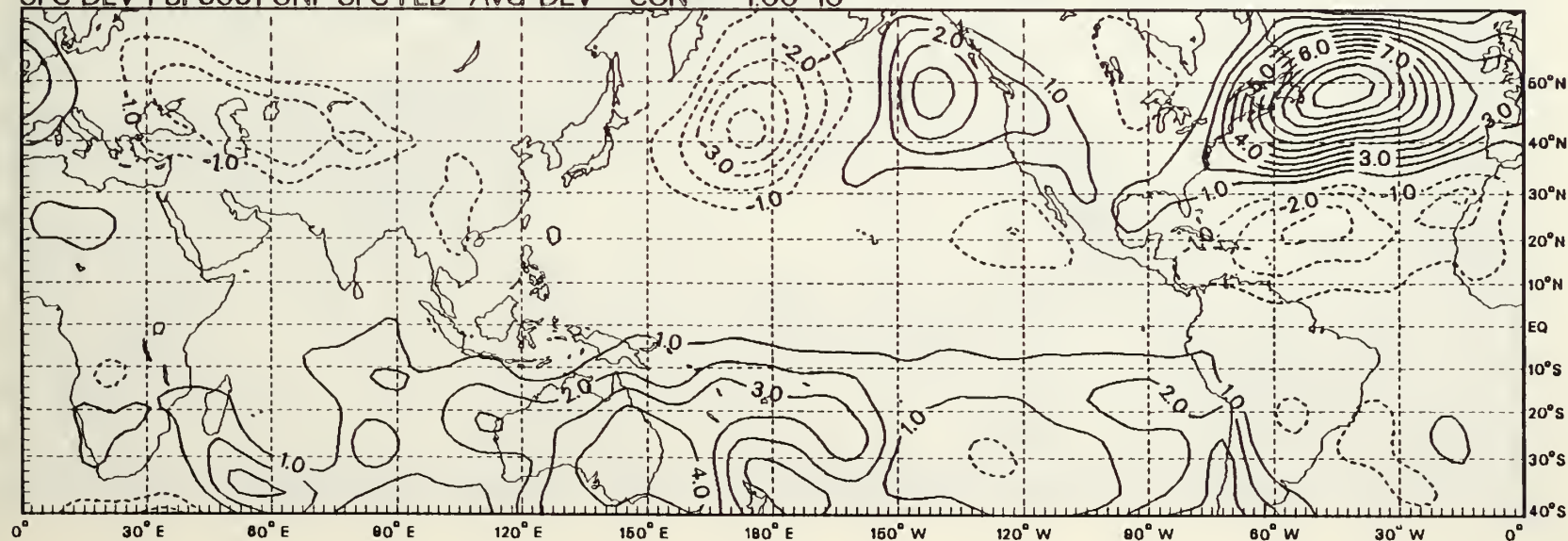


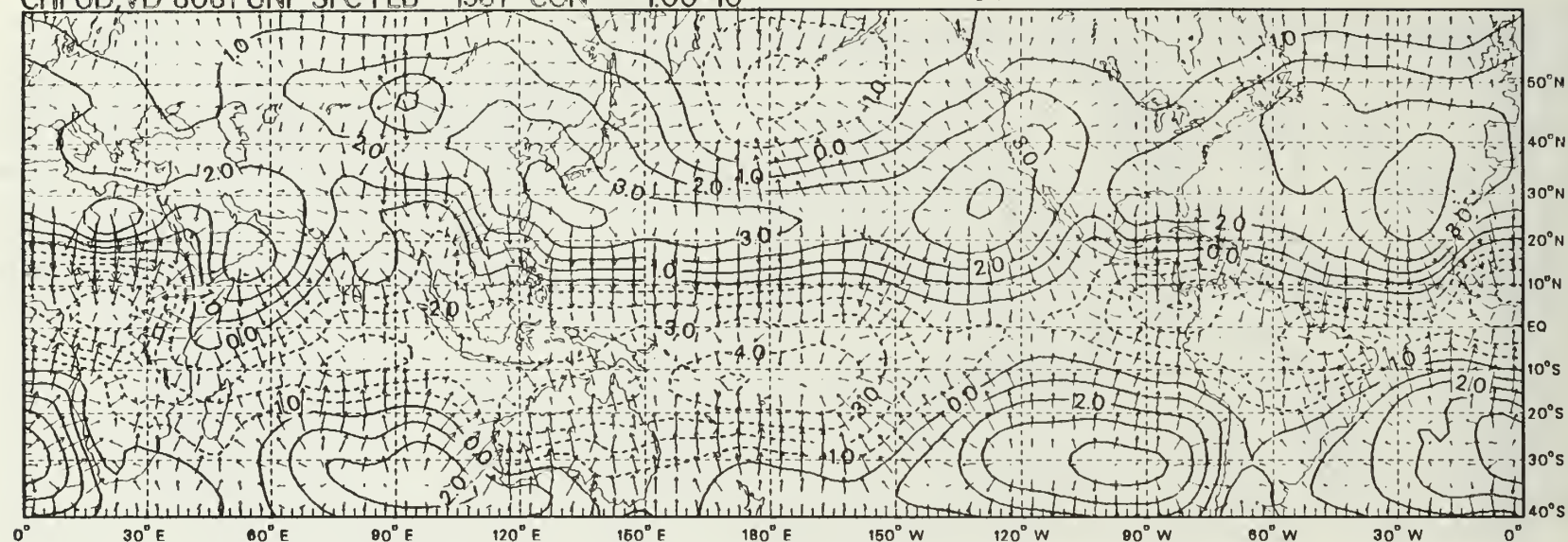
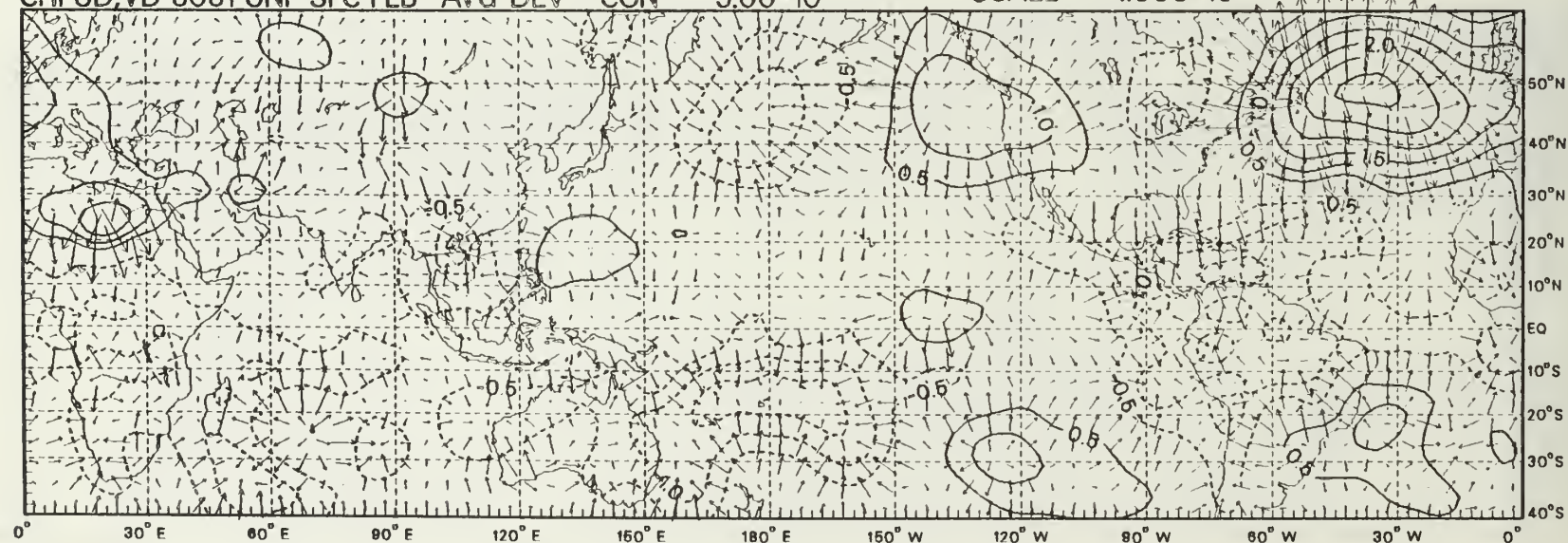




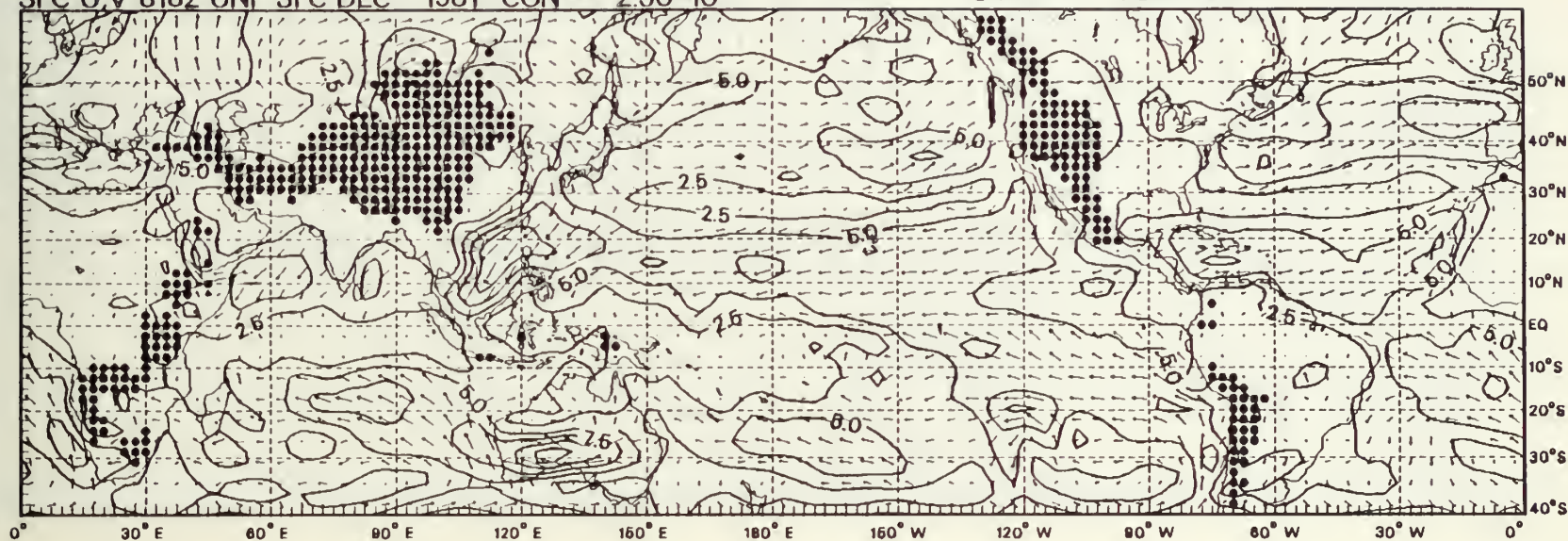
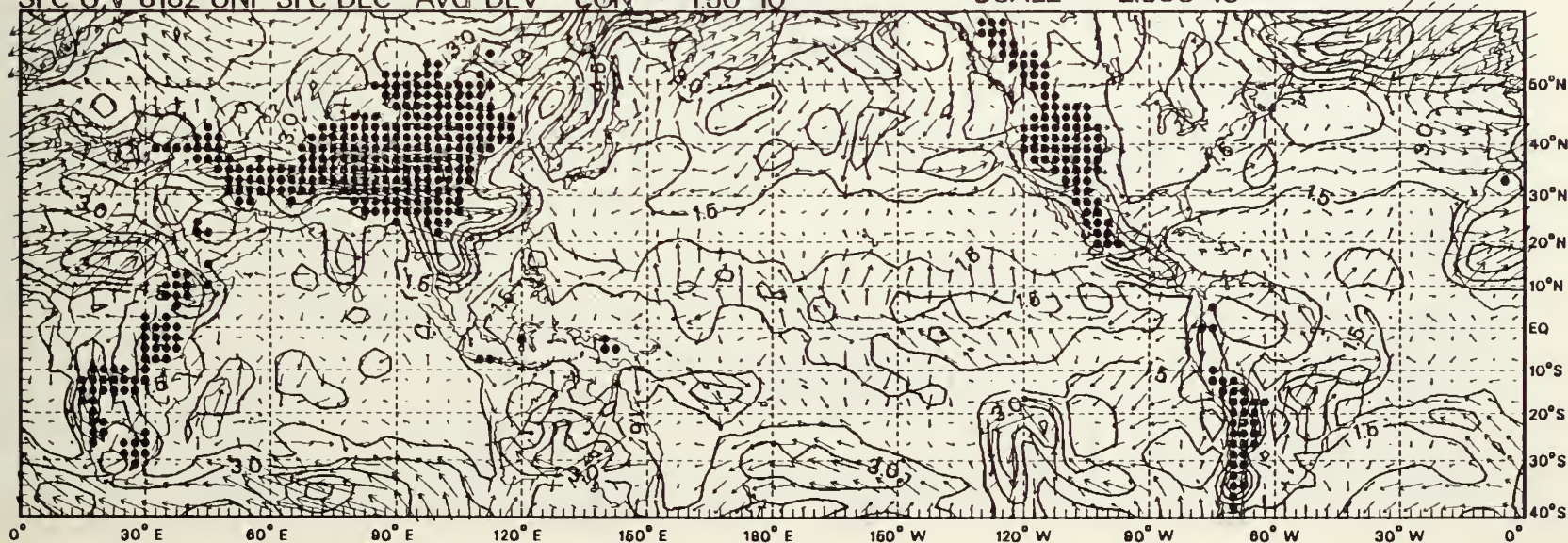
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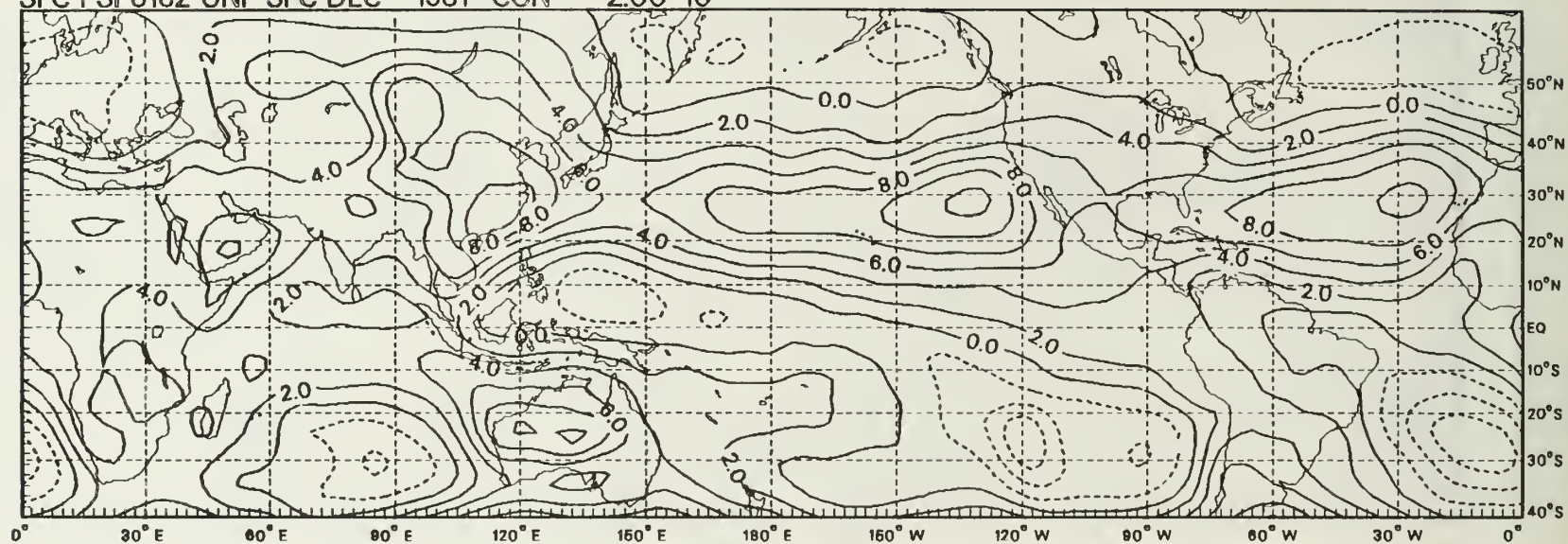
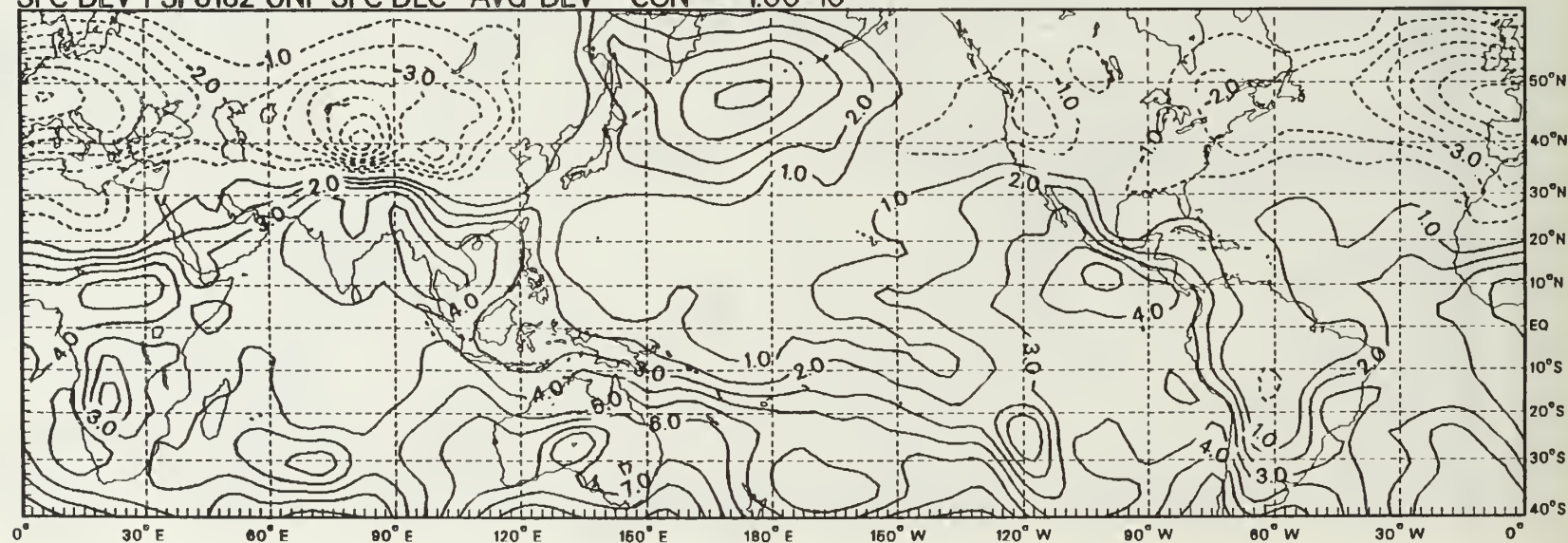


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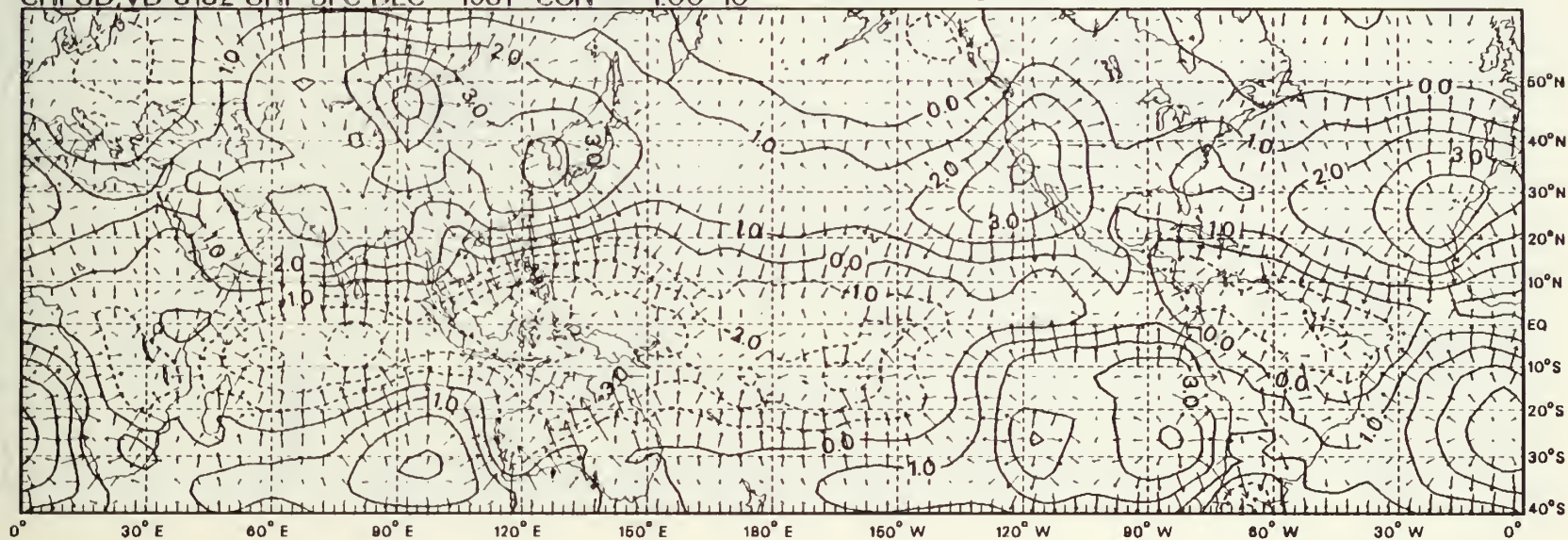
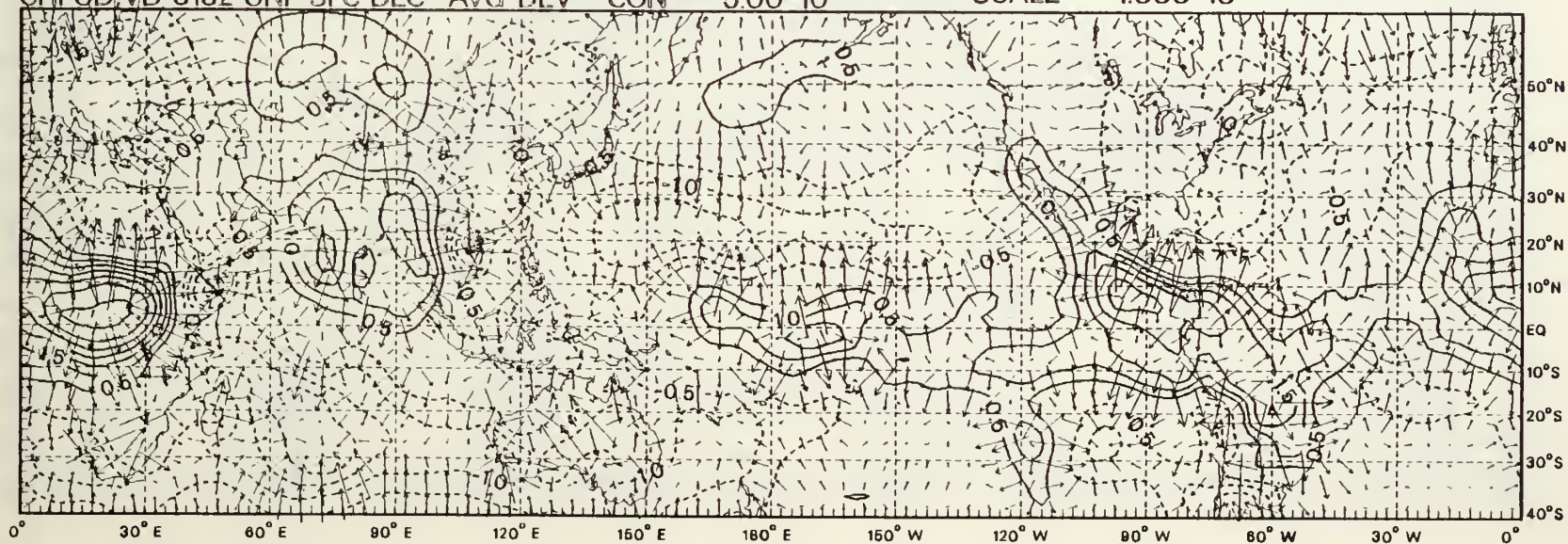
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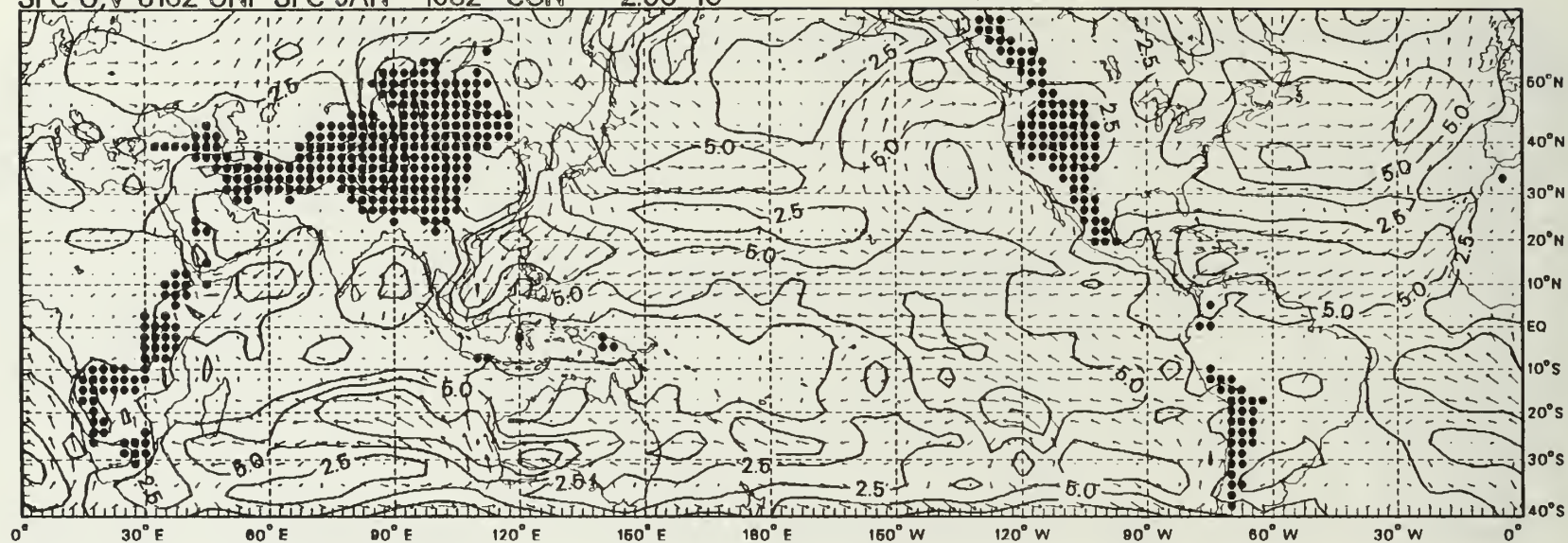
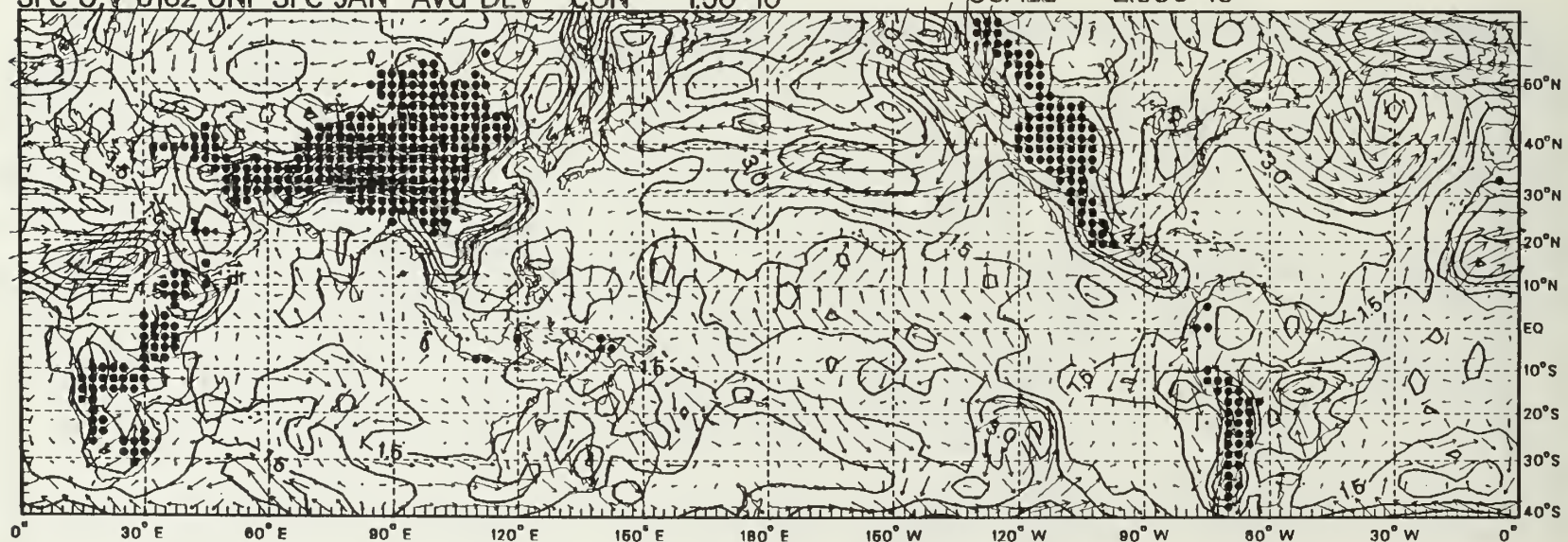
SFC U.V 8182 UNF SFC DEC 1981 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U.V 8182 UNF SFC DEC AVG DEV CON =  $150 \times 10^0$ SCALE =  $2500 \times 10^0$  —

SFC PSI 8182 UNF SFC DEC 1981 CON =  $2.00 \times 10^0$ SFC DEV PSI 8182 UNF SFC DEC AVG DEV CON =  $1.00 \times 10^0$ 

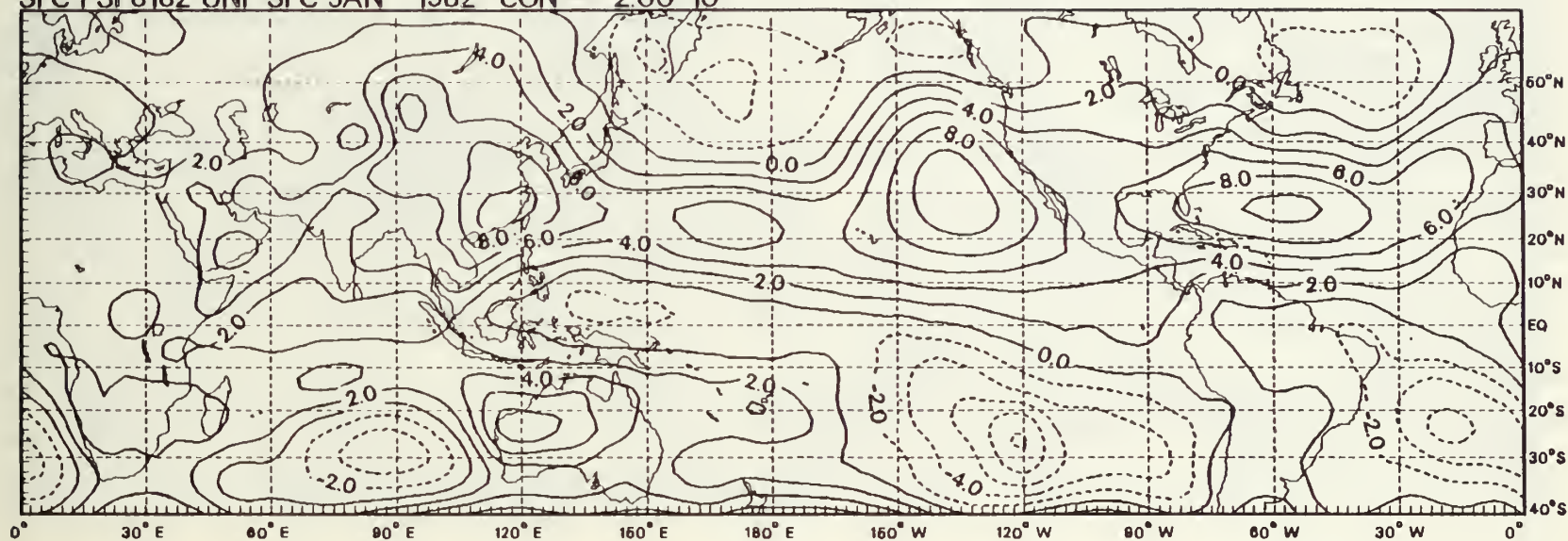
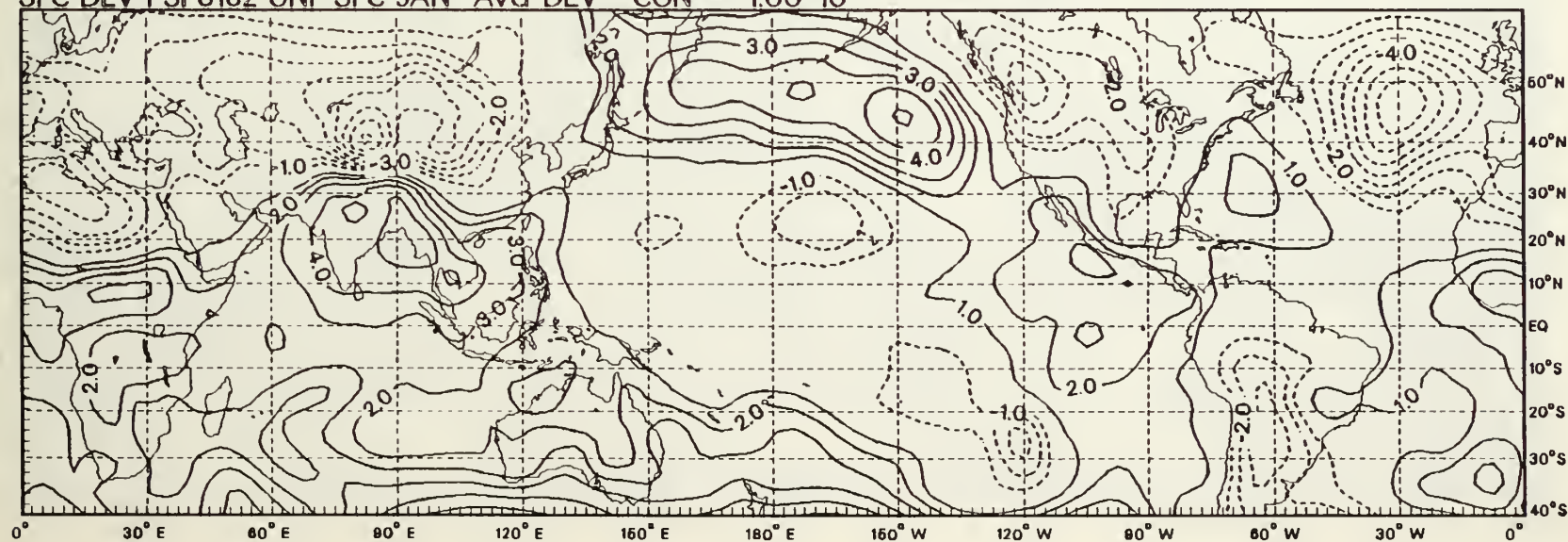


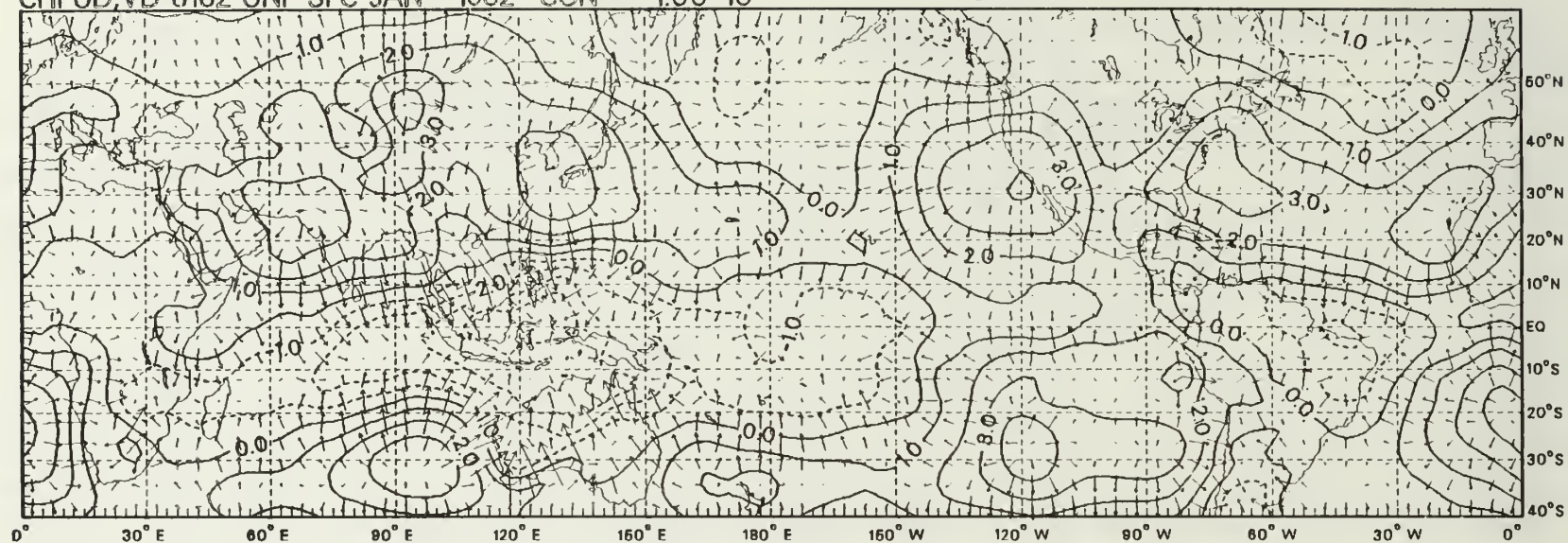
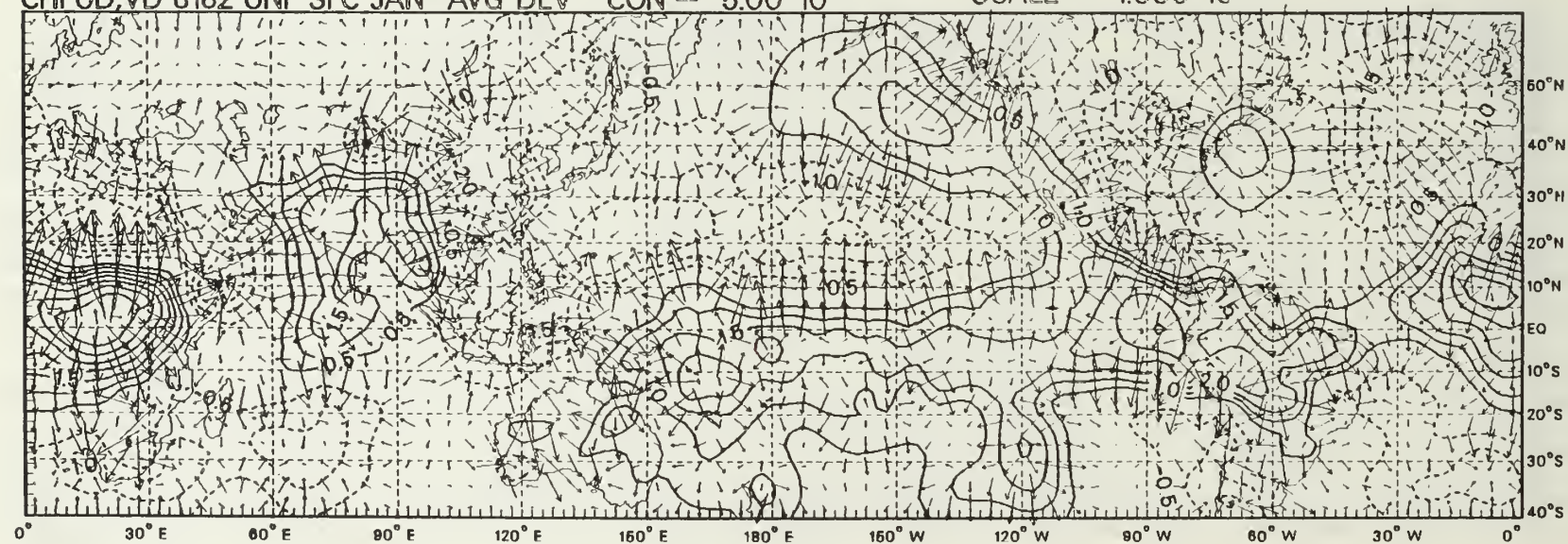
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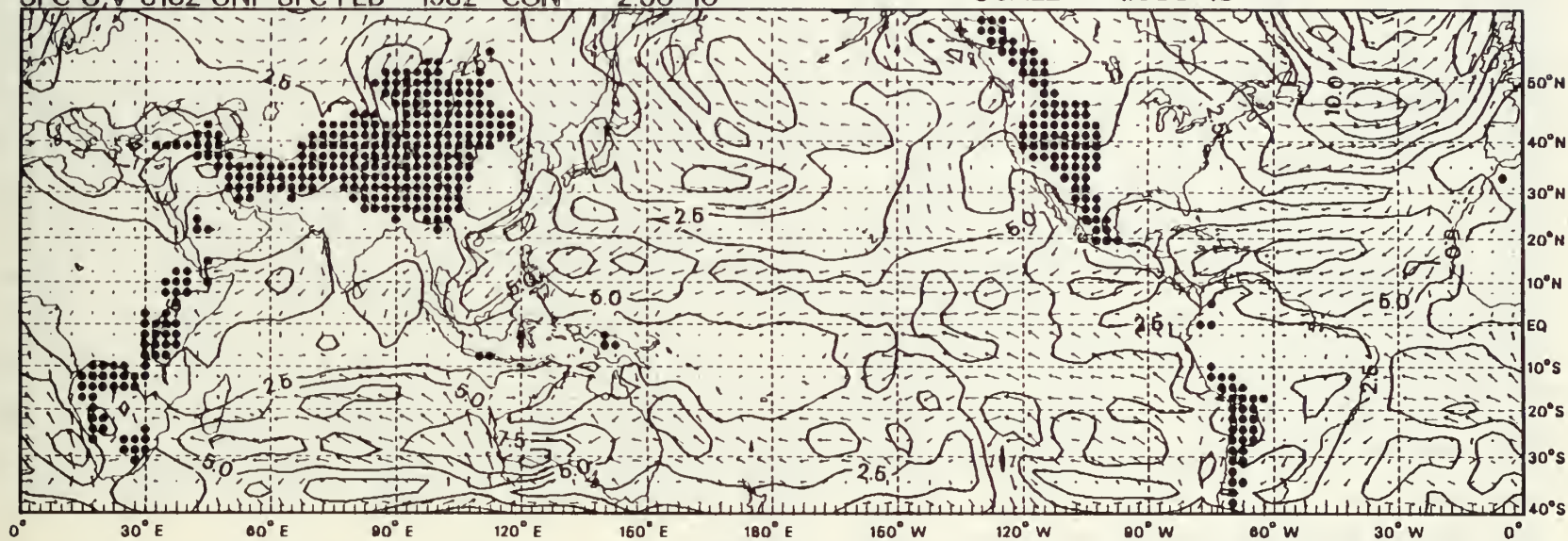
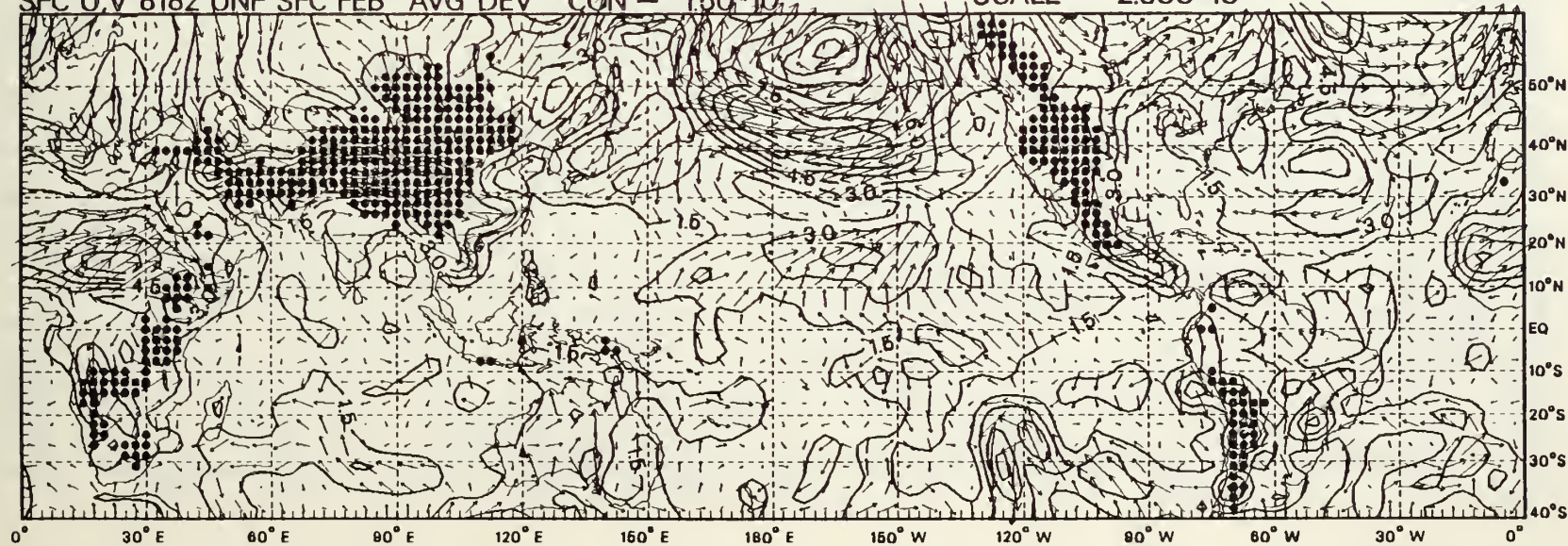
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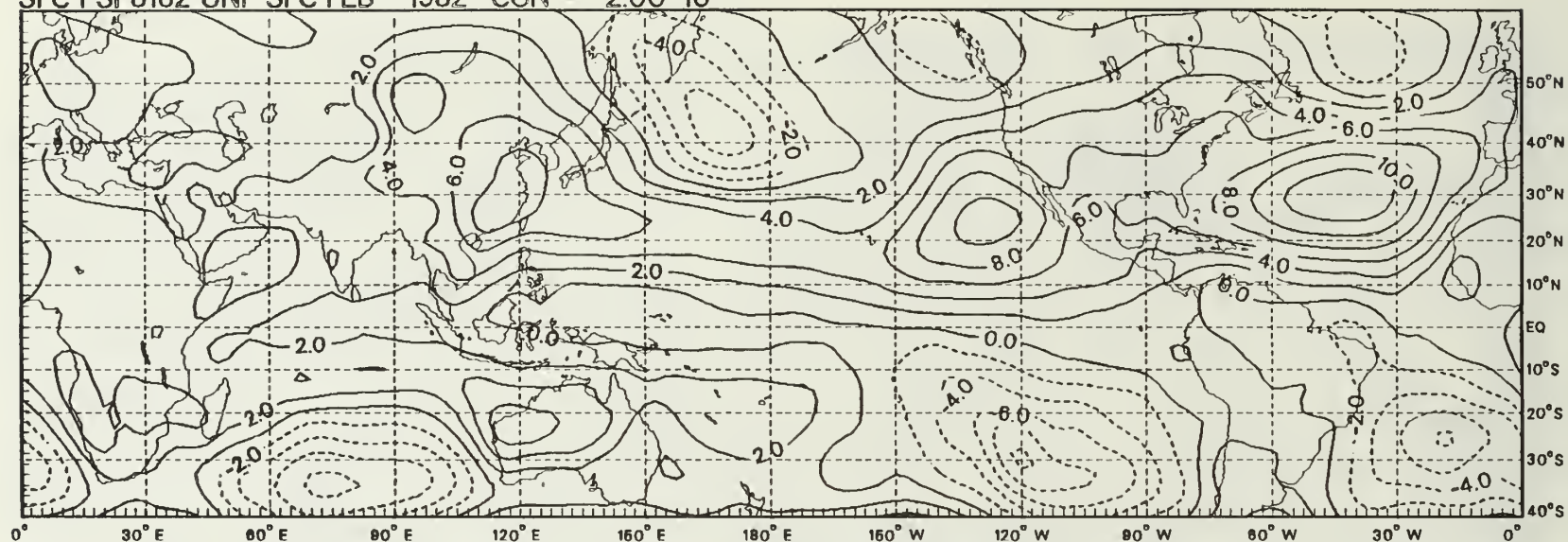
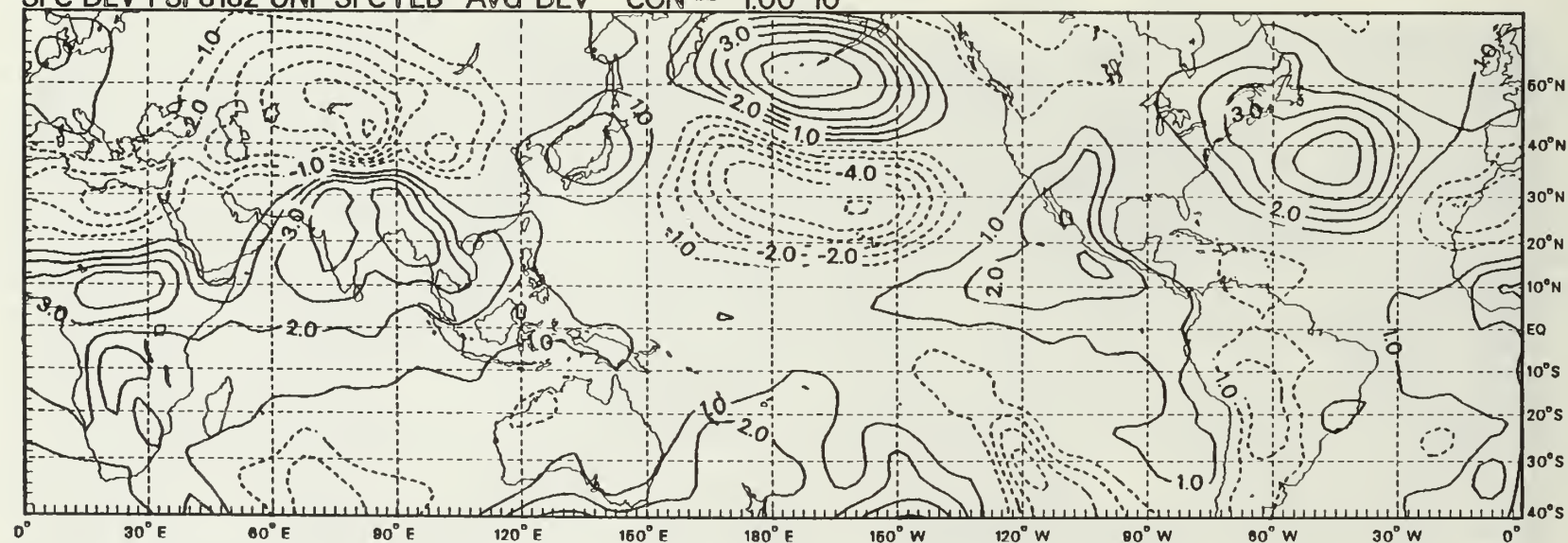


SFC PSI 8182 UNF SFC JAN 1982 CON =  $2.00 \times 10^0$ SFC DEV PSI 8182 UNF SFC JAN AVG DEV CON =  $1.00 \times 10^0$ 

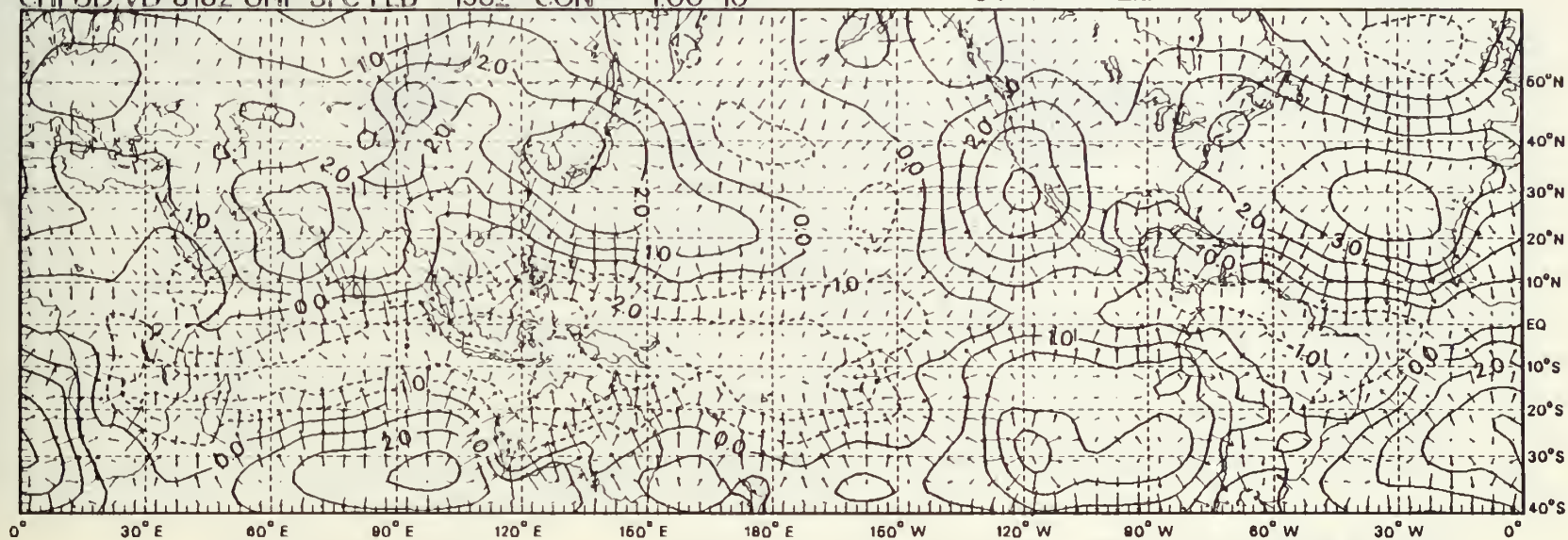
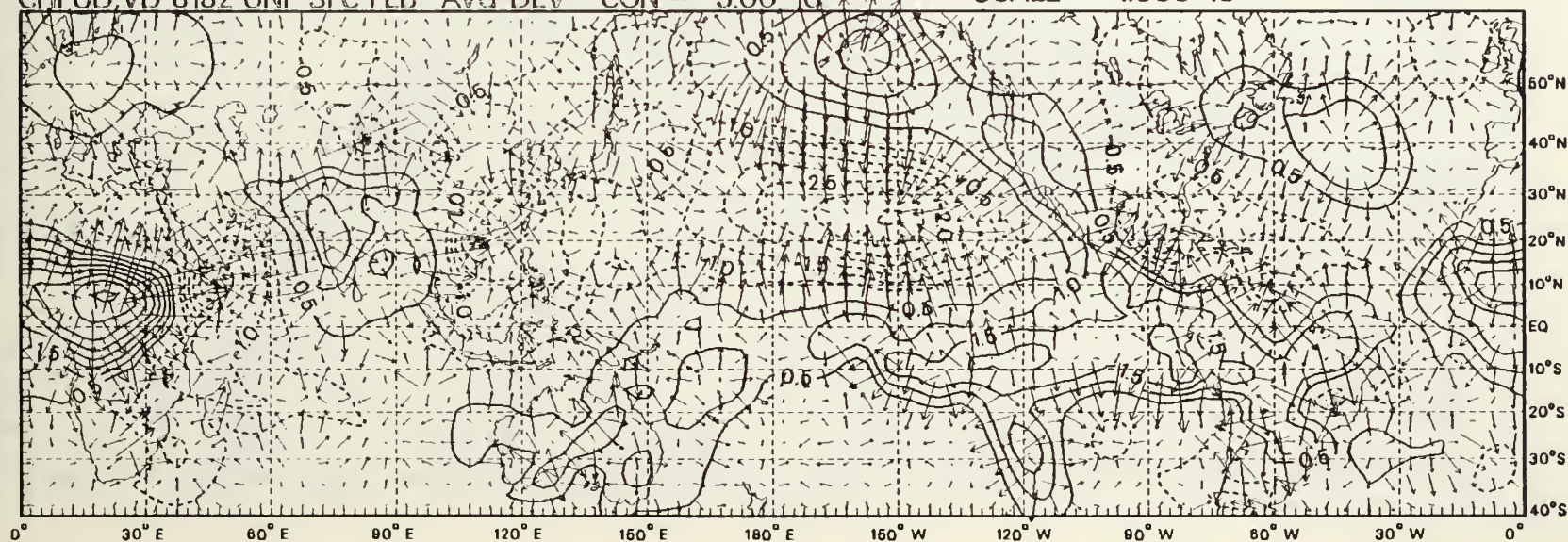
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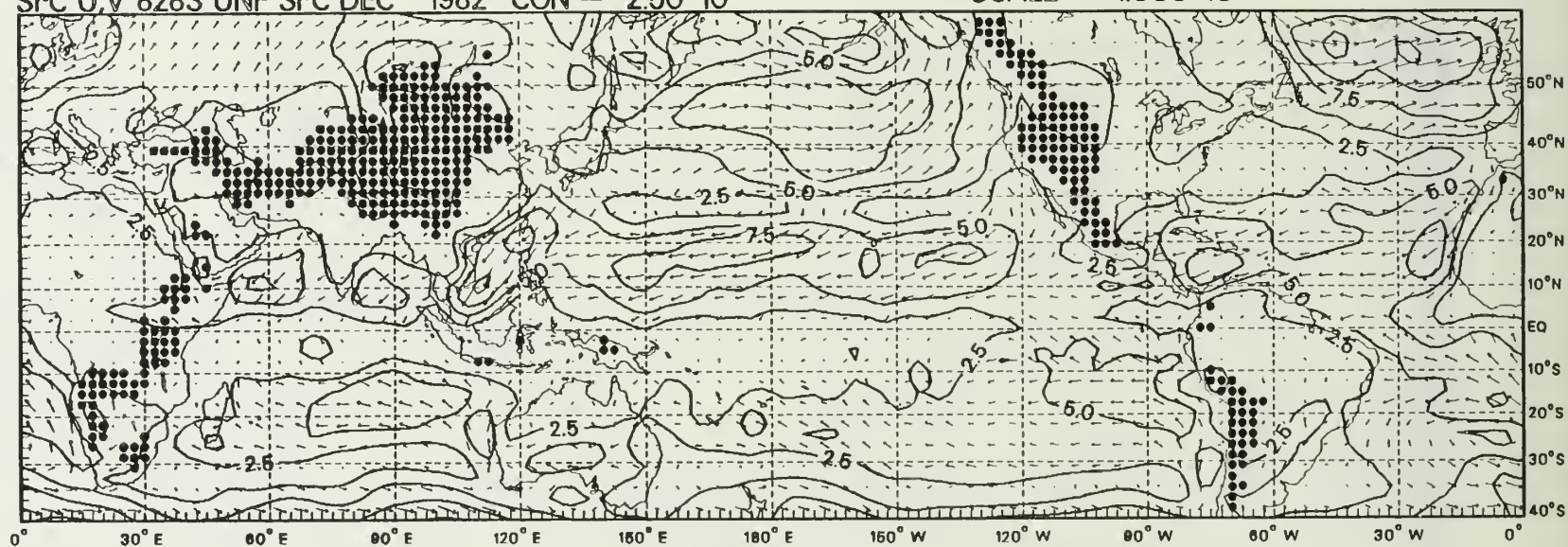
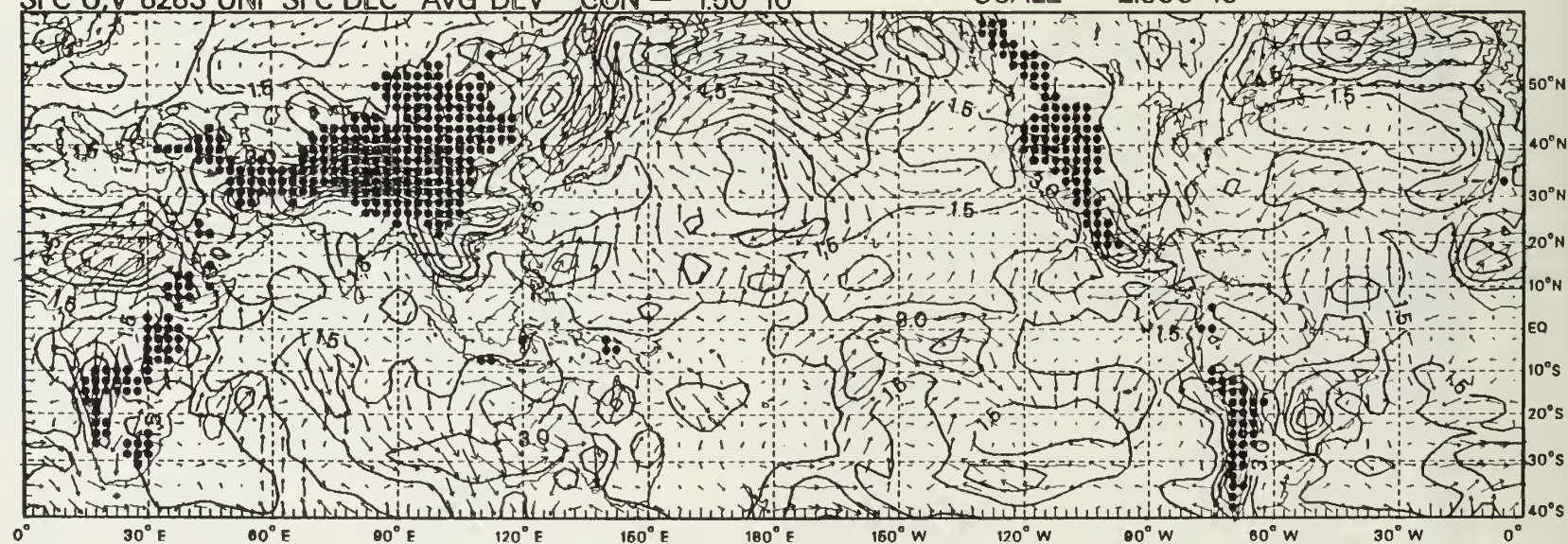
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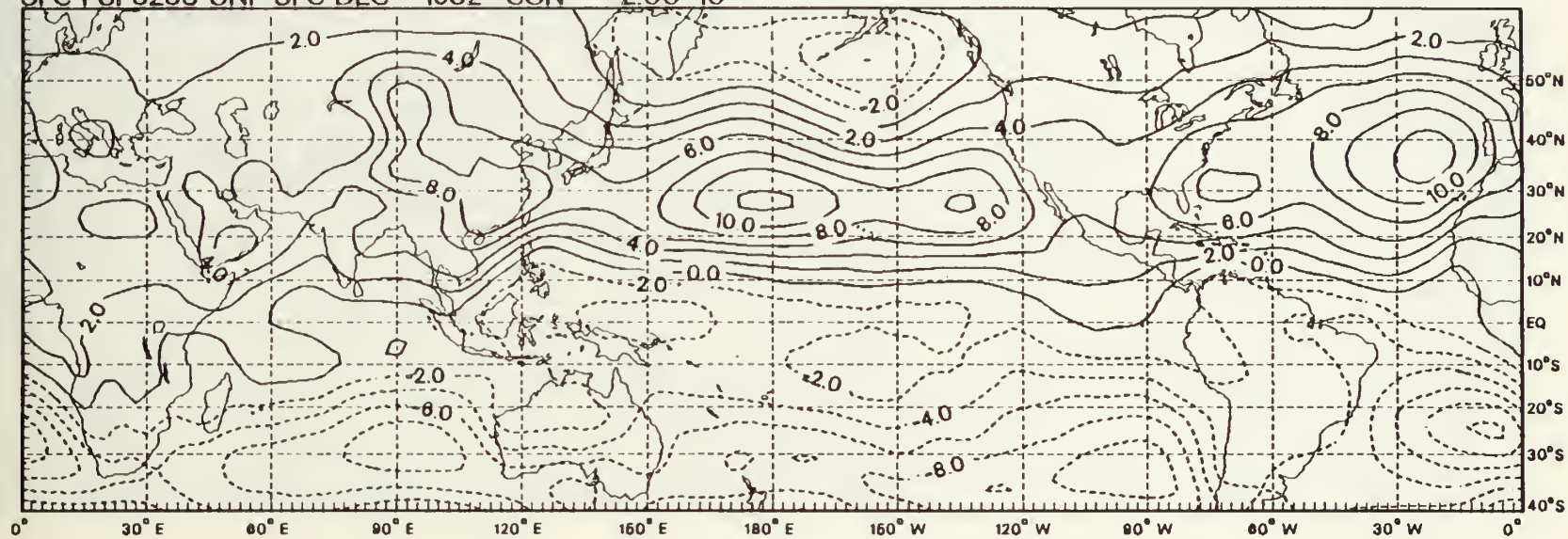
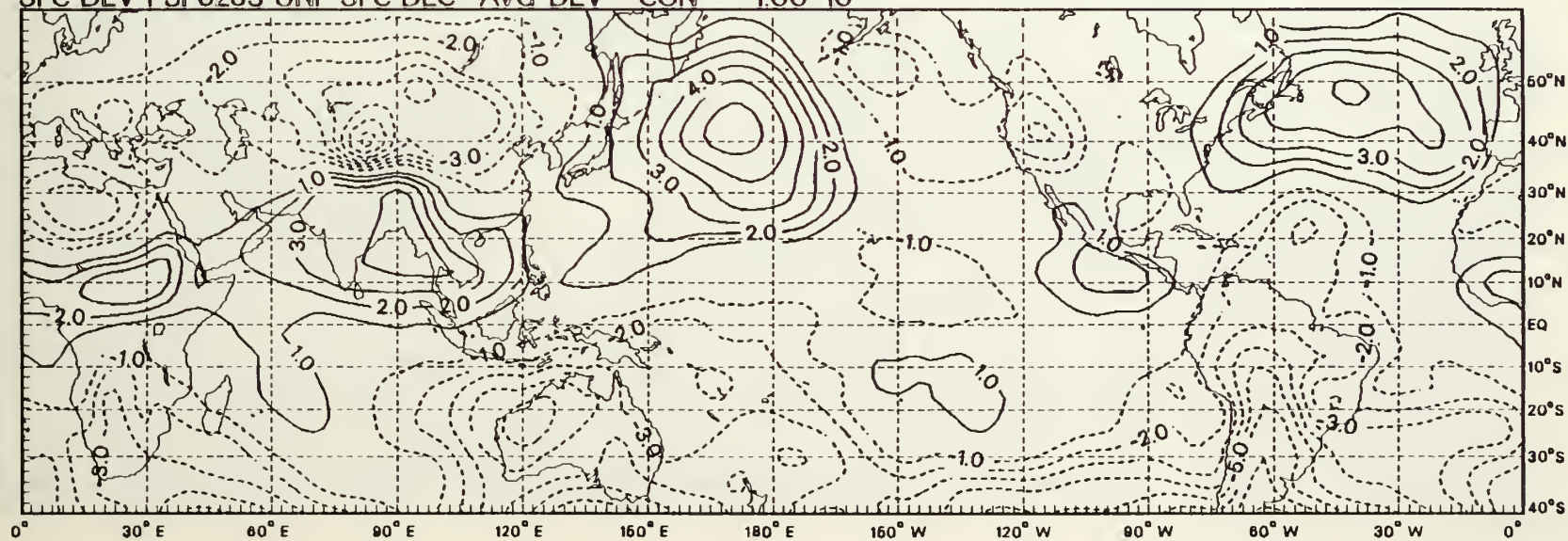


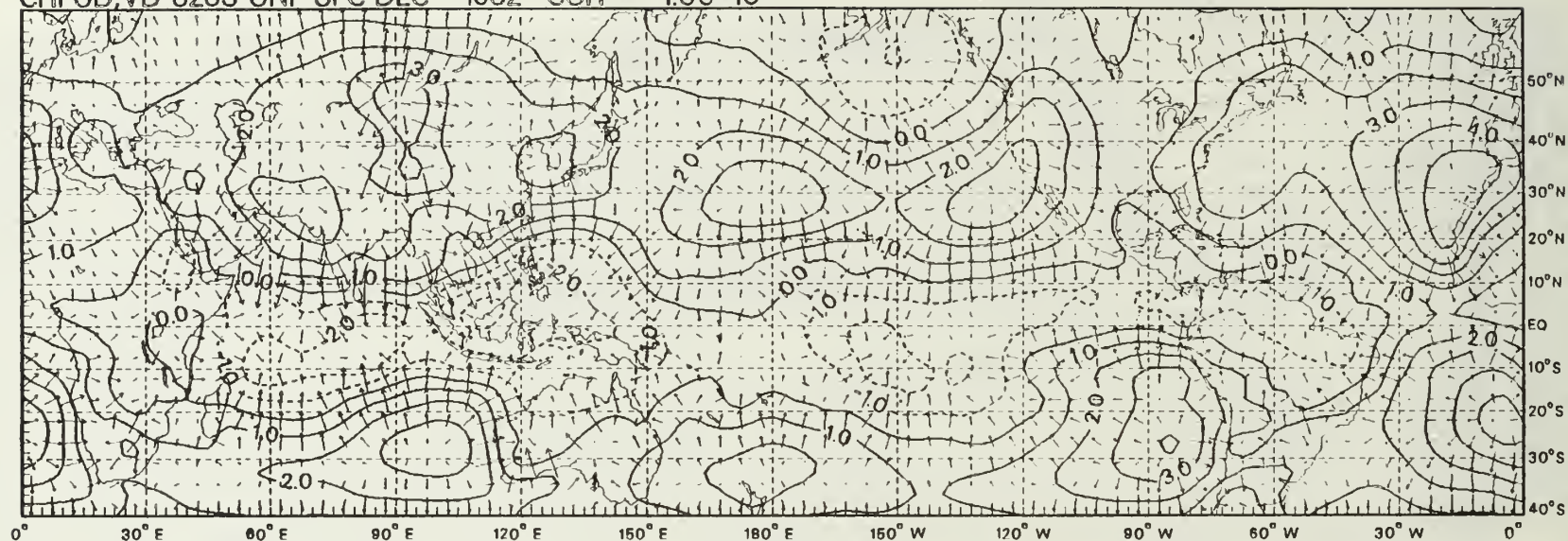
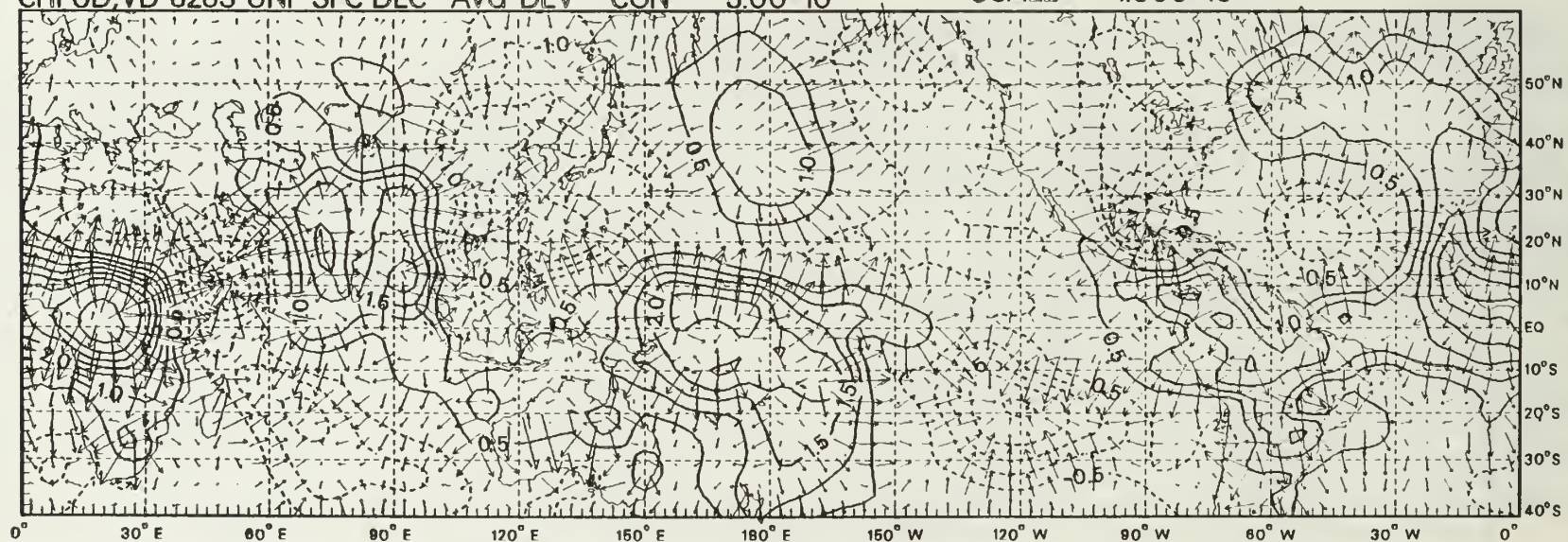
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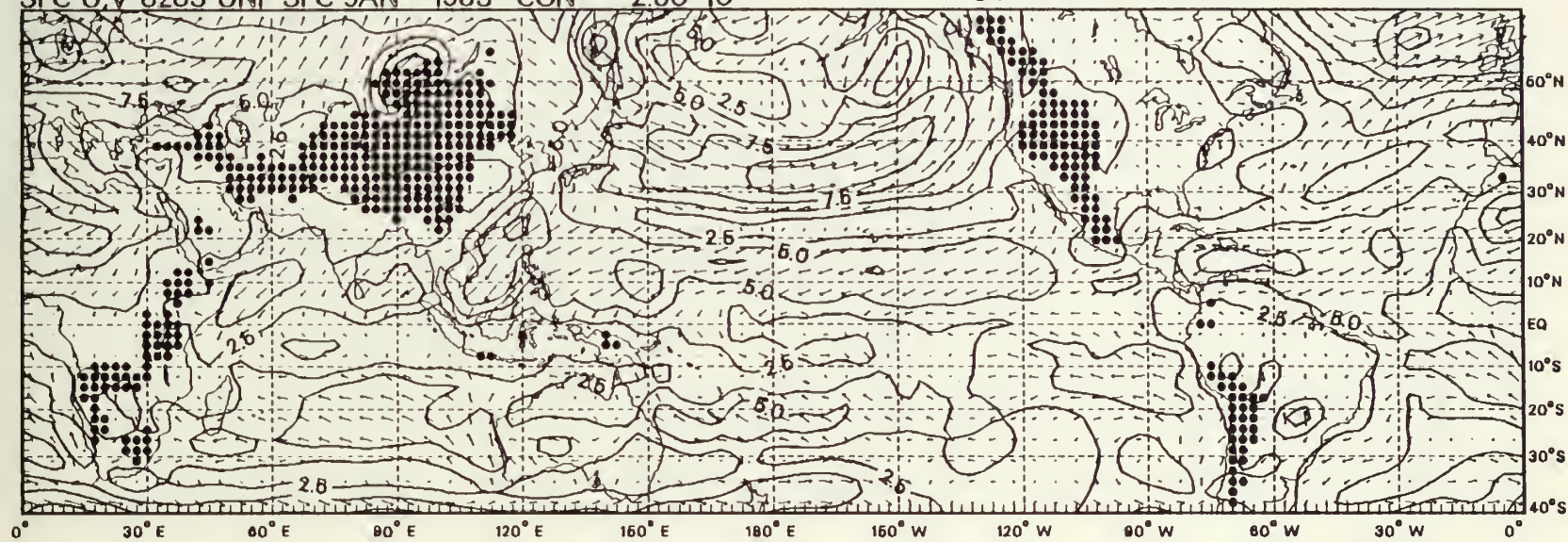
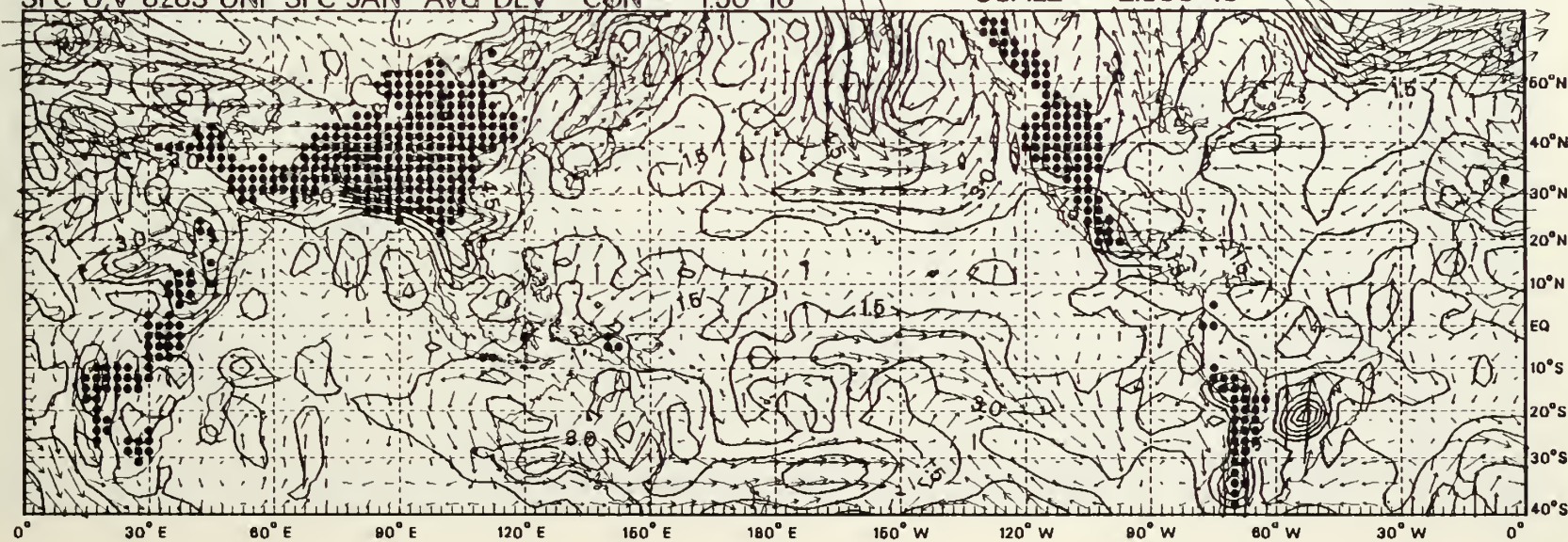
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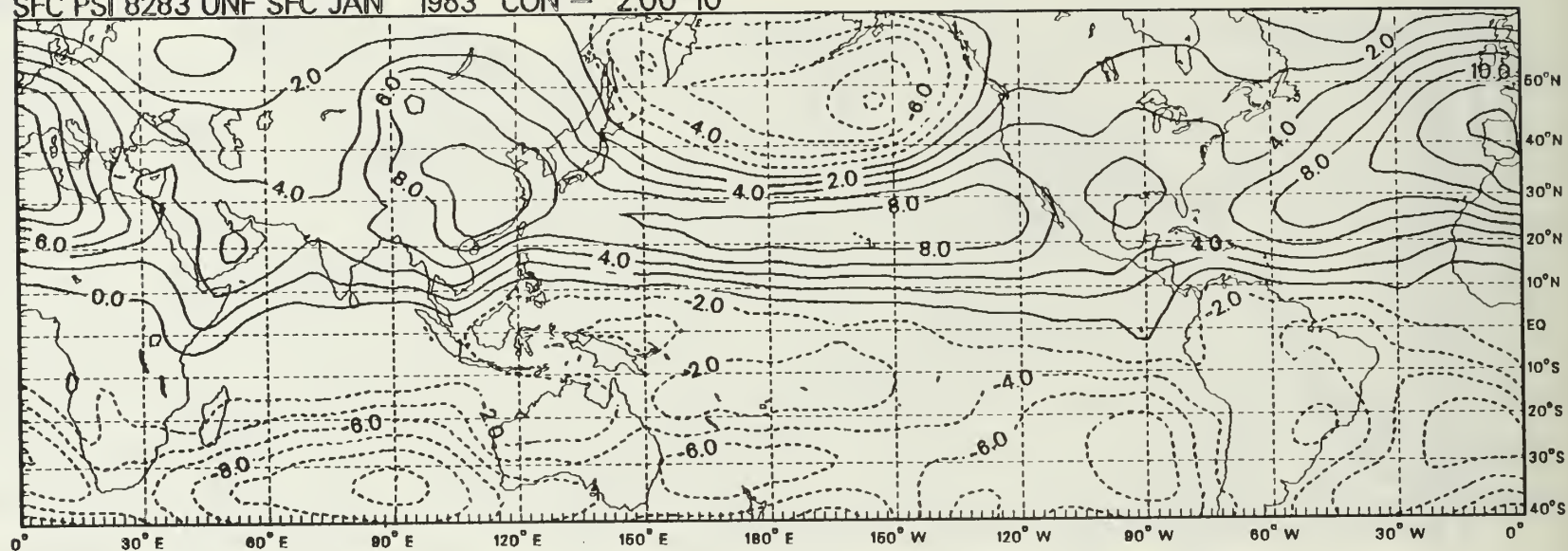
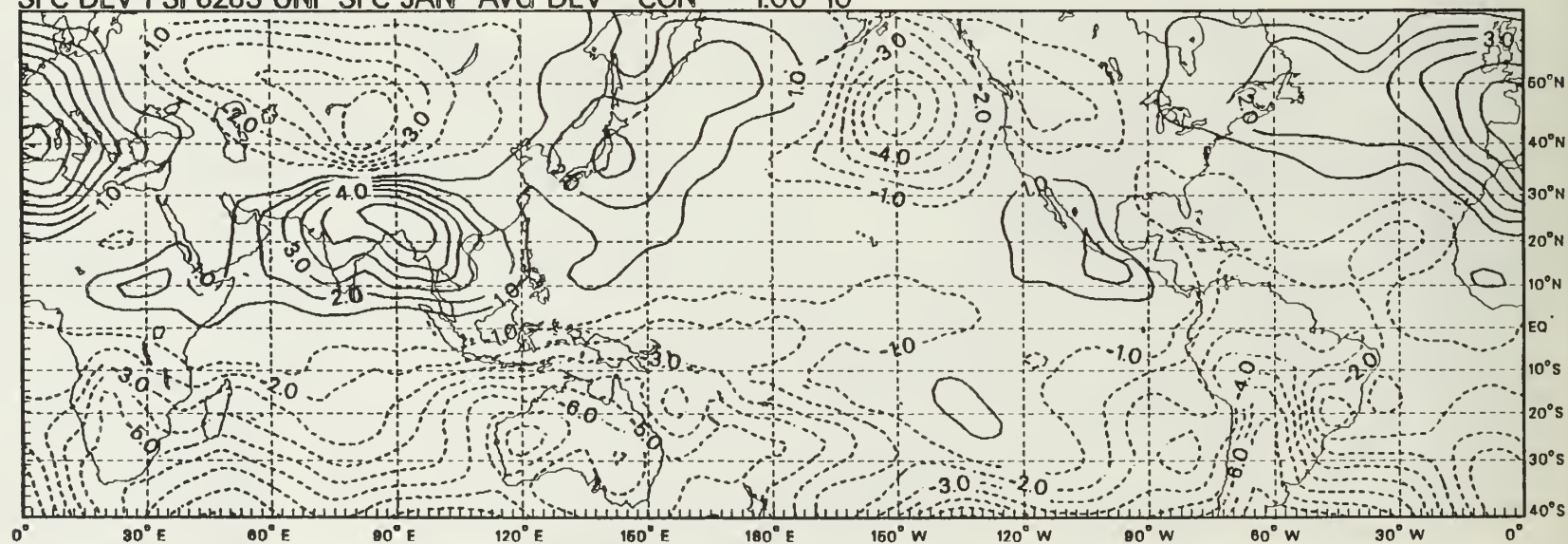
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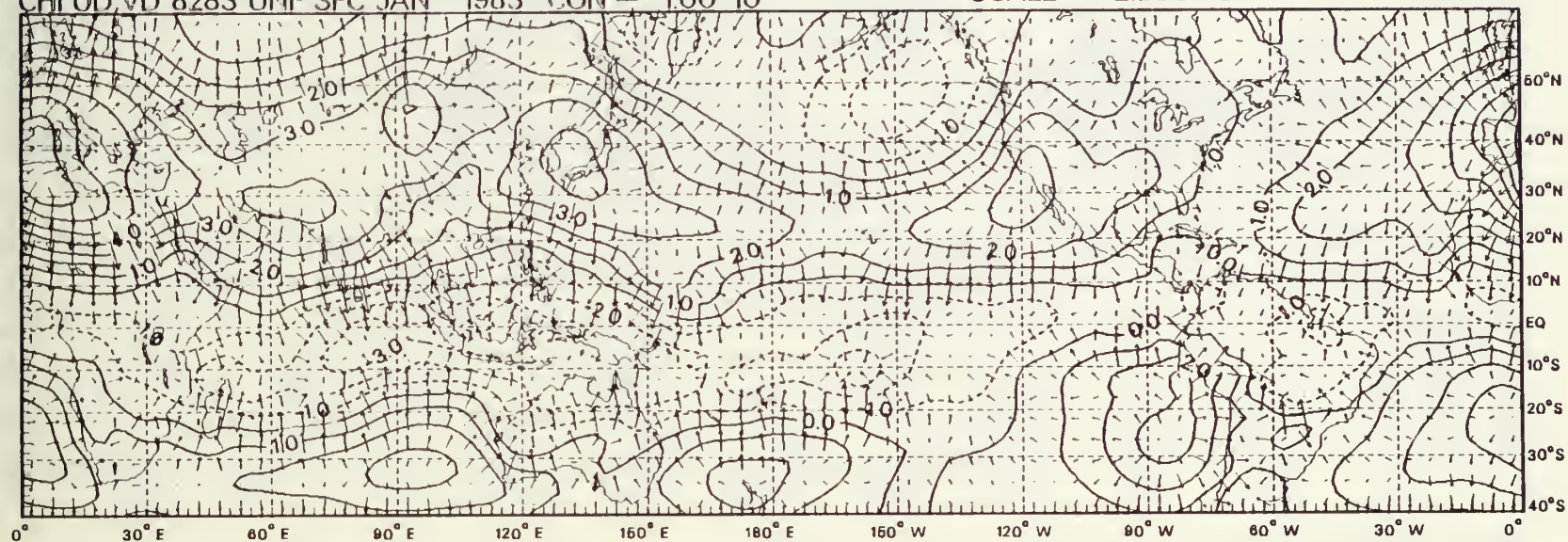
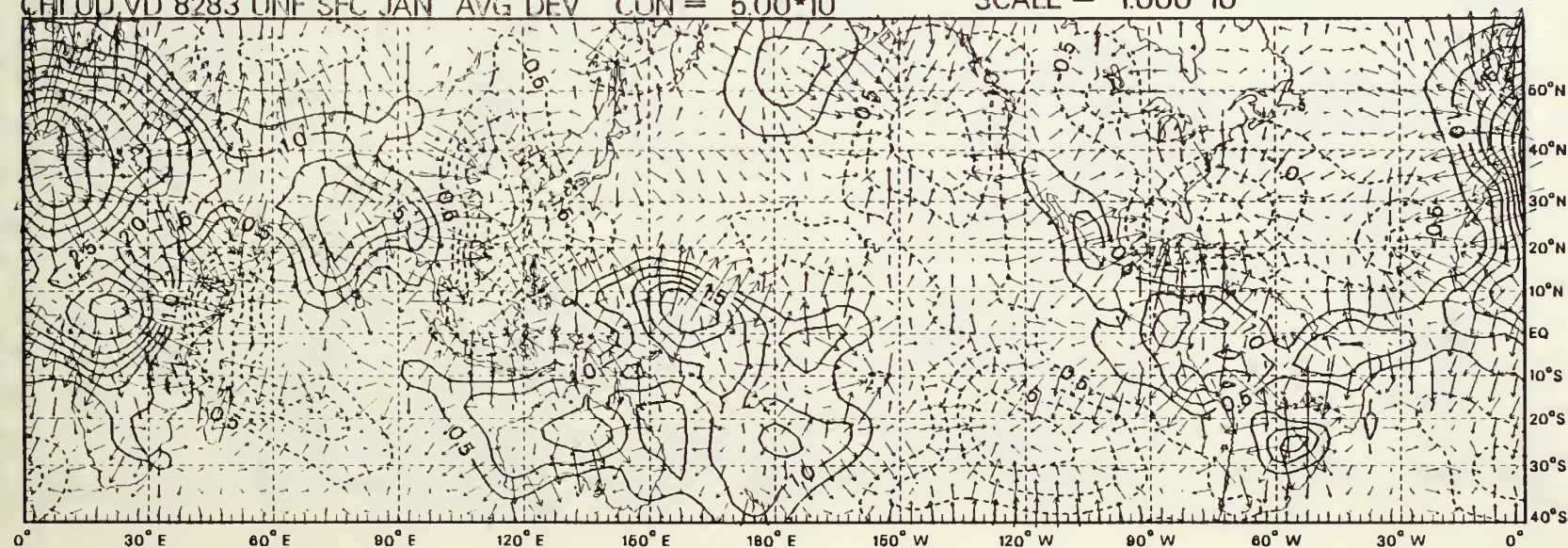


SFC U.V 8283 UNF SFC JAN 1983 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U.V 8283 UNF SFC JAN AVG DEV CON =  $150 \times 10^0$ SCALE =  $2.500 \times 10^0$ 

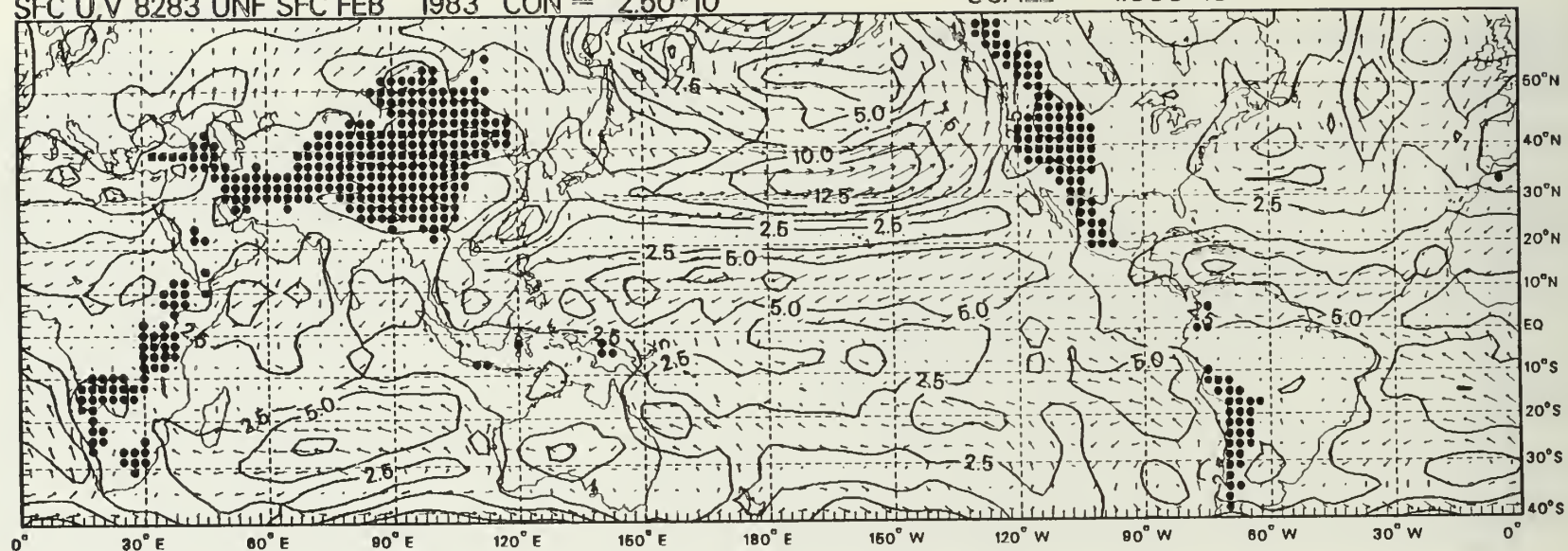
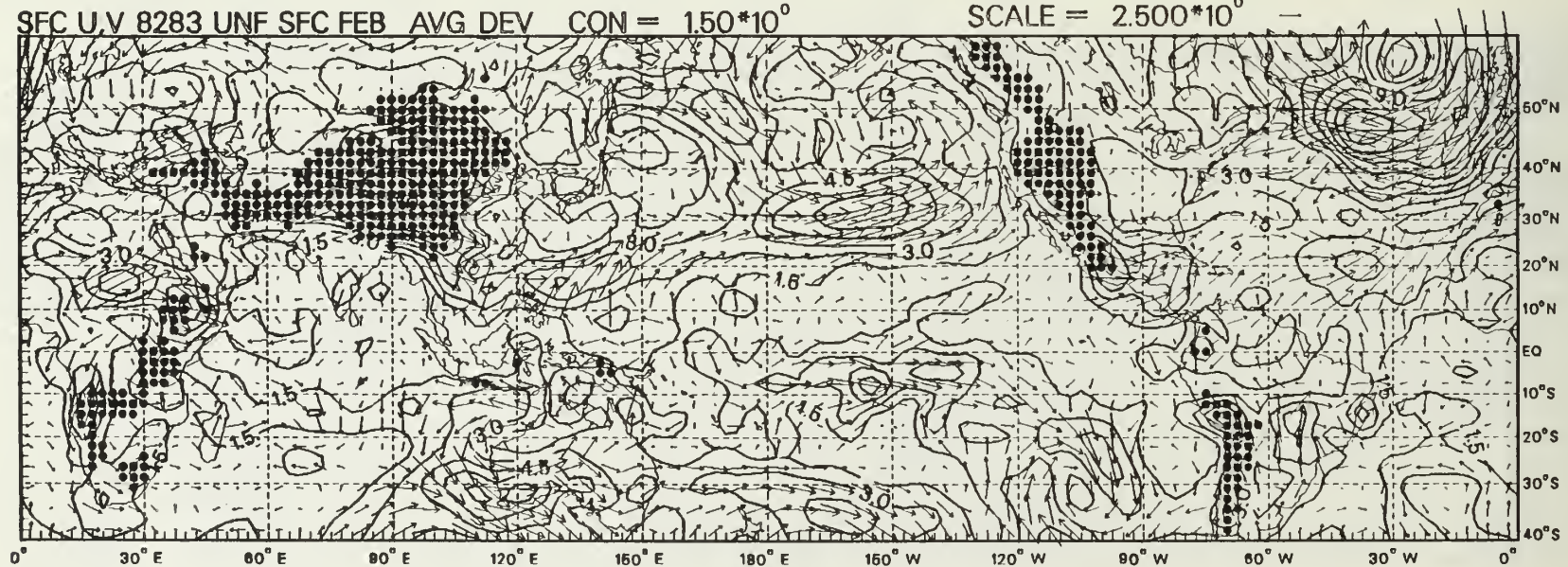


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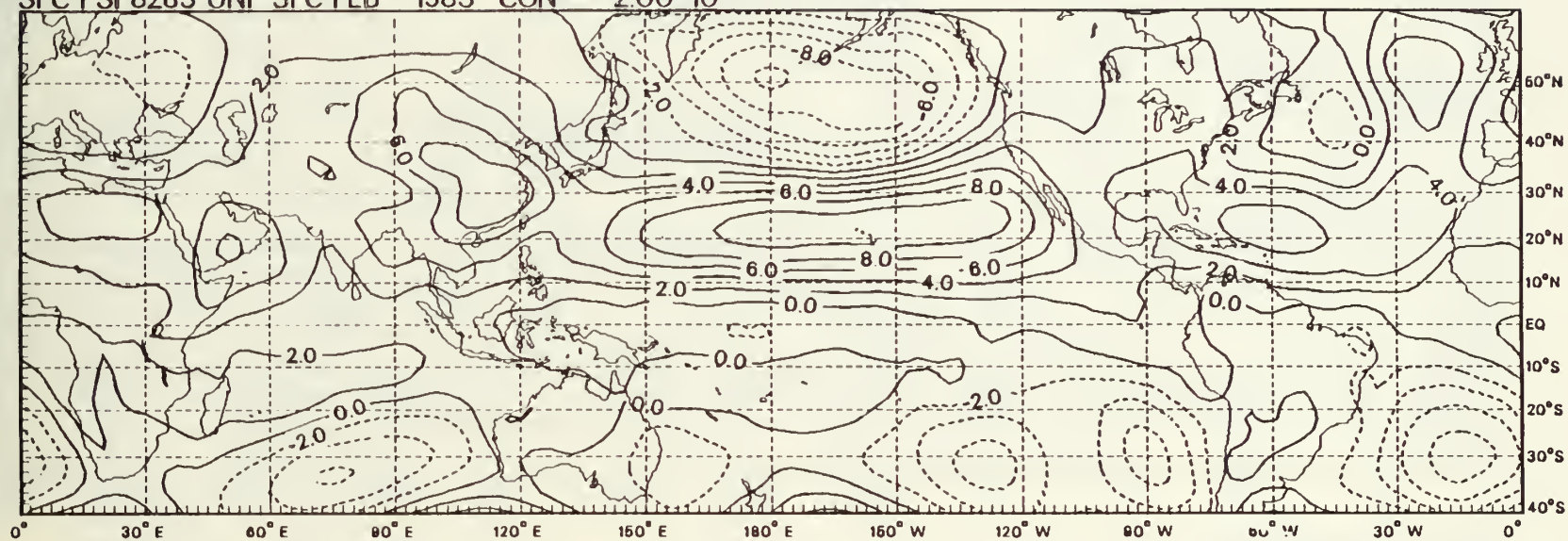
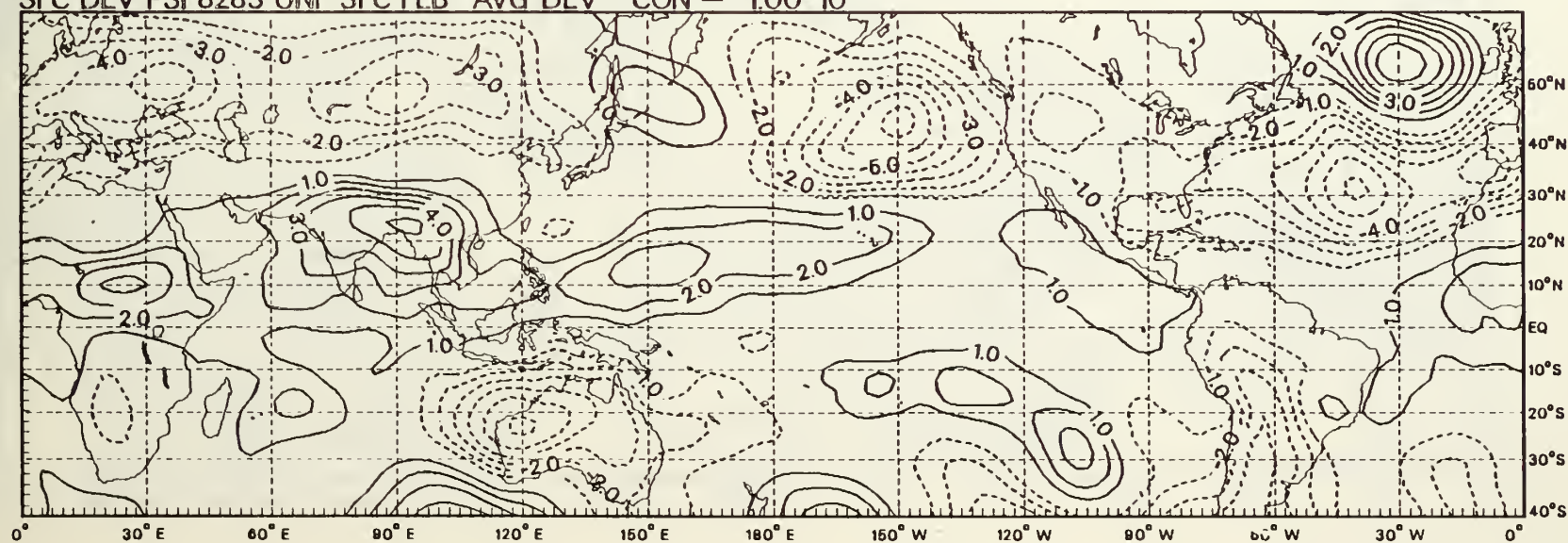


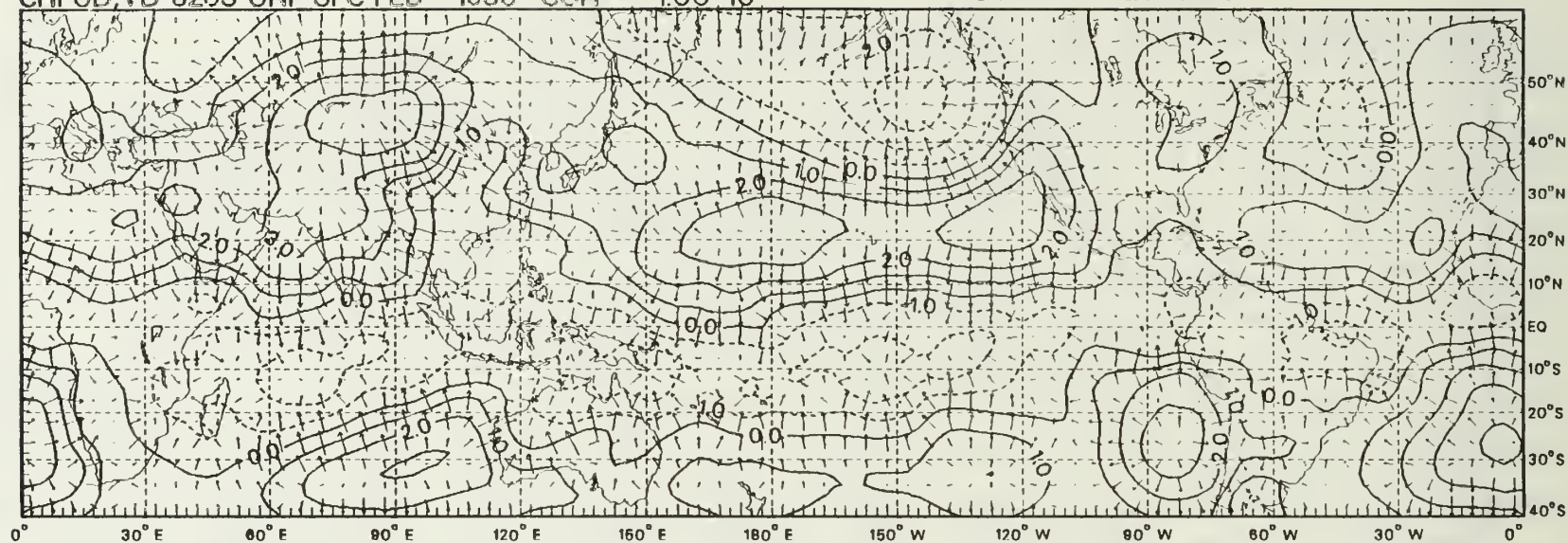
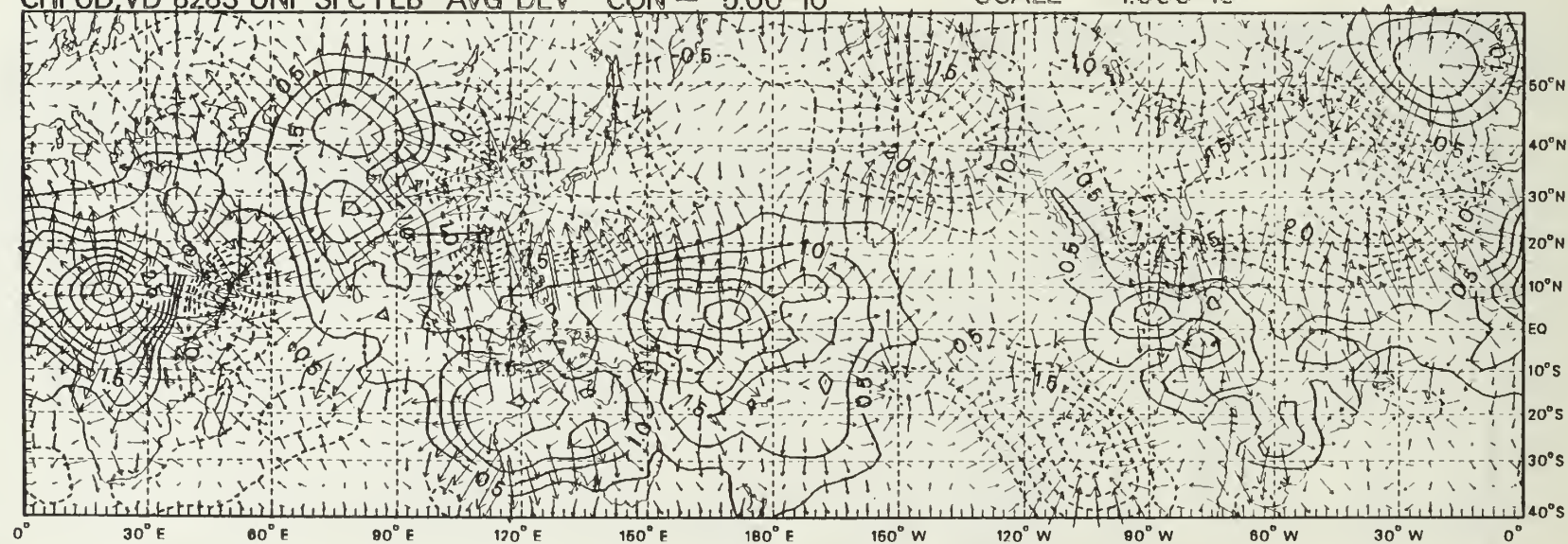
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SFC U.V 8283 UNF SFC FEB 1983 CON =  $2.50 \times 10^0$ SCALE =  $1.000 \times 10^1$  —SFC U.V 8283 UNF SFC FEB AVG DEV CON =  $1.50 \times 10^0$ SCALE =  $2.500 \times 10^0$  —



SFC PSI 8283 UNF SFC FEB 1983 CON =  $2.00 \times 10^0$ SFC DEV PSI 8283 UNF SFC FEB AVG DEV CON =  $1.00 \times 10^0$ 

CHI UD,VD 8283 UNF SFC FEB 1983 CON =  $1.00 \times 10^0$ SCALE =  $2.500 \times 10^0$ CHI UD,VD 8283 UNF SFC FEB AVG DEV CON =  $5.00 \times 10^{-1}$ SCALE =  $1.000 \times 10^0$ 



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